

COSTRUZIONI NAVALI II

(materiali compositi: criteri di resistenza)



Criterio delle massime tensioni

$$\sigma_L^t < \sigma_{LU}^t$$

$$|\sigma_L^c| < |\sigma_{LU}^c|$$

$$\sigma_T^t < \sigma_{TU}^t$$

$$|\tau_{LT}| < |\tau_{LTU}|$$

$$|\sigma_T^c| < |\sigma_{TU}^c|$$

Criterio delle massime deformazioni

$$\varepsilon_L^t < \varepsilon_{LU}^t$$

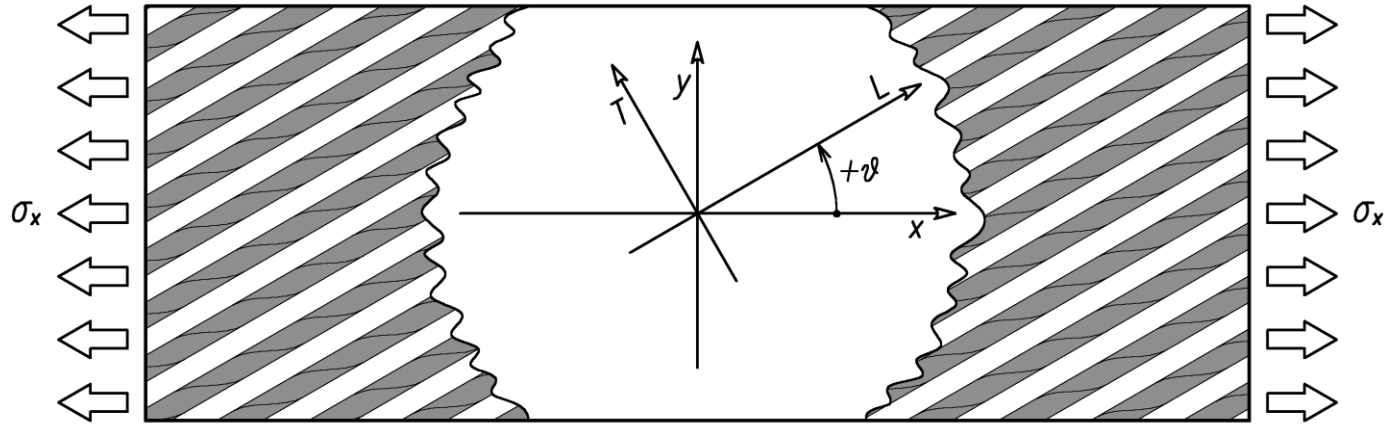
$$|\varepsilon_L^c| < |\varepsilon_{LU}^c|$$

$$\varepsilon_T^t < \varepsilon_{TU}^t$$

$$|\gamma_{LT}| < |\gamma_{LTU}|$$

$$|\varepsilon_T^c| < |\varepsilon_{TU}^c|$$

Lamina ortotropa soggetta a carico monoassiale



$$\begin{cases} \sigma_L = \sigma_x \cos^2 \theta \\ \sigma_T = \sigma_x \sin^2 \theta \\ \tau_{LT} = -\sigma_x \cos \theta \sin \theta \end{cases}$$

$$\begin{cases} \varepsilon_L = \frac{1}{E_L} (\cos^2 \theta - \nu_{LT} \sin^2 \theta) \sigma_x \\ \varepsilon_T = \frac{1}{E_T} (\sin^2 \theta - \nu_{TL} \cos^2 \theta) \sigma_x \\ \gamma_{LT} = -\frac{1}{G_{LT}} (\cos \theta \sin \theta) \sigma_x \end{cases}$$

Criterio di TSAI-HILL

$$F.I. = \left(\frac{\sigma_L}{\sigma_{LU}} \right)^2 - \frac{\sigma_L \sigma_T}{\sigma_{LU}^2} + \left(\frac{\sigma_T}{\sigma_{TU}} \right)^2 + \left(\frac{\tau_{LT}}{\tau_{LTU}} \right)^2$$

$$\sigma_{LU} = \sigma_{LU}^t \quad \text{se} \quad \sigma_L > 0 \quad (\text{trazione}) \quad \sigma_{TU} = \sigma_{TU}^t \quad \text{se} \quad \sigma_T > 0$$

$$\sigma_{LU} = \sigma_{LU}^c \quad \text{se} \quad \sigma_L < 0 \quad (\text{compressione}) \quad \sigma_{TU} = \sigma_{TU}^c \quad \text{se} \quad \sigma_T < 0$$

Criterio di TSAI–WU

$$F.I. = \left(F_1 \sigma_L + F_2 \sigma_T \right) + \left(F_{11} \sigma_L^2 + F_{22} \sigma_T^2 + 2 F_{12} \sigma_L \sigma_T + F_{66} \tau_{LT}^2 \right)$$

$$F_1 = \frac{1}{\sigma_{LU}^t} - \frac{1}{|\sigma_{LU}^c|}$$

$$F_2 = \frac{1}{\sigma_{TU}^t} - \frac{1}{|\sigma_{TU}^c|}$$

$$F_{11} = \frac{1}{\sigma_{LU}^t |\sigma_{LU}^c|}$$

$$F_{22} = \frac{1}{\sigma_{TU}^t |\sigma_{TU}^c|}$$

$$F_{66} = \frac{1}{\tau_{LTU}^2}$$

$$F_{12} = -\frac{1}{2} \sqrt{\frac{1}{\sigma_{LU}^t \sigma_{LU}^c \sigma_{TU}^t \sigma_{TU}^c}}$$

Verifica di resistenza di un laminato

$$\begin{Bmatrix} \underline{N} \\ \underline{M} \end{Bmatrix} = \begin{bmatrix} \underline{A} & \underline{B} \\ \underline{B} & \underline{D} \end{bmatrix} \begin{Bmatrix} \underline{\varepsilon}^o \\ \underline{\chi} \end{Bmatrix}$$

$$\begin{Bmatrix} \underline{\varepsilon}^o \\ \underline{\chi} \end{Bmatrix} = \begin{bmatrix} \underline{A} & \underline{B} \\ \underline{B} & \underline{D} \end{bmatrix}^{-1} \begin{Bmatrix} \underline{N} \\ \underline{M} \end{Bmatrix}$$

$$\begin{Bmatrix} \underline{\varepsilon}^o \\ \underline{\chi} \end{Bmatrix} = \begin{bmatrix} \underline{A}^{-1} & \underline{0} \\ \underline{0} & \underline{D}^{-1} \end{bmatrix} \begin{Bmatrix} \underline{N} \\ \underline{M} \end{Bmatrix}$$

$$\underline{\varepsilon}_{(x,y)_k} = \underline{\varepsilon}_{(x,y)}^o + z \underline{\chi}_{(x,y)}$$

$$\underline{\varepsilon}_{(L,T)_k}^* = \underline{T}(\theta_k) \underline{\varepsilon}_{(x,y)_k}^*$$

$$\underline{\varepsilon}_{(L,T)_k}$$

$$\underline{\sigma}_{(L,T)_k} = \underline{Q}_k \underline{\varepsilon}_{(L,T)_k}$$

$$F.I._k < 1$$