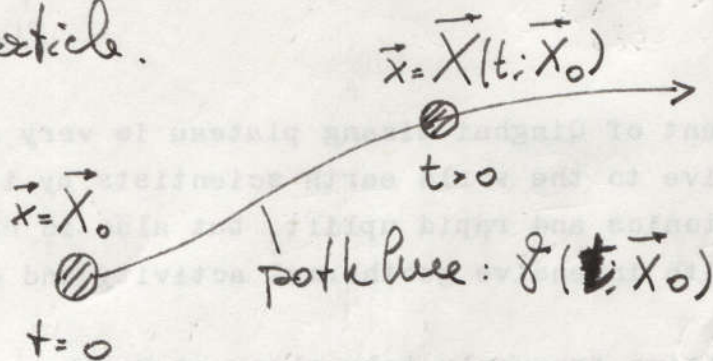


Acoustic propagation equations

- Substantial derivative: time-rate-of-change of a quantity following the motion of a fluid particle.



φ : generic quantity (e.g. density).

$$\varphi = \varphi(\vec{x}, t)$$

Following the motion of a fluid particle:

$$\varphi|_{\gamma(t; \vec{x}_0)} = \varphi(\vec{X}(t; \vec{x}_0), t)$$

$$\frac{d\varphi|_{\gamma(t; \vec{x}_0)}}{dt} = \frac{\partial \varphi}{\partial x_\kappa} \bigg|_{\vec{X}(t; \vec{x}_0), t} \frac{dX_\kappa}{dt} + \frac{\partial \varphi}{\partial t}$$

$$\frac{dX_\kappa}{dt} \equiv u_\kappa(\vec{X}(t; \vec{x}_0), t)$$

$$\Rightarrow \frac{d\varphi|_{\gamma(t; \vec{x}_0)}}{dt} = \frac{\partial \varphi}{\partial x_\kappa} u_\kappa + \frac{\partial \varphi}{\partial t}$$

$$\text{Notation: } \frac{D\varphi}{Dt} \equiv \frac{d\varphi|_{\gamma(t; \vec{x}_0)}}{dt}$$

• Physical significance of $\nabla \cdot \vec{u}$

$\frac{D}{Dt} \int_{\Omega_m} 1 dV$: time-rate of change of the volume of a material particle

Reynolds' transport theorem (Leibniz theorem applied to material volume):

$$\frac{D}{Dt} \int_{\Omega_m} 1 dV = \int_{\Omega_m} \frac{\partial 1}{\partial t} dV + \int_{\partial \Omega_m} 1 \vec{u} \cdot \hat{n} dS$$

$$= \int_{\Omega_m} \nabla \cdot \vec{u} dV$$

$$\Rightarrow \boxed{\nabla \cdot \vec{u} = \frac{1}{\int \Omega_m} \frac{D \int \Omega_m}{Dt}}$$

$\nabla \cdot \vec{u} > 0$ denotes expansion of fluid particles

$\nabla \cdot \vec{u} < 0$ denotes compression of fluid particles

- A simple derivation of the mass-conservation equation:

$$\frac{D S_m}{Dt} = 0 \quad \text{where } S_m \text{ is the mass of a fluid particle}$$

$$S_m = \rho \delta V$$

$$0 = \frac{D S_m}{Dt} = \rho \frac{D \delta V}{Dt} + \delta V \frac{D \rho}{Dt}$$

$$= \rho \delta V \frac{1}{\delta V} \frac{D \delta V}{Dt} + \rho \delta V \frac{1}{\delta V} \frac{D \rho}{Dt}$$

$$= S_m \left[\nabla \cdot \vec{u} + \frac{1}{\rho} \frac{D \rho}{Dt} \right]$$

$$\Rightarrow \boxed{\frac{1}{\rho} \frac{D \rho}{Dt} + \nabla \cdot \vec{u} = 0} \quad (1)$$

Alternative derivation: integral form. M : mass of a material volume. Then: $DM/Dt = 0$. Then, use Leibnitz's theorem to get the integral, conservation form of the mass-conservation equation.

Then, use Gauss' theorem to derive the differential, conservation form.

- A simple derivation of Euler's equations

Consider an "inviscid flow", where viscous effects are negligible (e.g., flow in regions far from solid bodies, where shear stresses are relatively weak). Then:

$$\underline{\underline{\sigma}} = -p \underline{\underline{I}}$$

Newton's law of motion yields:

$$\frac{D}{Dt}(\rho m \vec{u}) = \nabla \cdot \underline{\underline{\sigma}} \delta V$$

$$\Rightarrow \rho m \frac{D\vec{u}}{Dt} = \nabla \cdot \underline{\underline{\sigma}} \delta V \quad \text{as } \rho m = \text{const}$$

$$\Rightarrow \boxed{\rho \frac{D\vec{u}}{Dt} = -\nabla p} \quad (2)$$

- Propagation of weak acoustic (i.e., "pressure") disturbances

Consider a quiescent, ideal gas. In this equilibrium state, $P = P_0$ and $\rho = \rho_0$ throughout the "flow" field. Consider a weak perturbation propagating through the field, i.e. a perturbation giving rise to a very small "condensation" δ :

$$\delta \equiv \frac{\rho - \rho_0}{\rho_0} \ll 1$$

Assume that viscous effects are negligible, so that eq (1) and (2) can be used to model the flow. Since gases are poor heat conduction media, the flow can be assumed as adiabatic. Thus, the flow is isentropic and adiabatic or in other words, isentropic.

For isentropic transformations:

$$de = Tds - p d\sigma = - p d\sigma$$

For an ideal gas:

$$e = c_v T$$

$$p\sigma = \frac{R_0}{M} T \equiv R \cdot T$$

Thus:

$$C_v dT = - \frac{RT}{v} dv$$

$$\Rightarrow \frac{dT}{T} = - \frac{R}{C_v} \frac{dv}{v}$$

$$\Rightarrow T v^{R/C_v} = \text{const}$$

Poisson's identity: $C_p - C_v = R$

Definition of $\gamma \equiv C_p/C_v$

$$\Rightarrow C_p = \frac{\gamma R}{\gamma - 1} \quad C_v = \frac{R}{\gamma - 1}$$

$$\Rightarrow T v^{\gamma-1} = \text{const}$$

Using the equation of state:

$$\begin{aligned} P v^{\gamma} &= \text{const} \\ \frac{P}{\rho^{\gamma}} &= \text{const} \\ P T^{\frac{\gamma}{1-\gamma}} &= \text{const} \end{aligned}$$

Let's reconsider eq. (1):

$$\frac{1}{\rho(1+\delta)} \rho \frac{D\delta}{Dt} \approx \frac{\rho_0}{\rho_0} \frac{D\delta}{Dt} = \frac{D\delta}{Dt}$$

Thus, the mass conservation equation yields:

$$\frac{D\delta}{Dt} + \nabla \cdot \vec{u} = 0$$

We make the additional assumption that the velocity perturbation \vec{u} , i.e., the velocity of the fluid particles interested by the pressure disturbance, is very small compared to the propagation velocity of the disturbance itself, i.e.,

$$\frac{u}{c} = Re \ll 1$$

where Re denotes the Reynolds number. Then

$$\frac{D\delta}{Dt} = \underbrace{\frac{\partial \delta}{\partial t}}_1 + \underbrace{u \frac{\partial \delta}{\partial x}}_2 \approx \frac{\partial \delta}{\partial t}$$

$$\frac{\delta c}{L} \gg \frac{u \delta}{L}$$

Thus, the mass conservation equation reduces to:

$$\boxed{\frac{\partial \delta}{\partial t} + \nabla \cdot \vec{u} = 0} \quad (3a)$$

Consider $f(x-ct)$; $df/dt = -cf'$; $\rightarrow df/dx = f'$

Let's reconsider (2):

$$\rho \frac{D\vec{u}}{Dt} \sim \rho_0 \frac{\partial \vec{u}}{\partial t}$$

(linearized continuity eqns)
(as before)

$$\Rightarrow \boxed{\rho_0 \frac{\partial \vec{u}}{\partial t} = -\nabla p} \quad (3b)$$

From the state equation for isentropic transformations:

$$\frac{P}{\rho^\gamma} = \text{const} \Rightarrow \frac{dP}{\rho} - \gamma \frac{d\rho}{\rho} = 0$$

$dP \sim P'$ acoustic pressure

$$P' \equiv P - P_0$$

$$\frac{dP}{P} \sim \frac{P'}{P_0}$$

$$\frac{d\rho}{\rho} \sim \delta$$

$$\Rightarrow \boxed{\frac{P'}{P_0} \approx \gamma \delta} \quad (3c)$$

Let's rewrite (3a), (3b), (3c) for convenience:

$$\boxed{\frac{\partial \delta}{\partial t} + \nabla \cdot \vec{u} = 0} \quad (3a)$$

$$\boxed{\rho_0 \frac{\partial \vec{u}}{\partial t} = -\nabla P'} \quad (3b)$$

$$\boxed{\delta = \frac{1}{\gamma} \frac{P'}{P_0}} \quad (3c)$$

From (4a) and (4c):

$$\frac{1}{\rho_0} \frac{\partial \rho'}{\partial t} = -\nabla \cdot \vec{u} \quad (5a)$$

$$\Rightarrow \frac{1}{\rho_0} \frac{\partial^2 \rho'}{\partial t^2} = -\nabla \cdot \frac{\partial \vec{u}}{\partial t} \quad (5b)$$

From (4b):

$$\frac{\rho_0}{\rho_0} \nabla \cdot \frac{\partial \vec{u}}{\partial t} = -\nabla^2 \rho' \quad (5c)$$

Substituting (5b) in (5c) yields:

$$-\frac{\rho_0}{\rho_0} \frac{\partial^2 \rho'}{\partial t^2} + \nabla^2 \rho' = 0$$

$$\Rightarrow \boxed{\frac{\partial^2 \rho'}{\partial t^2} - \frac{\rho_0}{\rho_0} \nabla^2 \rho' = 0}$$

$$c^2 \equiv \frac{\rho_0}{\rho_0} = \rho_0 B_0 \text{ speed of sound}$$

$$\boxed{\frac{\partial^2 \rho'}{\partial t^2} - c^2 \nabla^2 \rho' = 0} \text{ wave equation}$$

Meaning of c^2 is very clear in 1D, where the general solution in "open field" is

$$\rho' = f(x-ct) + g(x+ct)$$

c is indeed the propagation velocity of the pressure disturbance.

In air:

$$\gamma \approx 1.4 \quad R \approx 287 \frac{\text{J}}{\text{kg K}}$$

$$T_0 \approx 293 \text{ K}$$

$$c = \sqrt{\gamma R T_0} \approx 343 \text{ m/s}$$

In Helium:

$$R = 2077 \frac{\text{J}}{\text{kg K}}$$

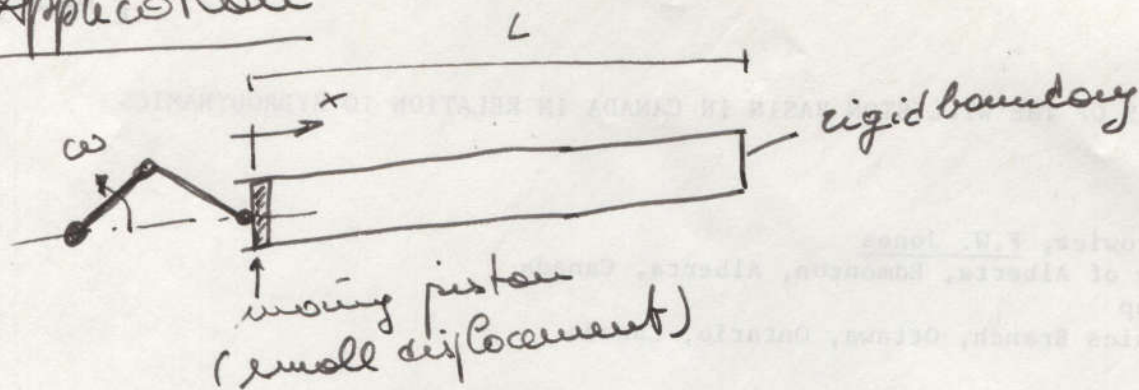
$$c \approx 923 \text{ m/s}$$

In CO_2 :

$$R = 188.9 \frac{\text{J}}{\text{kg K}}$$

$$c = 278 \text{ m/s}$$

Application



$$6a) \quad \frac{\partial^2 p'}{\partial t^2} - c^2 \frac{\partial^2 p'}{\partial x^2} = 0$$

$$6b) \quad u'(0,t) = U \cos \omega t$$

$$6c) \quad u'(L,t) = 0$$

$$6d) \quad p'(x,0) = 0 ; u'(x,0) = 0$$

From (6b) :

$$\rho \frac{\partial u'}{\partial t} = - \frac{\partial p'}{\partial x}$$

From 6b) :

$$\rho \frac{\partial u'}{\partial t} = \rho U \omega \sin \omega t = - \frac{\partial p'}{\partial x}$$

$$\Rightarrow \boxed{\frac{\partial p'}{\partial x} = \rho U \omega \sin \omega t} \quad \text{at } x=0$$

From 6c) :

$$\boxed{\frac{\partial p'}{\partial x} = 0} \quad \text{at } x=L$$

Thus, we are left with :

$$\frac{\partial^2 p'}{\partial t^2} - c^2 \frac{\partial^2 p'}{\partial x^2} = 0 \quad x \in (0,L)$$

$$\frac{\partial p'}{\partial x} = \rho U \omega \sin \omega t \quad \text{at } x=0$$

$$\frac{\partial p'}{\partial x} = 0 \quad \text{at } x=L$$

$$P'(x, 0) = 0; \quad u'(x, 0) = 0$$

From $u'(x, 0) = 0$ and (5a):

$$\frac{\partial \delta}{\partial t} = 0$$

From (5c):

$$\frac{\partial}{\partial t} \left(\frac{1}{r} \frac{P'}{\rho_0} \right) = 0 \Rightarrow \frac{\partial P'}{\partial t}(x, 0) = 0$$

A very simple F.D. solution:

$$\frac{P_j^{u+1} - 2P_j^u + P_j^{u-1}}{(\Delta t)^2} - c^2 \frac{P_{j+1}^u - 2P_j^u + P_{j-1}^u}{h^2} = 0$$

B.C. at $x=0$

$$\frac{P_1^{u+1} - P_0^{u+1}}{h} = 0$$

$$P_0^{u+1} = P_1^{u+1} \quad \text{or} \quad P_0^{u+1} = P_1^{u+1} - \rho_0 U h c \omega \Delta t$$

B.C. at $x=L$

$$P_{N+1}^{u+1} = P_N^{u+1}$$

I.C. 1:

$$P_j^0 = 0 \quad \forall j$$

I.C. 2:

$$P_j^1 = P_j^0 \quad \forall j \quad \text{Why?}$$

Homework:

HOMEWORK

- 1) Note problem dimensions
- 2) Solve analytically (implicit transient)
- 3) Solve numerically
- 4) Derive stability limit (e.g., by von Neumann analysis).

5) Derive the modified PDE for the proposed scheme.
Present results.

6) Try an explicit scheme
(i.e., $\frac{\delta^2 P}{\delta x^2}$ computed at t_{n+1})

$$\text{or } \frac{\delta^2 P}{\delta x^2} \approx (1-\alpha) \frac{\delta^2 P^n}{\delta x^2} + \alpha \frac{\delta^2 P^{n+1}}{\delta x^2}$$

Derive stab. limit.

7) Verify your algorithms using
either analytical solutions or MDS.

The Neumann Stability analysis

$$P_j^{n+1} = -P_j^{n-1} + 2(1-\alpha^2)P_j^n + \alpha^2(P_{j+1}^n + P_{j-1}^n)$$

$$\alpha = \frac{c\Delta t}{h}$$

Look for a harmonic solution

$$P_j^n = \theta^n e^{i\tilde{k}x_j} = \theta^n e^{2\pi i \frac{j}{L} \tilde{k}}$$

$$\tilde{k} \equiv \frac{2\pi k}{L}$$

Introduce the "modified" wavenumber

$$\hat{k} \equiv \tilde{k}h$$

$$P_j^n = \theta^n e^{i\hat{k}j}$$

Then:

$$\theta^2 = 2(1-\alpha^2)\theta - 1 + 2\alpha^2 \cos(\hat{k}) \theta$$

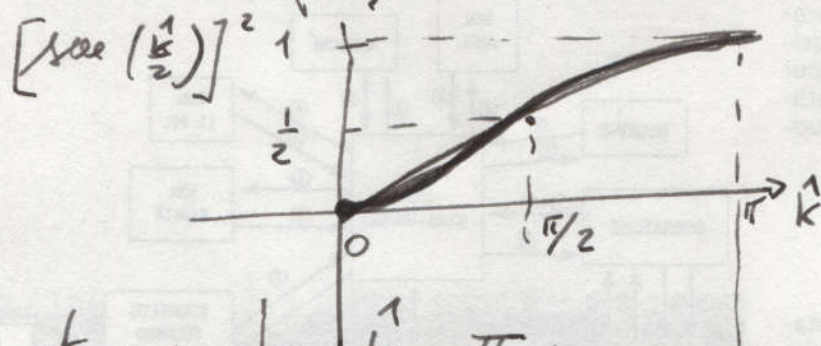
Let $\beta \equiv 1 - 2\alpha^2 \sin^2(\frac{\hat{k}}{2})$ to get: $\frac{1}{2}(1 + \cos(\frac{k}{2} + \frac{k}{2}))$ and expand...

$$\boxed{\theta_{1,2} = \beta \pm \sqrt{\beta^2 - 1}}$$

For $|\beta| > 1$ at least one of the $|\theta_{1,2}|$ is bigger than 1. Thus, we look for $|\beta| \leq 1$ for stability:

$$-1 \leq 1 - 2\alpha^2 \sec^2\left(\frac{k^1}{2}\right) \leq 1$$

$$-1 \leq 1 - 2\alpha^2 \sec^2\left(\frac{k^1}{2}\right) \Rightarrow 1 - \alpha^2 \sec^2\left(\frac{k^1}{2}\right) \geq 0$$



Worst case for $k^1 = \pi$:

$$1 - \alpha^2 \geq 0 \Rightarrow \boxed{\alpha \leq 1}$$

$$1 - 2\alpha^2 \sec^2\left(\frac{k^1}{2}\right) \leq 1 \Rightarrow -2\alpha^2 \sec^2\left(\frac{k^1}{2}\right) \leq 0 \text{ True } \forall k^1$$

Thus, the stability condition derived from

$$V.N. analysis is \boxed{\alpha \leq 1}$$

Analytical solution of the wave equation in 1D

$$\frac{\partial^2 u}{\partial t^2} = c^2 \frac{\partial^2 u}{\partial x^2} \quad (1)$$

Solve by

▷ d'Alembert's method

▷ Fourier Transform

▷ Separation of variables

Let's try to solve (1) by d'Alembert's method.

$$\xi = x - ct \quad \eta = x + ct$$

$$\begin{aligned} u_{,x} &= u_{,\xi} \xi_{,x} + u_{,\eta} \eta_{,x} \\ &= u_{,\xi} + u_{,\eta} \end{aligned}$$

$$\begin{aligned} u_{,\eta} &= u_{,\xi} (-c) + u_{,\eta} \cdot c \\ &= c(u_{,\eta} - u_{,\xi}) \end{aligned}$$

$$u_{,xx} = u_{,\xi\xi} + 2u_{,\xi\eta} + u_{,\eta\eta}$$

$$\begin{aligned} u_{,tt} &= c^2((-c)u_{,\xi\eta} - (-c)u_{,\xi\eta} + c u_{,\eta\eta} - c u_{,\xi\xi}) \\ &= c^2(u_{,\xi\xi} - 2u_{,\xi\eta} + u_{,\eta\eta}) \end{aligned}$$

Thus eq (1) becomes

$$c^2(u_{\eta\eta} - 2u_{\xi\eta} + u_{\xi\xi}) = (u_{\xi\xi} + 2u_{\xi\eta} + u_{\eta\eta})c^2$$

\Rightarrow

$$u_{\xi\eta} = 0$$

See what happens solving along $\xi = \text{const}$ or $\eta = \text{const}$ lines: you find that $u = \text{const}$ along these lines. They are characteristic lines for eq (1).

However:

$$\frac{\partial}{\partial \xi} \frac{\partial u}{\partial \eta} = 0 \Rightarrow \frac{\partial u}{\partial \eta} = f(\xi)$$

$$\Rightarrow u = F(\xi) + g(\eta)$$

This is a general solution for eq (1) and can be written more conveniently as

$$u(x, t) = F(x + ct) + g(x - ct)$$

To get F and G we need the initial conditions.

$$u_{tt} - c^2 u_{xx} = 0 \quad t \geq 0$$

$$u(x, 0) = f(x)$$

$$u_t(x, 0) = g(x)$$

We need to express F and G in terms of f and g .
Thus;

$$u(x, 0) = F(x) + G(x) = f(x) \quad (2a)$$

$$u_t(x, 0) = F_x|_{t=0} + G_x|_{t=0}$$

$$= F_x|_{t=0} - G_x|_{t=0}$$

$$= c(F'(x) - G'(x)) = g(x) \quad (2b)$$

Differentiate (2a):

$$F'(x) + G'(x) = f'(x) \quad (2c)$$

Solve (2b), (2c) in terms of F' and G' :

$$F'(x) = \frac{1}{2} \left[f'(x) + \frac{1}{c} g(x) \right]$$

$$G'(x) = \frac{1}{2} \left[f'(x) - \frac{1}{c} g(x) \right]$$

Hence:

$$F(x) = \frac{1}{2} f(x) + \frac{1}{2c} \int_0^x g(y) dy + C_1$$

$$G(x) = \frac{1}{2} f(x) - \frac{1}{2c} \int_0^x g(y) dy + C_2$$

Notice that, from (2a):

$$f(x) = F(x) + G(x) = f(x) + C_1 + C_2$$

yielding

$$C = C_2 = -C_1$$

and

$$F(x) = \frac{1}{2} f(x) + \frac{1}{2c} \int_0^x g(y) dy - C$$

$$G(x) = \frac{1}{2} f(x) - \frac{1}{2c} \int_0^x g(y) dy + C$$

The ~~general~~ solution of the IVP is thus:

$$u(x,t) = F(x+ct) + G(x-ct)$$

$$= \frac{1}{2} (f(x+ct) + f(x-ct))$$

$$+ \frac{1}{2c} \int_{x-ct}^{x+ct} g(y) dy$$