

# Dynamic behavior of first-order and second-order processes

DINAMICA E CONTROLLO DEI PROCESSI CHIMICI  
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Corso di Laurea Magistrale in Ingegneria di Processo e dei Materiali



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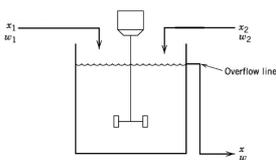
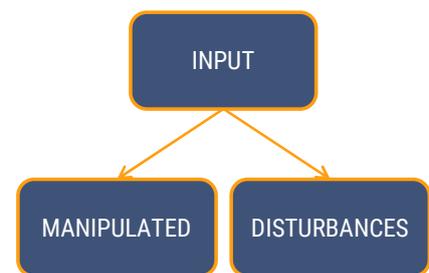
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## THE INPUTS TO A DYNAMIC SYSTEM

- To design a process control system, the dynamic system (i.e., the process) response to the input needs to be known
  - i.e., how the system responds to **any input** variable change that can affect the output (specifically, the target variable to control)
  - The **TF** is the tool allowing to evaluate the effect that different inputs transfer on the output
  - The adoption of TFs allows the generalization of the description of the dynamic behavior of a process



$$\text{Output } X'(s) = G_1(s) \text{input 1 } X_1'(s) + G_2(s) \text{input 2 } X_2'(s)$$

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## ANALYSIS OF THE DYNAMICS OF A SYSTEM

■ In order to study the study dynamics we will follow the following procedure:

1. We **perturb** the system applying a variation (**forcing function**) on each input ( $u_i$ ) **individually**, keeping any existent control loop **open**
  - ❖ In case of multiple input, they are changed alternatively one at a time
2. We **collect** the observation on the dynamic response of the output  $y$
3. We extract **general information** about the steady-state and dynamic behavior of the system
4. We exploit this information to **design** the controller, i.e. to determine the closed-loop response of the system



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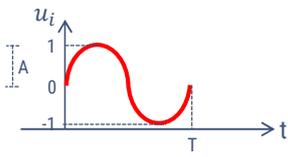
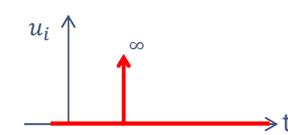
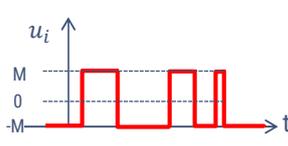


## LIST OF PERTURBATIONS

|                              | REAL EXAMPLES   | FORCING FUNCTION   | LAPLACE TRANSFORM                          |
|------------------------------|---|--|--|
| <b>STEP - S(t)</b><br>       | A valve whose opening is changed in a very short time interval  | $u(t) = \begin{cases} 0 & t < 0 \\ M & t \geq 0 \end{cases}$                         | $U_S(s) = \frac{M}{s}$                     |
| <b>RAMP - R(t)</b><br>       | A valve whose opening is changed at a constant rate   | $u(t) = \begin{cases} 0 & t < 0 \\ at & t \geq 0 \end{cases}$                        | $U_R(s) = \frac{a}{s^2}$                   |
| <b>RECTANGULAR PULSE</b><br> | A valve whose opening is instantaneously increased for a time interval and set back to initial value at the end | $u(t) = \begin{cases} 0 & t < 0 \\ h & 0 \leq t < t_w \\ 0 & t \geq t_w \end{cases}$ | $U_{RP}(s) = \frac{h}{s} (1 - e^{-t_w s})$ |

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| LIST OF PERTURBATIONS   |   | /cont'd   |   |
|---|---|---|---|
|   | REAL EXAMPLES   | FORCING FUNCTION  | LAPLACE TRANSFORM                             |
| <b>SINUSOIDAL - sin(t)</b><br> | Daily variation of cooling water temperature                                      | $u(t) = \begin{cases} 0 & t < 0 \\ A \sin \omega t & t \geq 0 \end{cases}$  | $U_{sin}(s) = \frac{A\omega}{s^2 + \omega^2}$ |
| <b>UNIT PULSE - UP(t)</b><br>  | Difficult to obtain; it can be approximated by a tracer injection for RTD studies | $u(t) = \begin{cases} 0 & t < 0 \\ \infty & 0 \leq t < t_w \\ 0 & t \geq t_w \end{cases}$<br>With $t_w \rightarrow 0$ | $U_{UP}(s) = 1$                               |
| <b>RANDOM</b><br>              | Usually characterized with statistical term (mean, st.dev.)                       |   |   |

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## FIRST-ORDER SYSTEMS

- They are constituted by a 1°-order differential equation with  $a_0 \neq 0$ :
 

$$\frac{a_1}{a_0} \frac{dy(t)}{dt} + y(t) = \frac{b_0}{a_0} u(t) \quad \rightarrow \quad \boxed{\tau \frac{dy(t)}{dt} + y(t) = Ku(t)}$$

Called: **first-order lag**

$$\boxed{G(s) = \frac{Y(s)}{U(s)} = \frac{K}{\tau s + 1}}$$
  - > K: **steady-state gain** of the system [output u.m./input u.m.]
  - >  $\tau > 0$ : **time constant** of the system [time]
- Assume that  $u(t)$  is at steady-state and at time  $t=0$  a perturbation occurs
- We need to take into account two different types of **perturbations**
  - > **Step** input change:  $U_S(s) = \frac{M}{s}$
  - > **Sinusoidal** input change:  $U_{sin}(s) = \frac{A\omega}{s^2 + \omega^2}$

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## STEP RESPONSE OF FO SYSTEMS

$$u(t) = \begin{cases} 0 & t < 0 \\ M & t \geq 0 \end{cases}$$

$$G(s) = \frac{K}{\tau s + 1}; \quad Y(s) = G(s)U(s); \quad U(s) = \frac{M}{s}$$

$$\rightarrow Y(s) = \frac{KM}{s(\tau s + 1)}$$

$$y|_{t=0^+} = 0$$
  

$$y|_{t=\infty} = KM$$

Upon inverse transform:  $y(t) = KM(1 - e^{-\frac{t}{\tau}})$

- ▶ The process starts responding to the perturbation instantaneously
- ▶ The speed of change y is maximum at t=0, then it progressively decreases to 0
- ▶ A new steady-state is attained only as  $t \rightarrow \infty$
- ▶ It only takes a time equal to 4-5 time constants for the transient to die out
- ▶  $\tau$  provides an indication on the speed of response:  $\uparrow \tau \rightarrow$  slow response
- ▶ K indicates how far the new steady state value of y is from the original one:  $\uparrow K \rightarrow$   $\uparrow$  amplification of input variation onto the output

| t       | y/(KM) |
|---------|--------|
| 0       | 0      |
| $\tau$  | 0.6321 |
| $2\tau$ | 0.8647 |
| $3\tau$ | 0.9502 |
| $4\tau$ | 0.9817 |
| $5\tau$ | 0.9933 |

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## RESPONSE OF FO SYSTEMS TO A SINUSOIDAL

$$u(t) = \begin{cases} 0 & t < 0 \\ A \sin \omega t & t \geq 0 \end{cases}$$

$$G(s) = \frac{K}{\tau s + 1}; \quad Y(s) = G(s)U(s); \quad U(s) = \frac{A\omega}{s^2 + \omega^2}$$

$$\rightarrow Y(s) = \frac{KA\omega}{(\tau s + 1)(s^2 + \omega^2)}$$

Upon inverse transform:  $y(t) = \frac{KA\omega\tau}{\omega^2\tau^2 + 1} e^{-\frac{t}{\tau}} + \frac{KA}{\sqrt{\omega^2\tau^2 + 1}} \sin(\omega t + \phi)$

$\phi = \tan^{-1}(-\omega\tau) = \text{phase angle [rad]}$

- ▶ An initial transient exists, which dies out after a few  $\tau$
- ▶ Then the response is purely sinusoidal (periodic), as the input perturbation
- ▶ The amplitude of the response sinusoid is different from that (A) of the forcing function; It depends on:
  - ❖ The process: K,  $\tau$
  - ❖ The forcing function, namely its angular frequency  $\omega$  (hence on frequency f or period  $T = 2\pi/\omega = 1/f$ )
- ▶ The system response lags behind the input
  - ❖ The phase shift  $\phi$  depends on the dynamic characteristics of the system ( $\tau$ ) and of those of the forcing function ( $\omega$ )

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## EFFECT OF FREQUENCY

$$u(t) = A \sin(\omega t)$$

$$y(t) = \frac{KA\omega\tau}{\omega^2\tau^2 + 1} e^{-\frac{t}{\tau}} + \frac{KA}{\sqrt{\omega^2\tau^2 + 1}} \sin(\omega t + \phi) \quad \phi = \tan^{-1}(-\omega\tau) = \text{phase angle [rad]}$$

- What's the influence of the input frequency  $f$  (hence its angular frequency  $\omega$ ) on the response?
- The ratio between the response amplitude and the input amplitude is given by:
 

Amplitude ratio

$$AR = \frac{\text{amplitude response}}{\text{amplitude input}} = \frac{K}{\sqrt{\omega^2\tau^2 + 1}}$$

❖  $\uparrow$  in.  $\omega \rightarrow \downarrow$  out. ampl  
 ❖  $\uparrow\uparrow$  in.  $\omega \rightarrow$  response flattens, i.e. the input is filtered by the process  
 ❖ The same holds true if the process has a  $\uparrow\uparrow\uparrow \tau$
- The phase shift (lag)  $\phi$  between the sine waves is maximum ( $-\pi/2\text{rad}$ ) when the input frequency is very large
- The input frequency can be denoted as «large» of «small» depending on the dynamic characteristic of the process ( $\tau$ )

What matters is the product  $\omega\tau$

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## EXAMPLES

- 4° ed., Example 5.1, p. 71; 3° ed, 5.1 p.78

**EXAMPLE 5.1**

A stirred-tank heating system described by Eq. 4-37 is used to preheat a reactant containing a suspended solid catalyst at a constant flow rate of 1000 kg/h. The volume in the tank is 2 m<sup>3</sup>, and the density and specific heat of the suspended mixture are, respectively, 900 kg/m<sup>3</sup> and 1 cal/g °C. The process initially is operating with inlet and outlet temperatures of 100 and 130 °C. The following questions concerning process operations are posed:

- What is the heater input at the initial steady state and the values of  $K$  and  $\tau$ ?
- If the heater input is suddenly increased by +30%, how long will it take for the tank temperature to achieve 99% of the final temperature change?
- Assume the tank is at its initial steady state. If the inlet temperature is increased suddenly from 100 to 120 °C, how long will it take before the outlet temperature changes from 130 to 155 °C?

$$T'(s) = \frac{1/wC}{\frac{m}{w}s + 1} Q'(s) + \frac{1}{\frac{m}{w}s + 1} T'_i(s)$$

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