Systems Dynamics

Course ID: 267MI - Fall 2020

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Lecture 4 Model Identification from Data

4. Model Identification from Data

4.1 System Identification: an Introduction

4.1.1 "Transparent Box" vs. "Black Box" Modeling Approach

4.2 An Example: a Real Application

System Identification: an Introduction

Modelling Identification Prediction & filtering

Disciplines providing tools to **estimate** variables and unknown parameters and to **design models** of natural and artificial systems using **experimental data**. Constructing models for a slice of reality and studying their properties is really what science is about. The **models** – "the hypotheses", "the laws of nature", "the paradigms" – can be of a more or less formal character, but they all have the **fundamental property** that they try **to link observations to some pattern**.

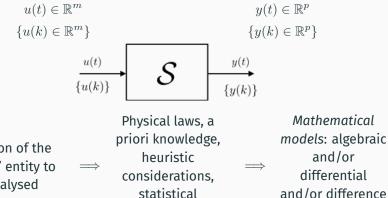
L. Ljung, T. Glad, "Modeling of Dynamic Systems", Prentice Hall, 1994

System Identification: an Introduction

"Transparent Box" vs. "Black Box" Modeling Approach So far, approach undertaken to devise dynamical models:

Inputs ("causes")

Outputs ("effects")



and/or difference equations

Definition of the "system" entity to be analysed

evidence, etc.



Experimental data, sensor measurements, historical data, etc.

"Black-box" modeling approach

Input, output and disturbance variables are characterized in terms of numerical sequences. These are the data to be used to determine the dynamical model.

Given: $\{y(k)\}, \{u(k)\}$

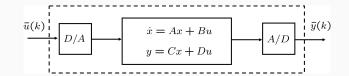
Discrete-time model:

- continuous-time system and data obtained by sampling
- discrete-time system and data inherently discrete-time

Finite-difference equations

Continuous-Time System and Data Obtained by Sampling

Linear, time-invariant case:



 $u(t) = \bar{u}(k) \qquad \text{Recall the step-invariant transform} \qquad \bar{y}(k) = y(t_k)$ $t_k \le t < t_{k+1} \qquad \begin{cases} \bar{x} \left[(k+1) \right] = \bar{A}\bar{x} \left(k \right) + \bar{B}\bar{u} \left(k \right) \\ \bar{y} \left(k \right) = \bar{C}\bar{x} \left(k \right) + \bar{D}\bar{u} \left(k \right) \end{cases}$

Letting $t_{k+1} - t_k = \Delta$

$$\bar{A} = e^{A\Delta}$$
 $\bar{B} = \int_0^\Delta e^{Ar} B \, dr$ $\bar{C} = C$ $\bar{D} = D$

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Continuous-Time System and Data Obtained by Sampling (cont.)

$$\begin{array}{c} \bar{u}(k) \\ \hline D/A \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} \dot{x} = Ax + Bu \\ y = Cx + Du \\ \hline \end{array} \\ \hline \end{array} \\ \hline \end{array} \\ \hline \begin{array}{c} \bar{y}(t_{k'}) \\ \hline \end{array} \\ \hline \end{array}$$

 $\begin{array}{ll} u(t) = \bar{u}(k) & \text{What if the output is sampled at} & \bar{y}(k) = y\left(t_{k'}\right) \\ t_k \leq t < t_{k+1} & t_{k'} \neq t_k \text{ with } t_k \leq t_{k'} < t_{k+1} \end{array}$

· Let's recall the expression

$$y(t) = C e^{A(t-t_0)} x(t_0) + C \int_{t_0}^t e^{A(t-\tau)} Bu(\tau) d\tau + Du(t)$$

for the movement of the output of a continuous-time LTI system (from "Fundamentals of Automatic Control").

Continuous-Time System and Data Obtained by Sampling (cont.)

• Let's consider t_k as initial time instant (i.e $t_0 = t_k$), the instant $t_{k'}$ as final time instant and let's assume $t_{k'} - t_k = \alpha$. Recall also the stair-wise behavior of the input signal: $u(t) = \bar{u}(k), t_k \leq t < t_{k+1}$.

$$y(t_{k'}) = C e^{A\alpha} x(t_k) + C \left(\int_{t_k}^{t_{k'}} e^{A(t_{k'} - \tau)} B \, d\tau \right) u(t_k) + Du(t_k)$$

- Substitute $r = t_{k'} - \tau\,$ into the integral term and rewrite the expression

$$y(t_{k'}) = C e^{A\alpha} x(t_k) + C \left(\int_0^\alpha e^{Ar} dr \right) Bu(t_k) + Du(t_k)$$

· Let's compare with the discrete-time output expression

$$\bar{y}(k) = \bar{C}\bar{x}(k) + \bar{D}\bar{u}(k)$$

Continuous-Time System and Data Obtained by Sampling (cont.)

• If $t_{k'} \neq t_k$ then

$$\bar{C} = C e^{A\alpha} \qquad \bar{D} = C \left(\int_0^\alpha e^{Ar} dr \right) B + D \qquad t_{k'} - t_k = \alpha \left(< \Delta \right)$$

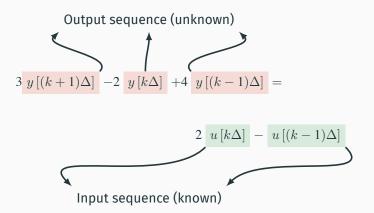
• When $t_{k'} = t_k$ obviously

$$\bar{C} = C \qquad \bar{D} = D$$

 In both the cases the following expressions hold (remember the step-invariant transform)

$$\bar{A} = e^{A\Delta}$$
 $\bar{B} = \int_0^\Delta e^{Ar} B \, dr$ $\Delta = t_{k+1} - t_k \, \forall k$

As usual, let's assume Δ as the sampling time.



• With sampling-time Δ enhanced:

$$\begin{aligned} &3y\left[(k+1)\Delta\right]-2y\left[k\Delta\right]+4y\left[(k-1)\Delta\right]=\\ &2u\left[k\Delta\right]-u\left[(k-1)\Delta\right]\end{aligned}$$

• Compact:

$$3y_{k+1} - 2y_k + 4y_{k-1} = 2u_k - u_{k-1}$$

- Typical framework: linear finite-difference equations with constant coefficients.
- General expression takes on the form:

$$a_n y_{k+n} + a_{n-1} y_{k+n-1} + \dots + a_0 y_k =$$

 $b_m u_{k+m} + b_{m-1} u_{k+m-1} + \dots + b_0 u_k$

with given initial conditions

$$\{y_k: k = -n, -(n-1), \ldots, 0\}$$

and known input sequence u_k .

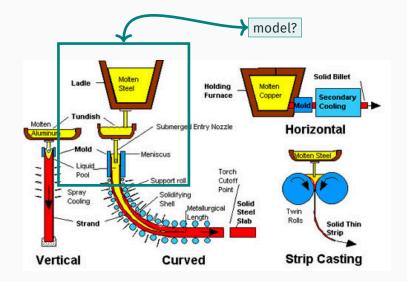
An Example: a Real Application

A Real Application: Steel Continuous Casting

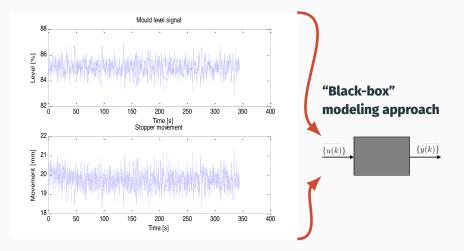


The molten steel can be tapped from the bottom of the ladle into an intermediate container known as the tundish. The temperature of the melt is now below 1.600°C. The open mould consists of four watercooled plates between which the hot steel slides. A solidified shell is formed during casting. The casting temperature is around 1.540°C. The steel is still glowing hot but hos solidified all the way through when it is cut into slabs by means of oxygen lances. The temperature Cooling continues by is 1.000°C. Every slab is marked before it is quenching with water along placed on the cooling bed. the whole of the strand.

A Real Application: Steel Continuous Casting (cont.)



A Real Application: Steel Continuous Casting (cont.)



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