

# Image Processing for Physicists

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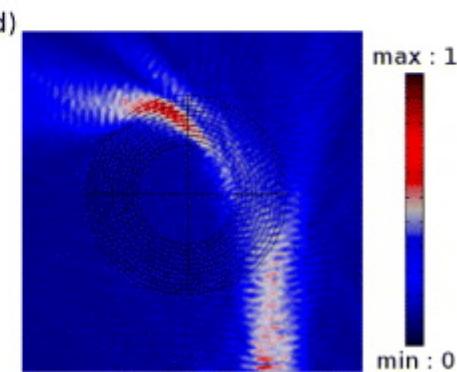
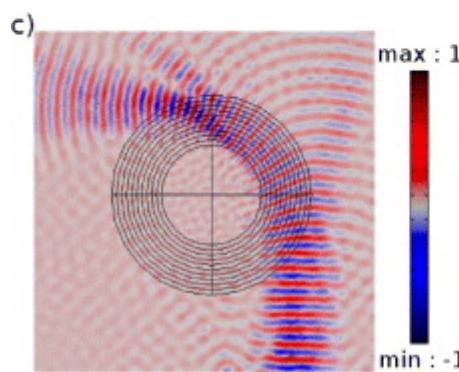
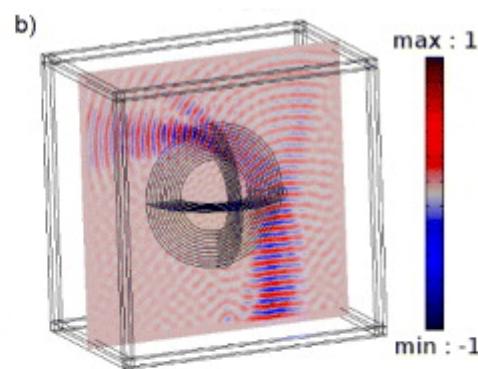
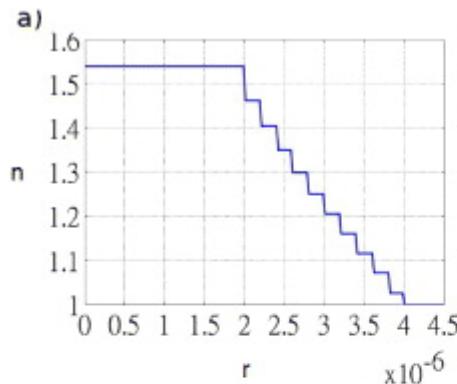
# Overview

- Propagation modelization
- Wave propagation:
  - Near-field regime
  - Far-field regime

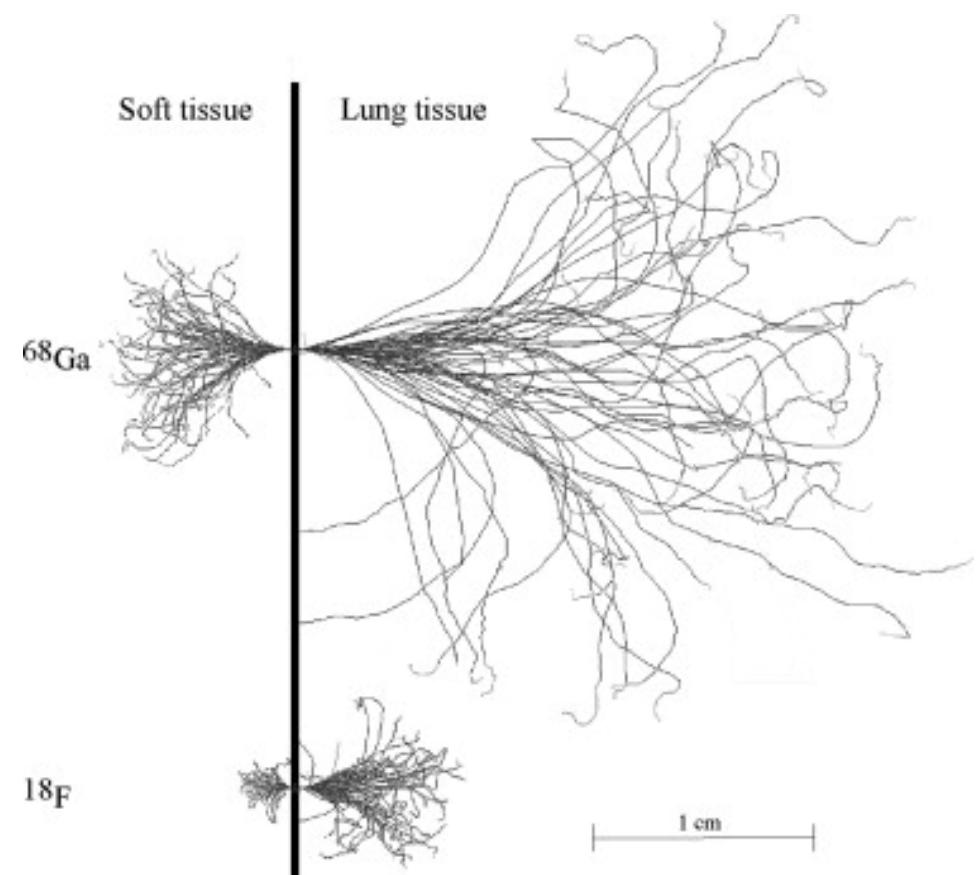
# Propagation modeling

- Motivations:

## 1. Validation



Finite element simulation of an electro-magnetic field in a dielectric



sources: T.M. Chang *et al.* New J. Phys. (2012)  
A. Sanchez-Crespo, Appl. Rad. Isotopes (2012)

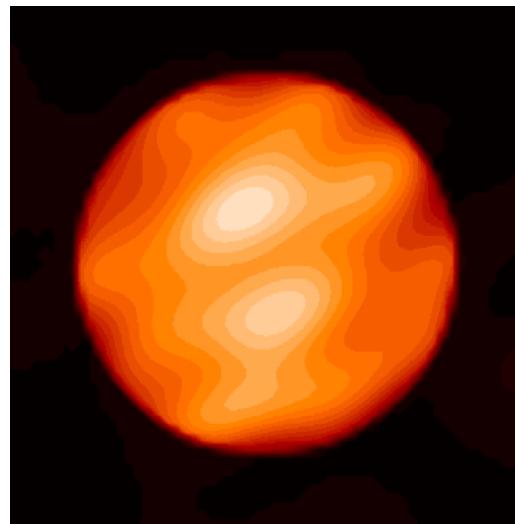
# Propagation modeling

- Motivations:

## 2. Inversion



Image reconstruction from sound wave propagation (ultrasonography)



The surface of Betelgeuse reconstructed from interferometric data (IOTA)



sources: wikipedia  
Haubois *et al. Astronom. & Astrophys.* (2009)

# Propagation modeling

- Particles
  - Model particle tracks (rays) through different media
  - Model may include: refraction, force fields, particle decay and interactions
  - Not included: diffraction
- Wave
  - Model the interaction of a field with a medium
  - Can be very complicated → approximations are needed

# Propagation modeling

Starting point: Helmholtz equation

- for EM field: neglect polarization (scalar wave approximation)

- for electron wave, assume high energy electrons

Maxwell eq.  $\rightarrow \nabla^2 \psi + \frac{n^2}{c^2} \frac{\partial^2}{\partial t^2} \psi = 0$  index of refraction (spatially dependent)

$\psi$ : complex-valued field (scalar: no polarization)

$n$ : index of refraction

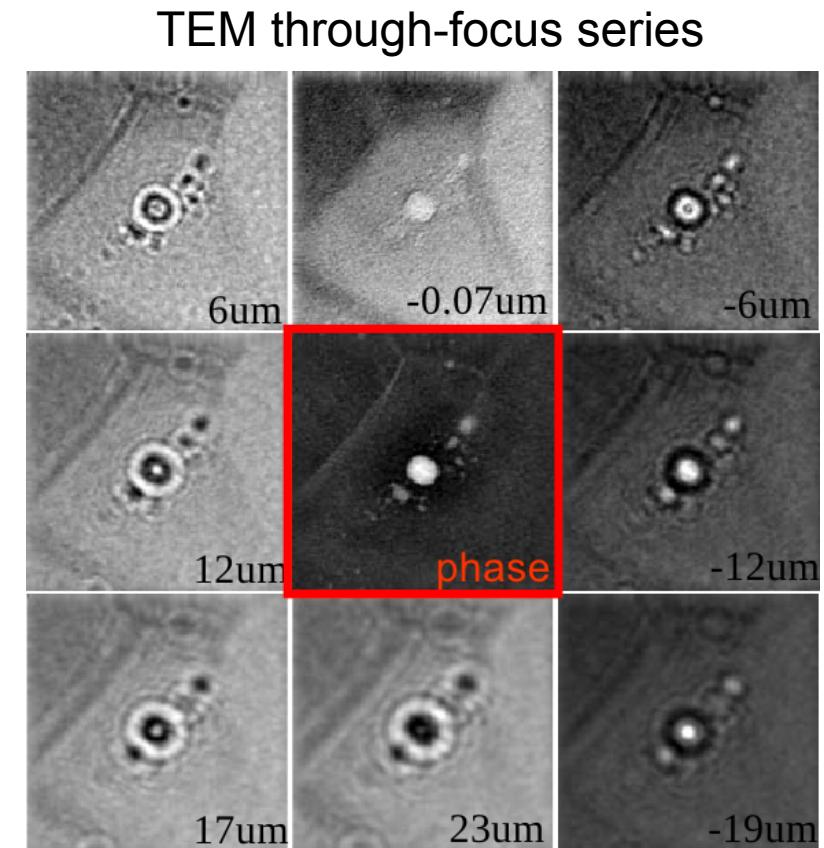
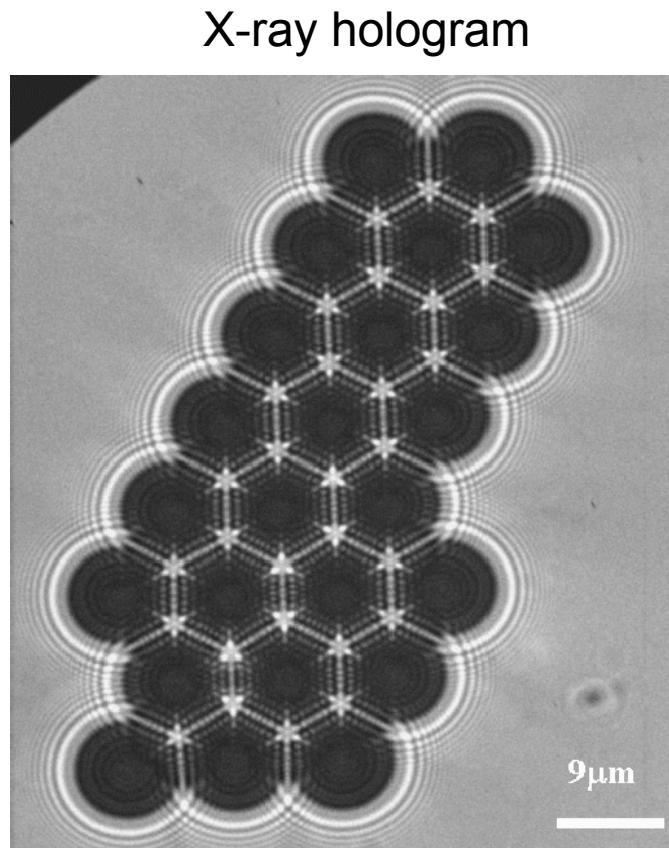
$c$ : speed of light

constant  $n \rightarrow$  plane wave solution  $\psi = \psi_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$

$k^2 = n^2 \frac{\omega^2}{c^2}$  "dispersion relation"

# Propagation modeling

- Useful to:
  - better understand optical systems
  - understand diffraction, holography, phase contrast, interferometry, ...



sources: Mayo et al. Opt. Express (2003)  
<http://www.christophkoch.com/Vorlesung/>

# The physics of propagation

In free space ( $n=1$ ) General solution

$$\psi(\vec{r}, t) = \sum_{\omega} \sum_{\vec{k}} A_{\omega\vec{k}} e^{i(\vec{k} \cdot \vec{r} - \omega t)}$$
$$\hookrightarrow |\vec{k}|^2 = \frac{\omega^2}{c^2}$$

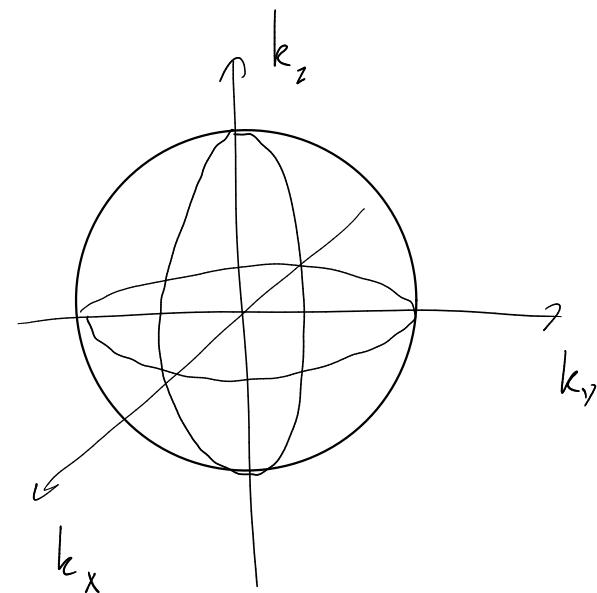
$$|\vec{k}| = \frac{2\pi}{\lambda}$$
$$\text{"u" = } \frac{1}{\rho}$$

Commonly, fix  $\omega$  and solve monochromatic case

$$\rightarrow \psi(\vec{r}) = \sum_{\vec{k}} A_{\vec{k}} e^{i\vec{k} \cdot \vec{r}} \quad \leftarrow \text{is this a Fourier transform?}$$
$$\hookrightarrow |\vec{k}| = \frac{\omega}{c}$$

$$k_x^2 + k_y^2 + k_z^2 = \frac{\omega^2}{c^2}$$

"Ewald" sphere



# The physics of propagation

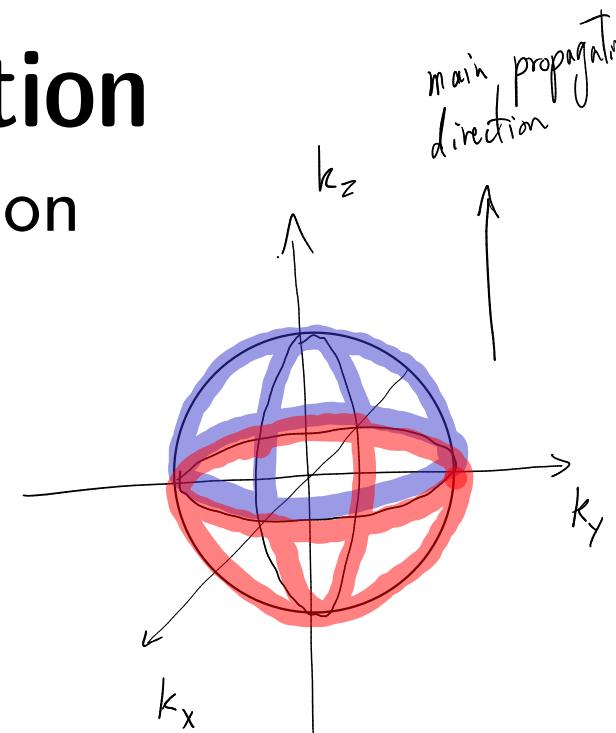
"Angular spectrum" representation

$$\frac{\omega^2}{c^2} = k^2 = k_z^2 + k_x^2 + k_y^2$$

$$k_z = \pm \sqrt{k^2 - k_x^2 - k_y^2}$$

$$\psi(\vec{r}) = \sum_{k_x k_y} A_{k_x k_y} e^{i(k_x x + k_y y + \sqrt{k^2 - k_x^2 - k_y^2} z)}$$

$$+ A_{k_x k_y}^* e^{i(k_x x + k_y y - \sqrt{k^2 - k_x^2 - k_y^2} z)}$$



← forward propagation

$$\psi(\vec{r}_2; z) = \sum_{\vec{k}_2} A_{\vec{k}_2} \exp(i \vec{k}_2 \cdot \vec{r}_2) \exp(i \sqrt{k^2 - k_2^2} z)$$

↑ 2D Fourier transform

# Forward propagation

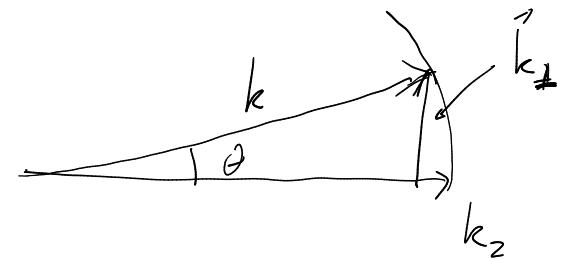
Angular spectrum  
 $k_x = "k \sin \theta"$

$$z=0: \psi(\vec{r}_\perp; z=0) = \sum_{\vec{k}_\perp} A_{\vec{k}_\perp} \exp(i\vec{k}_\perp \cdot \vec{r}_\perp)$$

$$\Rightarrow A_{\vec{k}_\perp} = \mathcal{T} \{ \psi(\vec{r}_\perp; z=0) \}$$

Oftentimes:  $|\vec{k}_\perp| \ll k$  (small angle diffraction)

$$\sqrt{k^2 - k_\perp^2} \approx k \sqrt{1 - \frac{k_\perp^2}{k^2}} \simeq k \left( 1 - \frac{k_\perp^2}{2k^2} \right)$$



*"paraxial approximation"*

$$= k - \frac{k_\perp^2}{2k}$$

$$\exp(i\sqrt{k^2 - k_\perp^2} z) \simeq \exp(ikz) \exp\left(-\frac{izk_\perp^2}{2k}\right)$$

*"Fresnel propagator"*

*parabolic approximation  
of a sphere*

# Forward propagation

$$\psi(r_1; z) = \mathcal{F}^{-1} \left\{ \mathcal{F} \left\{ \psi(r_1; z=0) \right\} \exp \left( -2\pi i \lambda z^{\frac{u^2}{2}} \right) \right\}$$

The trick for numerical implementations:

$$F.T. \quad e^{i2\pi x u}$$

$$D.F.T. \quad e^{i2\pi \frac{n \cdot k}{N}}$$

integers

$$x = n \cdot \Delta x$$

$$u = k \cdot \Delta u$$

$$\Delta x \Delta u = \frac{1}{N}$$

e.g.  $\Delta x, N$  are known

$$\hookrightarrow \Delta u = \frac{1}{\Delta x N}$$

sampling in real  
and Fourier space.

$$\exp(-\pi i \lambda z u^2) \rightarrow \exp(-\pi i \lambda z \cdot k^2 \frac{1}{\Delta x^2 N^2})$$

$$\exp(-\pi i \frac{\lambda}{\Delta x} \frac{z}{\Delta x} \left(\frac{k}{N}\right)^2)$$

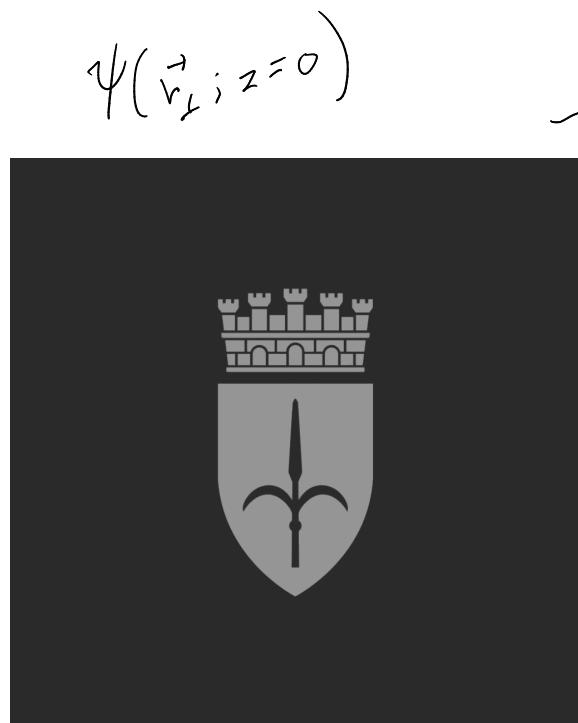
$\frac{k}{N}$  output of

not  $\frac{2\pi}{\lambda}$  here!

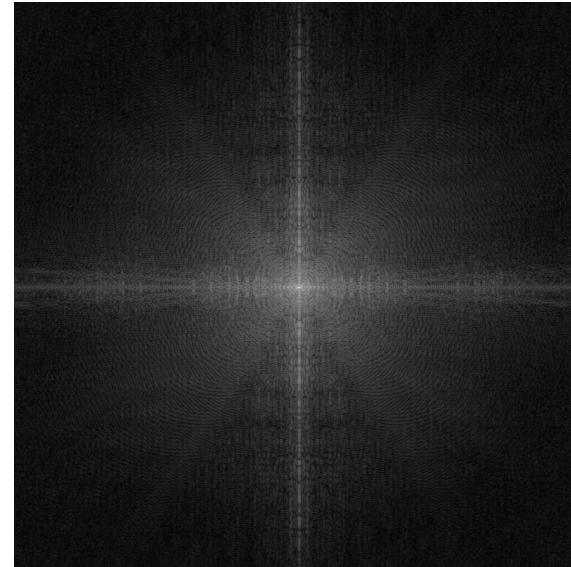
numpy.fft, fftfreq

# Forward propagation

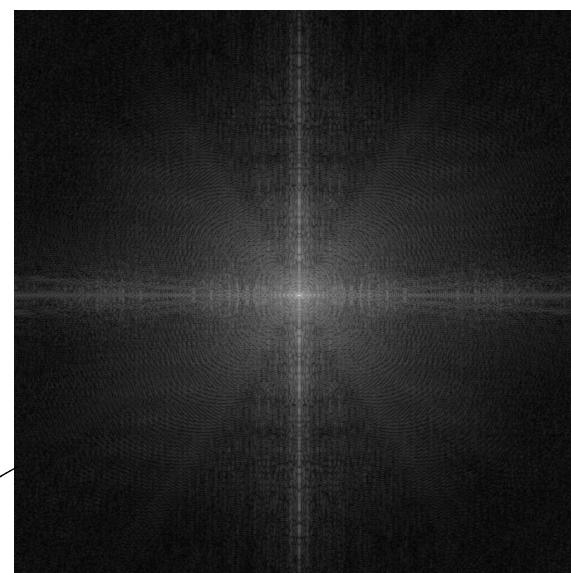
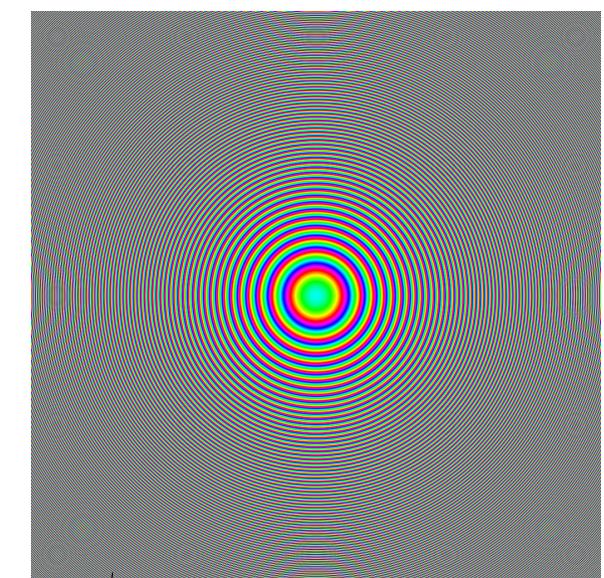
A numerical recipe



$$\mathcal{F}$$



$$\times \exp\left(\frac{-izk_1^c}{2h}\right)$$



# Near field, far field

$$\psi(\vec{r}_+; z) = \mathcal{F}^{-1} \left\{ \mathcal{F} \left\{ \psi(\vec{r}_+; z=0) \right\} \exp \left( - \frac{i z k_{\perp}^2}{2k_R} \right) \right\} \underbrace{\frac{2\pi}{\lambda}}$$

$4\pi^2 \vec{u}^2$

$$\downarrow \vec{k}_{\perp}^2$$

$$\vec{k}_1 = \vec{u} \cdot 2\pi$$

$(2\pi k u)$

$$e^{i k x}$$

$$\psi(\vec{r}_+; z) = \mathcal{F}^{-1} \left\{ \mathcal{F} \left\{ \psi(\vec{r}_+; z=0) \right\} \exp \left( - \pi i \lambda z \vec{u}^2 \right) \right\}$$

$\text{"}\mathcal{F}^{-1} \{ F \cdot G \} \text{"} = f * g$

notation

$$(\vec{r}_+ \rightarrow \vec{r}) = P_z(\vec{r}_+) * \psi(\vec{r}_+; z=0)$$

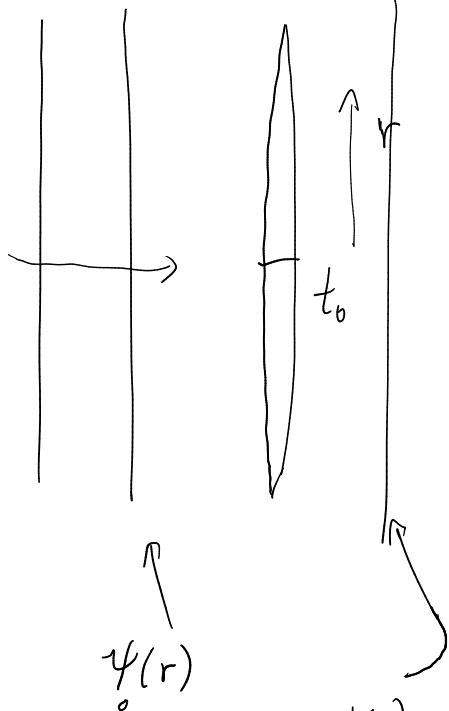
$$\mathcal{F}^{-1} \left\{ \exp \left( - \pi i \lambda z \vec{u}^2 \right) \right\}$$

$$\psi(\vec{r}, z) = - \frac{i 2\pi}{\lambda z} \int d^2 r' \psi(r', z=0) \underbrace{\exp \left( \frac{i k (r-r')^2}{2z} \right)}_1$$



"Fresnel - Huygens integral"

# Back focal plane of a lens



$$t(r) = t_0 - \alpha r^2 \quad (\text{model for thin lens thickness profile})$$

Passed the lens:

$$\phi(r) = \frac{2\pi}{\lambda} (n-1) t(r)$$

$$\frac{1}{2f} = (n-1)\alpha$$

$$= k(n-1)t_0 - k(n-1)\alpha r^2$$

$$\psi(r; z) = \frac{-ik}{z} \int d^2 r' \underbrace{\psi_0 e^{-ik(n-1)\alpha r'^2}}_{\text{exit wave}} e^{\frac{ik(\vec{r} - \vec{r}')^2}{2z}}$$

$$\psi(r) = \psi_0 e^{i\phi(r)}$$

(A lens acts as a Fourier transform operator)

$$= -\frac{ik}{z} \int d^2 r' \psi_0 \exp\left(ik\left[-\frac{1}{2f} r'^2 + \frac{r'}{2z} + \frac{r'^2 - \vec{r}\cdot\vec{r}'}{2z}\right]\right)$$

$$= -\frac{ik}{z} e^{\frac{ikr^2}{2z}} \int d^2 r' \psi_0 \underbrace{\exp\left(\frac{ik\vec{r}\cdot\vec{r}'}{z}\right)}_{\text{"u" }} \exp\left(\frac{ikr'^2}{2} \left(\frac{1}{z} - \frac{1}{f}\right)\right)$$

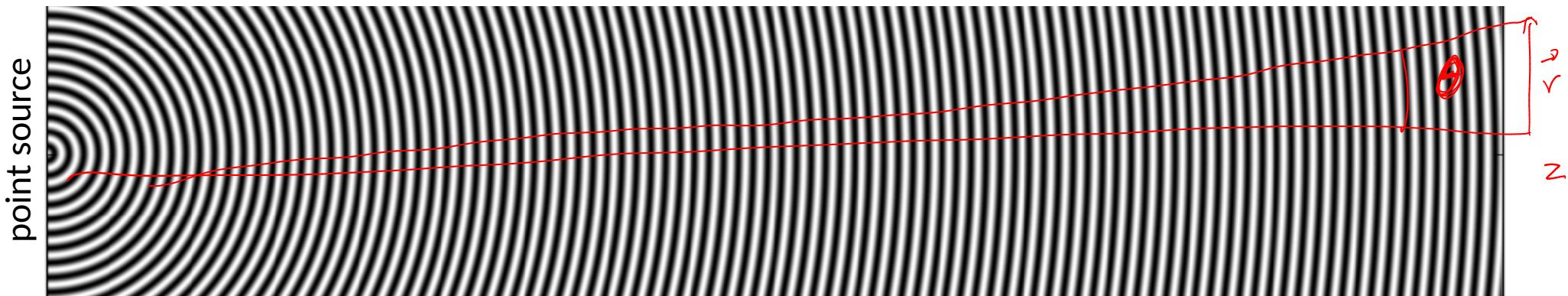
$$\psi(r; z=f) = \frac{ik}{z} e^{\frac{ikr^2}{2z}} \underbrace{\left\{ \psi_0(r) \right\}}_{\text{u}} \left( \vec{u} = \frac{\vec{r}}{z} \right)$$

# Plane waves, point sources

Far-field propagation (Fraunhofer regime):

$$\psi(r; z \rightarrow \infty) = \frac{ik}{2} e^{\frac{ikr^2}{2z}} \tilde{\mathcal{F}}\{\psi_0(r)\} \left( \vec{u} = \frac{\vec{k}r}{z} \right)$$

" $z \sin \theta$ "



circular waves  
evanescent waves  
contact region

parabolic waves  
near field  
Fresnel region

*carrier wave*

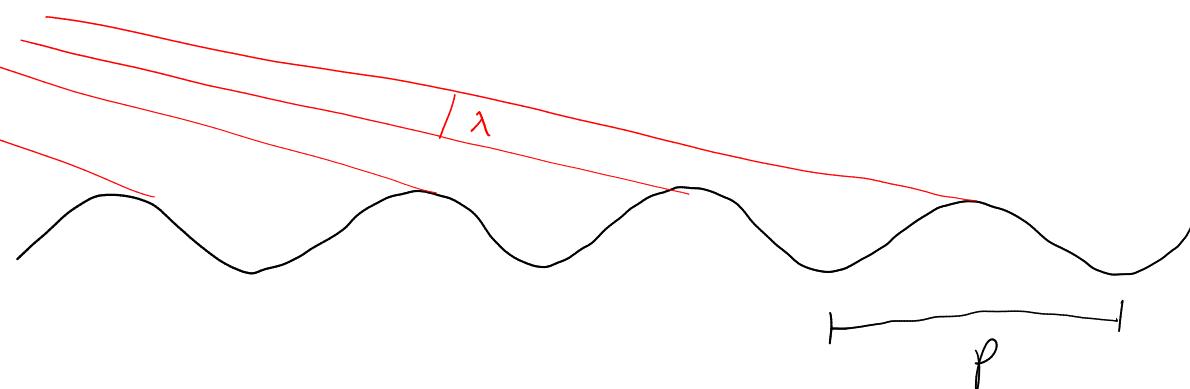
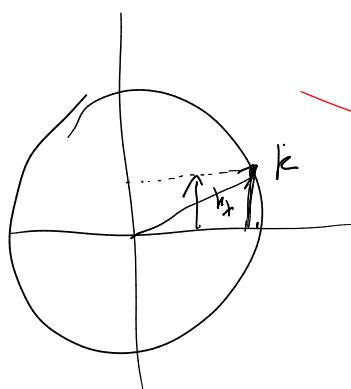
$\lambda$

$H$

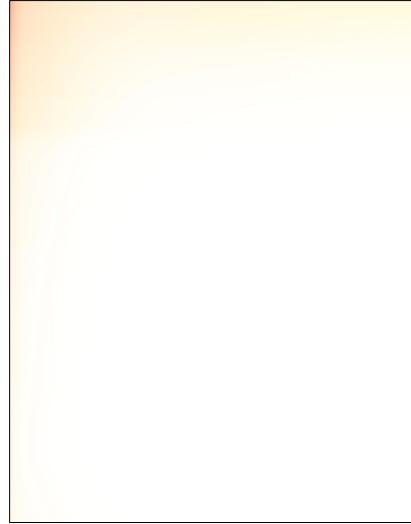
plane waves  
far field  
Fraunhofer region

oscillation of given

spatial frequency  
in initial image



# Why optical elements?



with objective lens

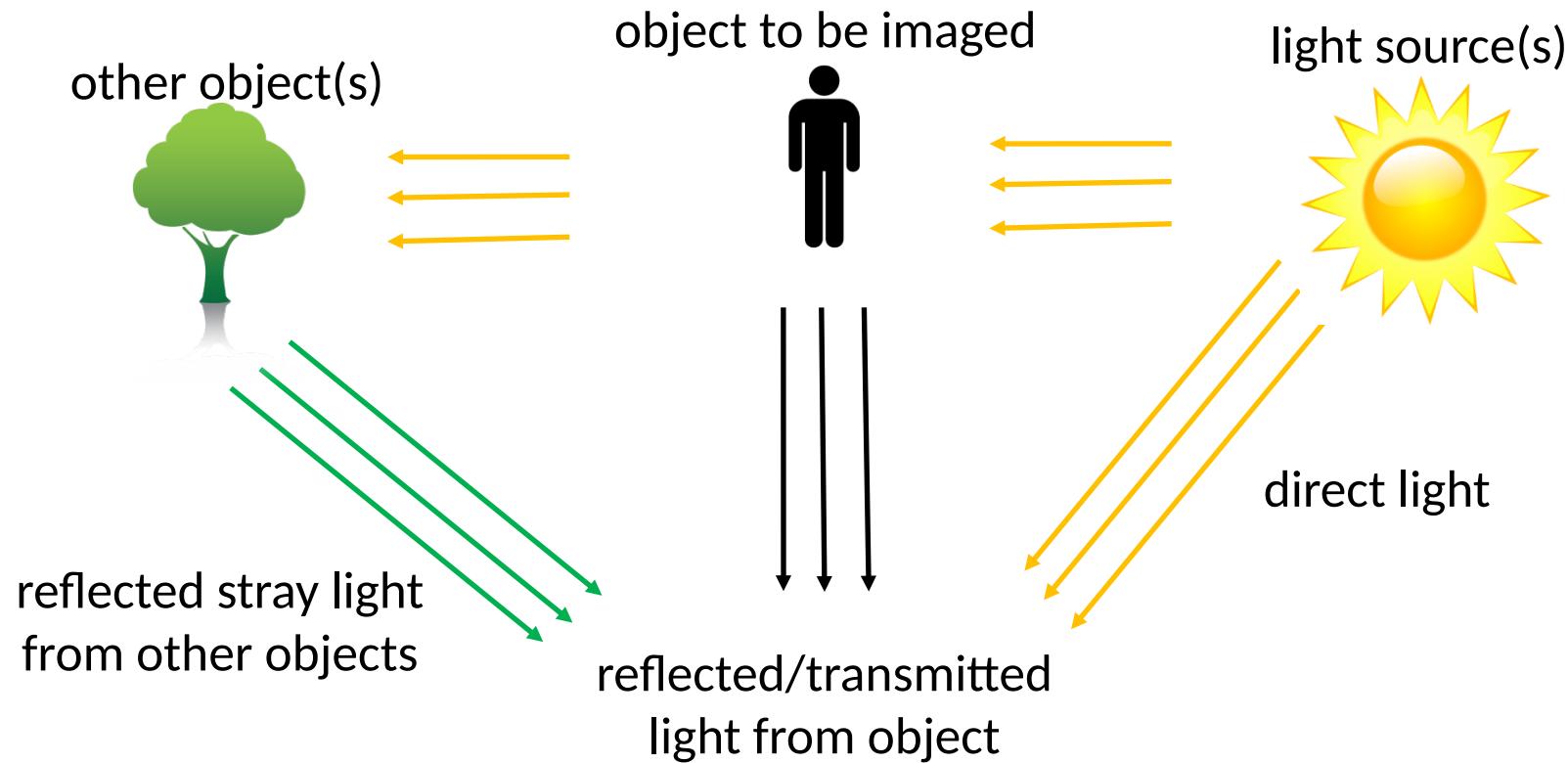


without objective lens



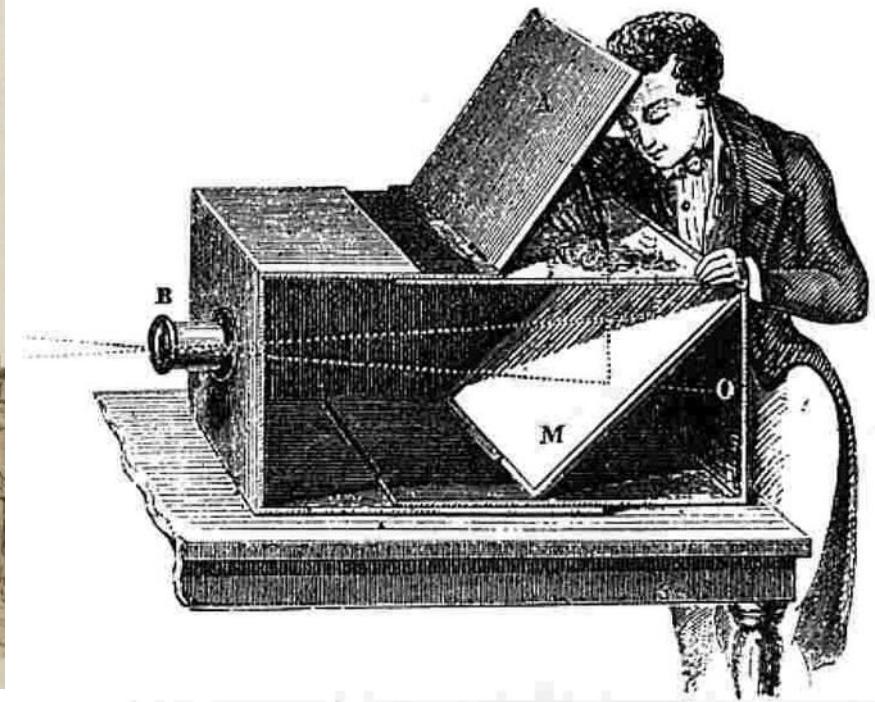
# Why optical elements?

- Information from many sources overlaps in detector plane
- Need models to understand image forming systems



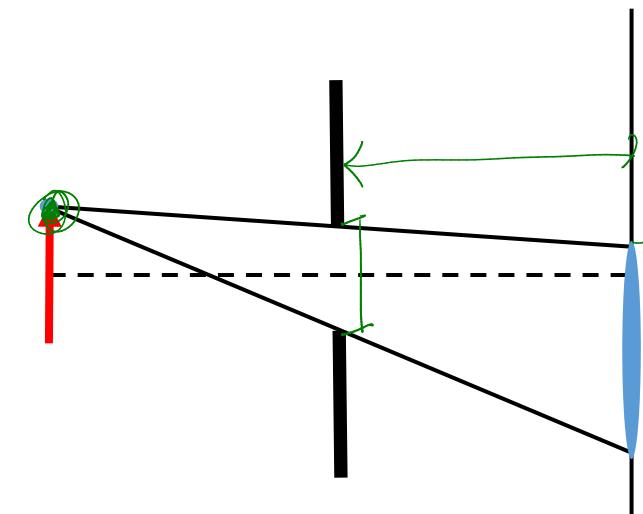
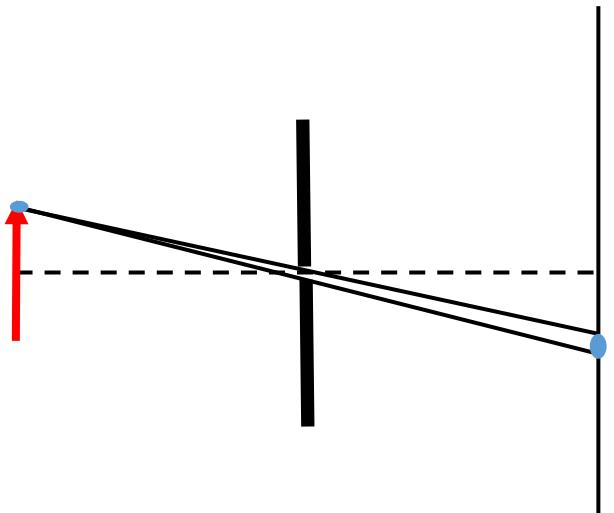
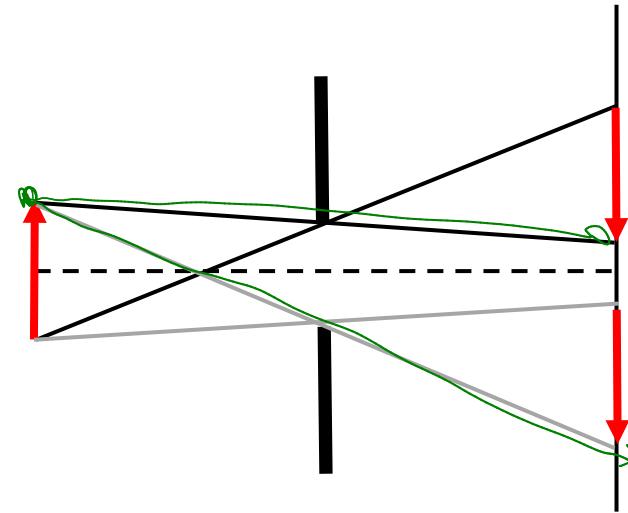
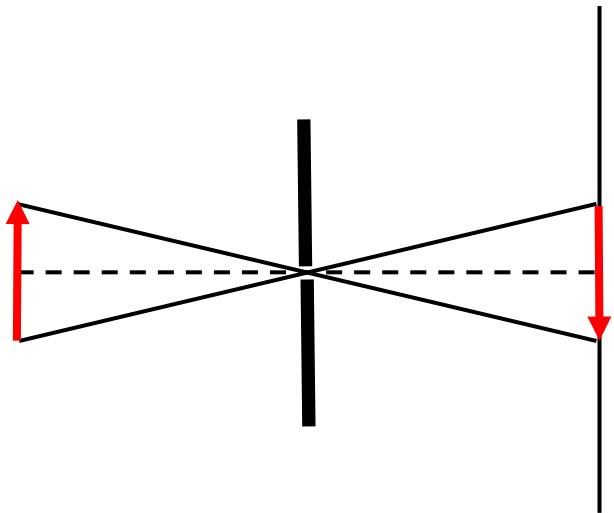
# Pinhole camera model

camera obscura



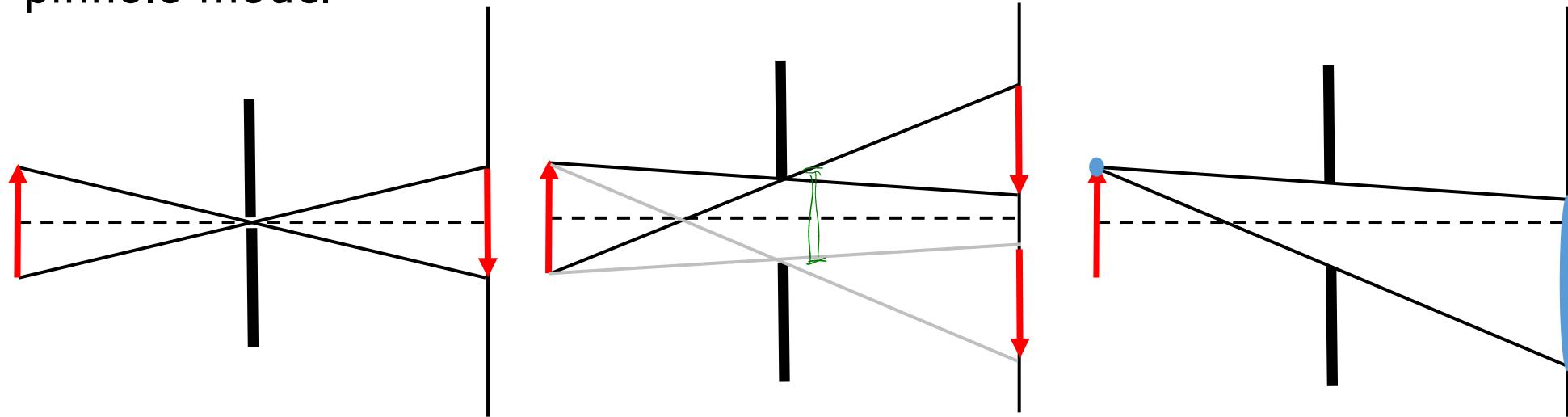
# Pinhole camera model

PSF determined by aperture width

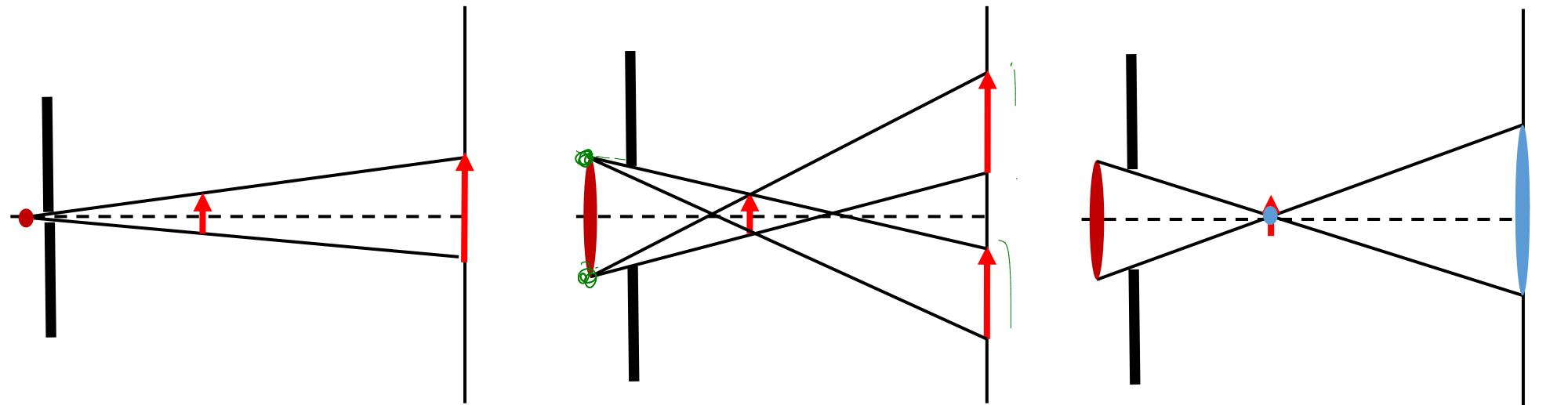


# Projection model

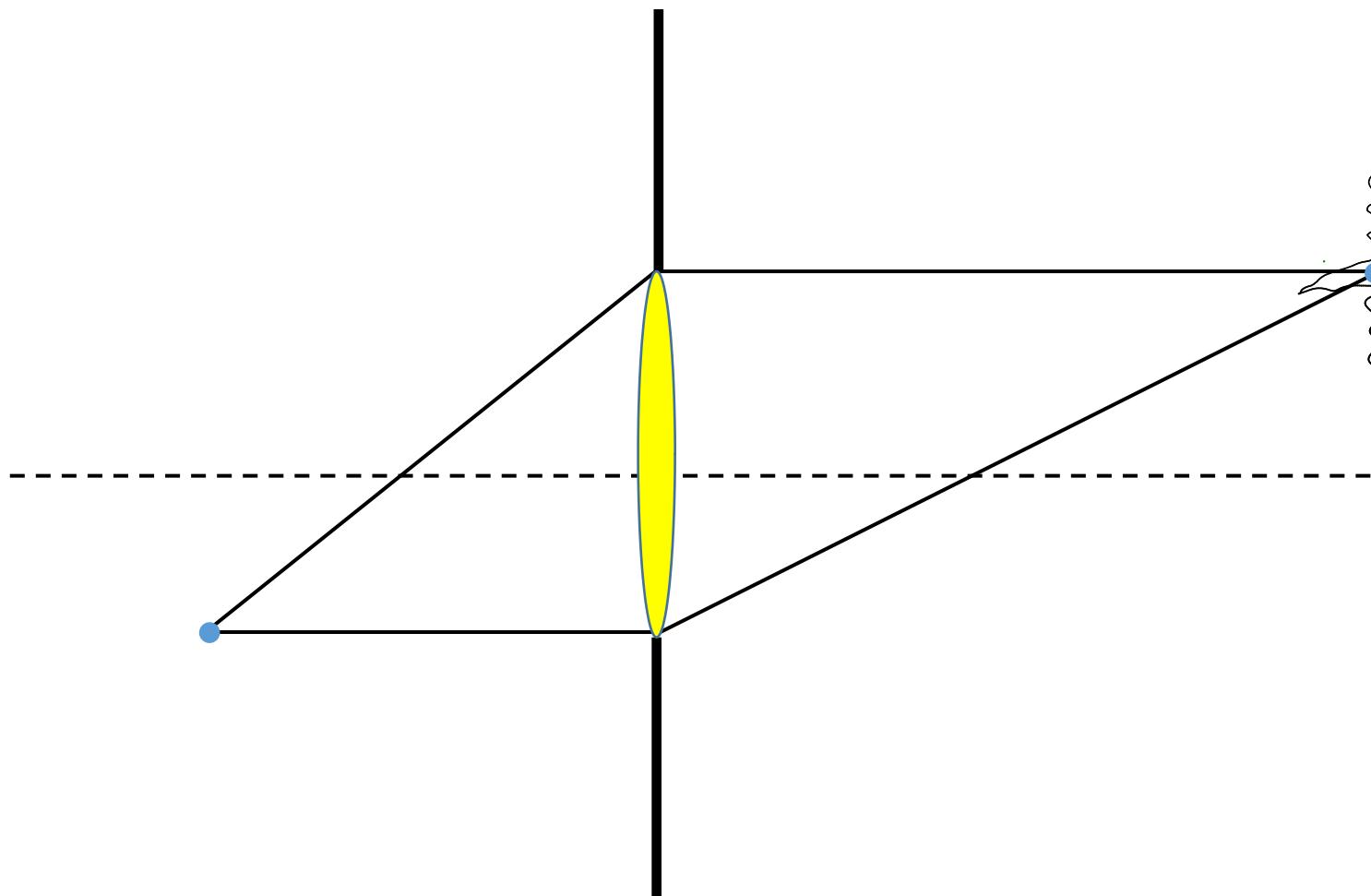
pinhole model



projection model



# Lens camera model

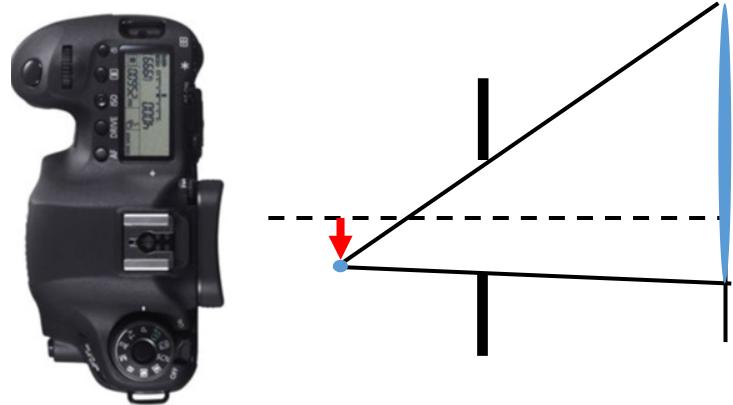


PSF:  
diffraction

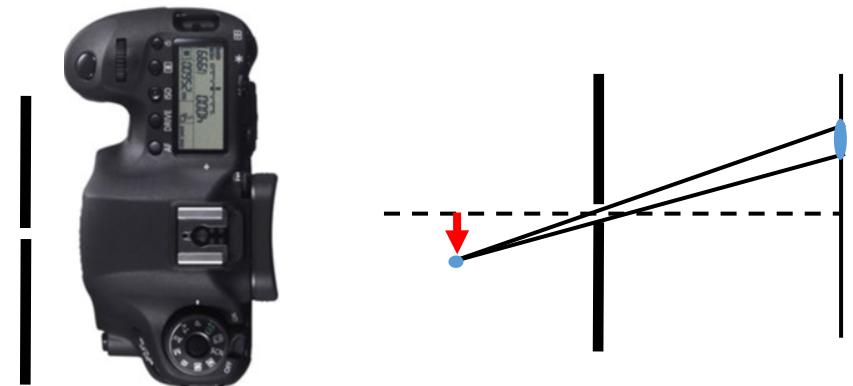
PSF  
related to  
F.T. of  
aperture

# Lens camera model

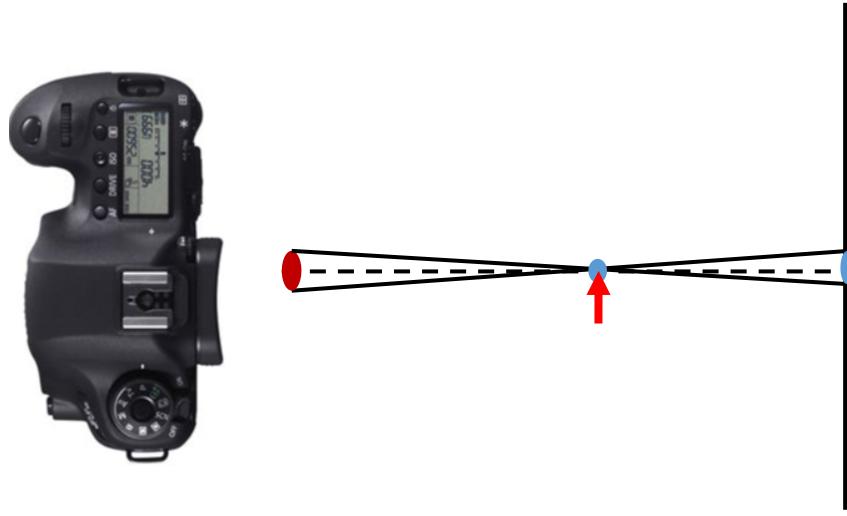
lensless model



pinhole camera model



projection model

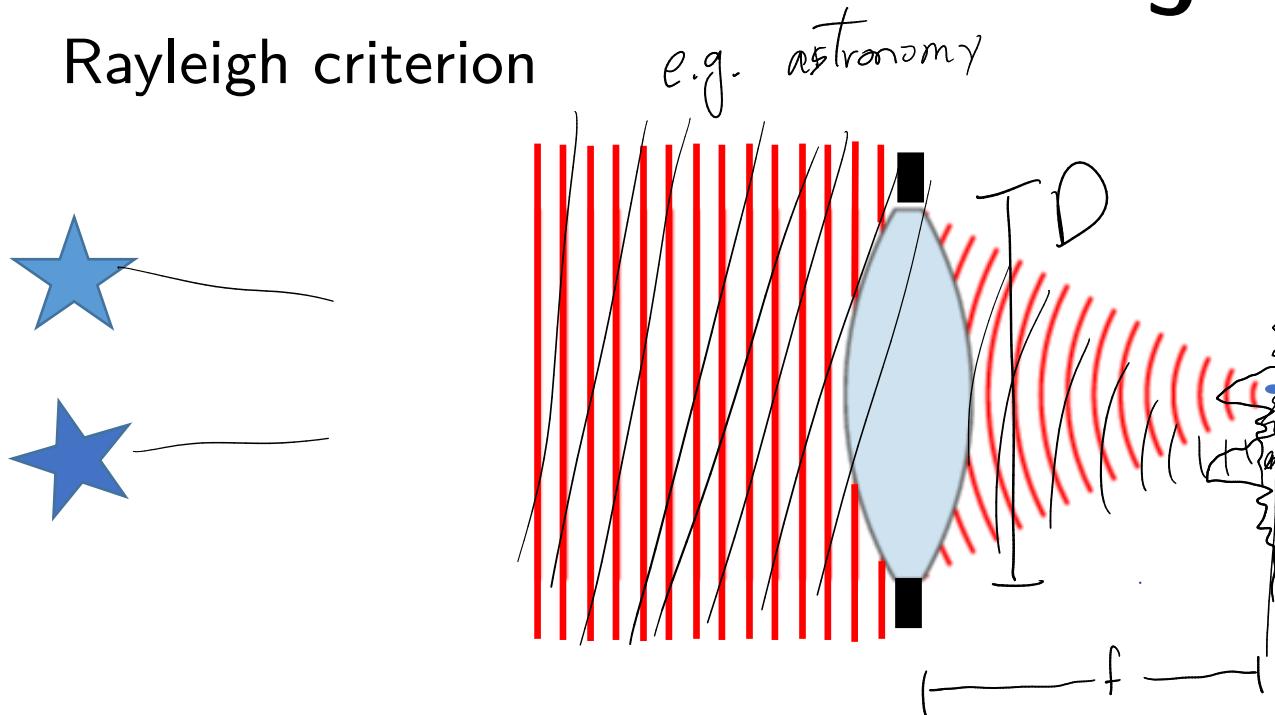


lens camera model

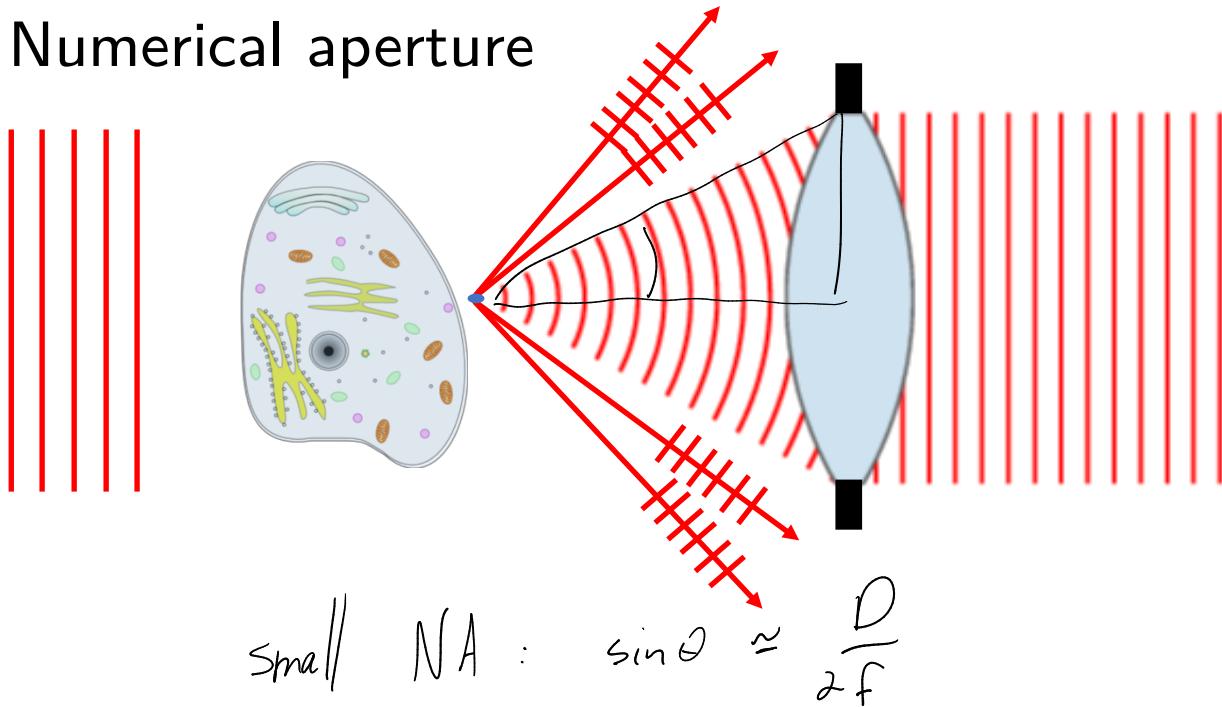


# Diffraction-limited imaging systems

- Rayleigh criterion



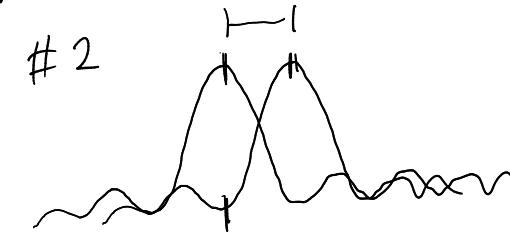
- Numerical aperture



PSF: Airy "disc"

Rayleigh criterion :

two points are resolvable  
if maximum of #1  
aligned with 1<sup>st</sup> minimum  
of #2



$$d_{\min} = \frac{f \cdot \lambda}{D} \cdot 1.22$$

NA : numerical aperture

$$NA = n \cdot \sin \theta$$

$$d_{\min} = 1.22 \frac{\lambda}{2NA}$$

# Scanning systems

## Transmission

- Scanning Transmission Electron Microscopy
- Scanning Transmission X-ray Microscopy
- ...

## Indirect (reflection, scattering, fluorescence, ...)

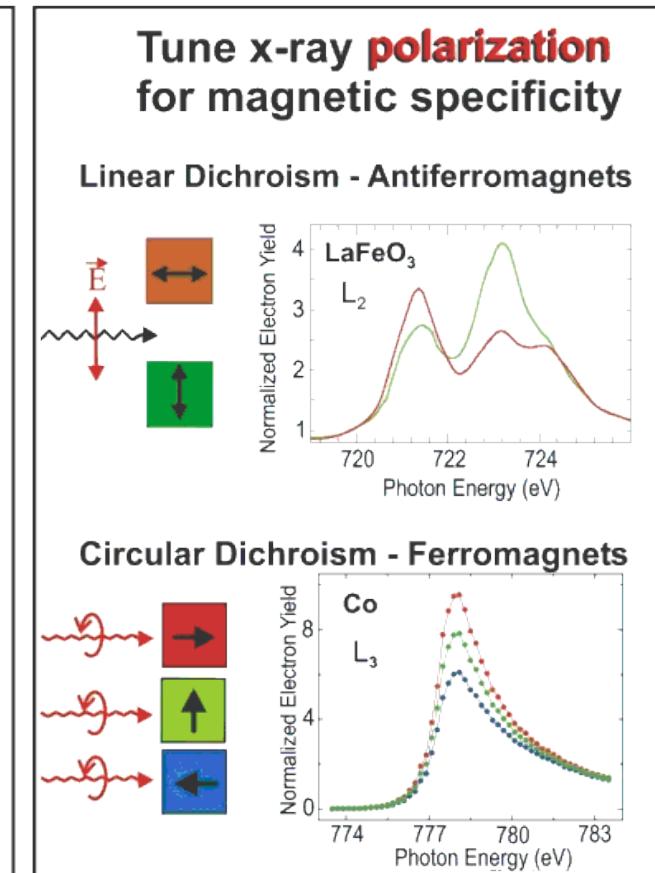
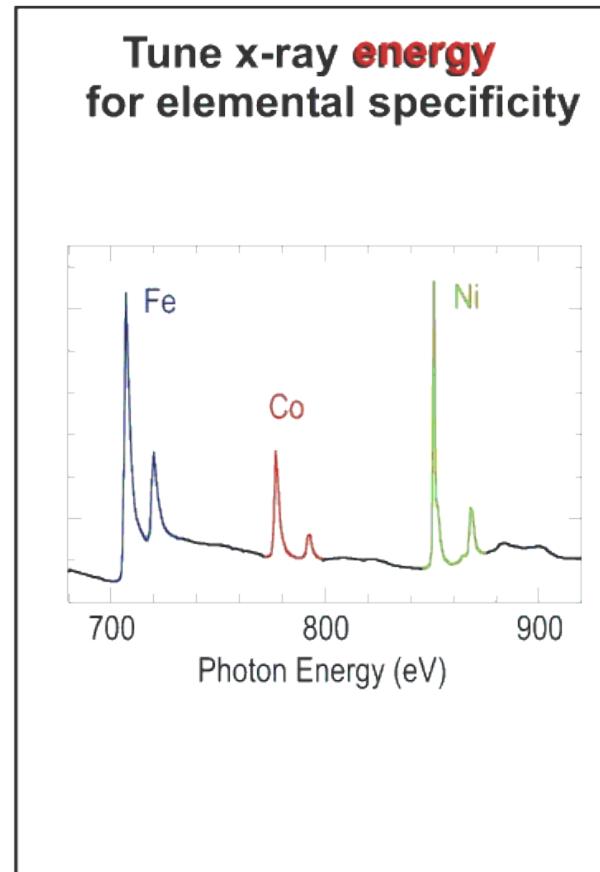
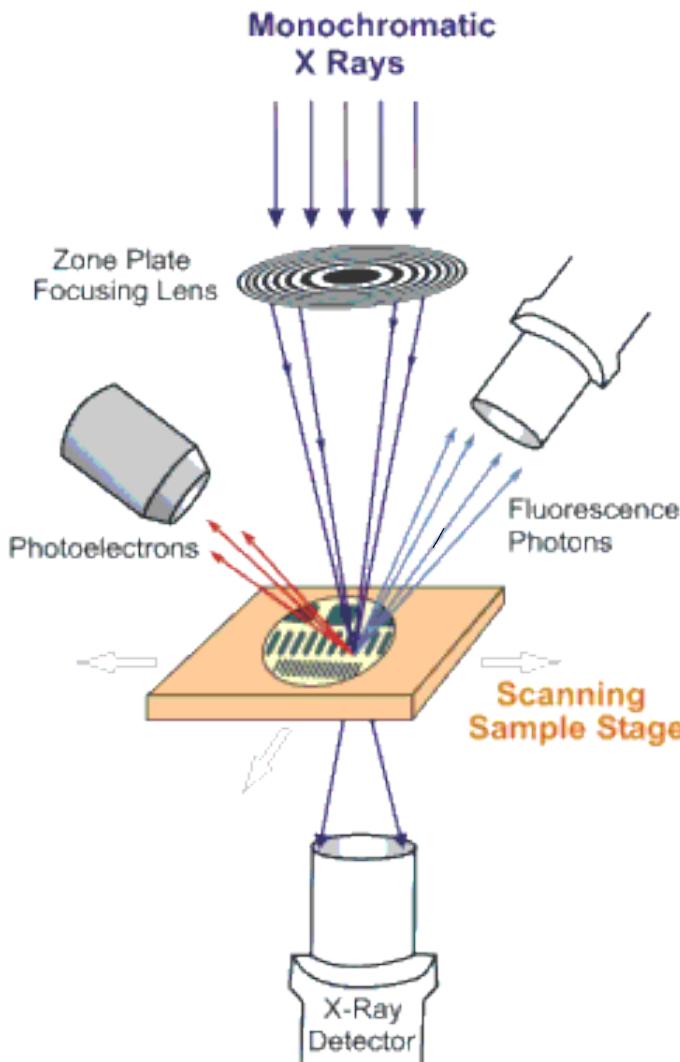
- Laser Scanning Confocal Micropsopy
- Scanning Electron Microscopy
- X-ray Fluorescence Microscopy
- PhotoEmission Electron Microscopy
- ...

## Physical probe

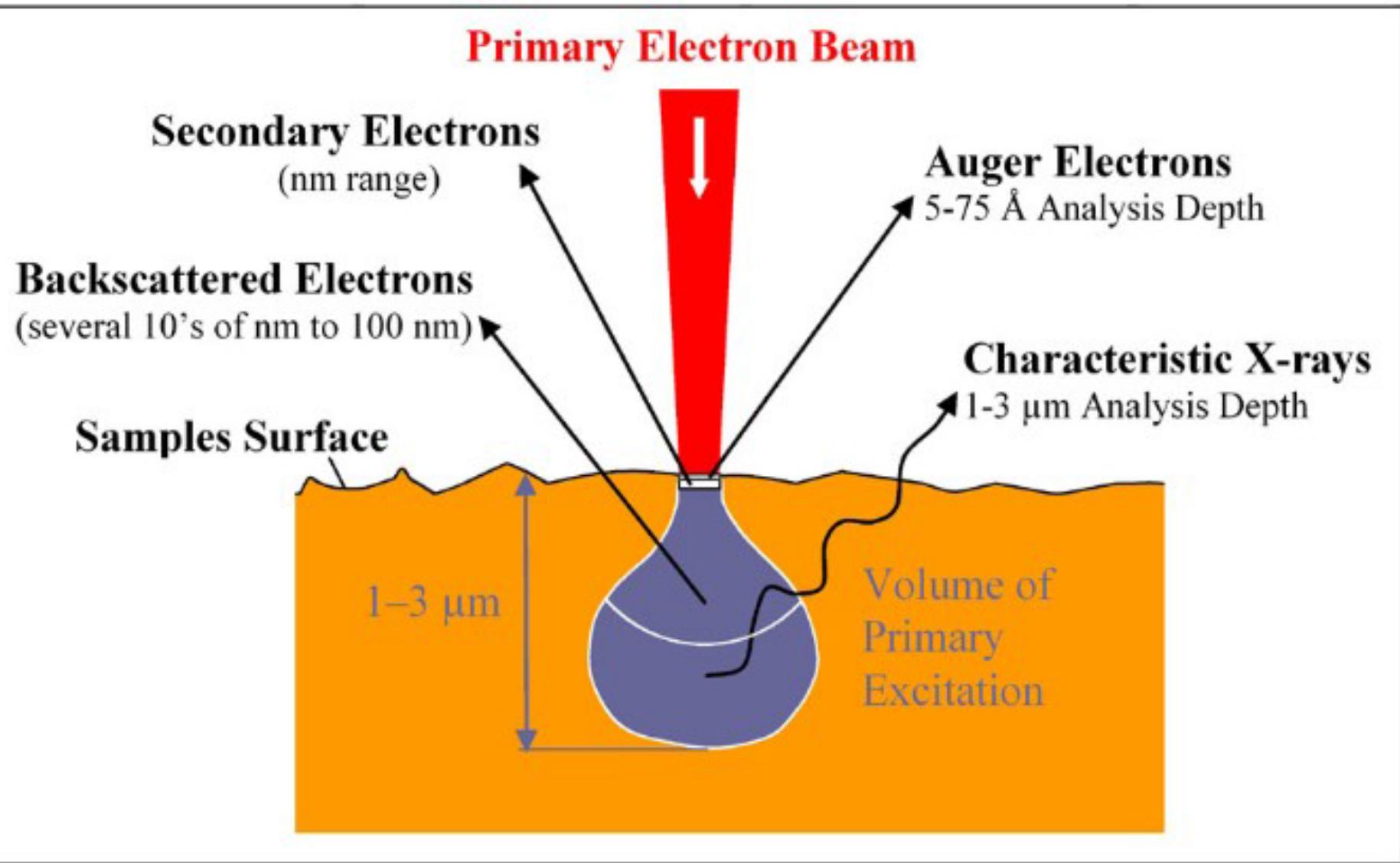
- Atomic Force Microscopy
- Scanning Tunneling Microscopy
- ...

# Scanning transmission X-ray microscopy

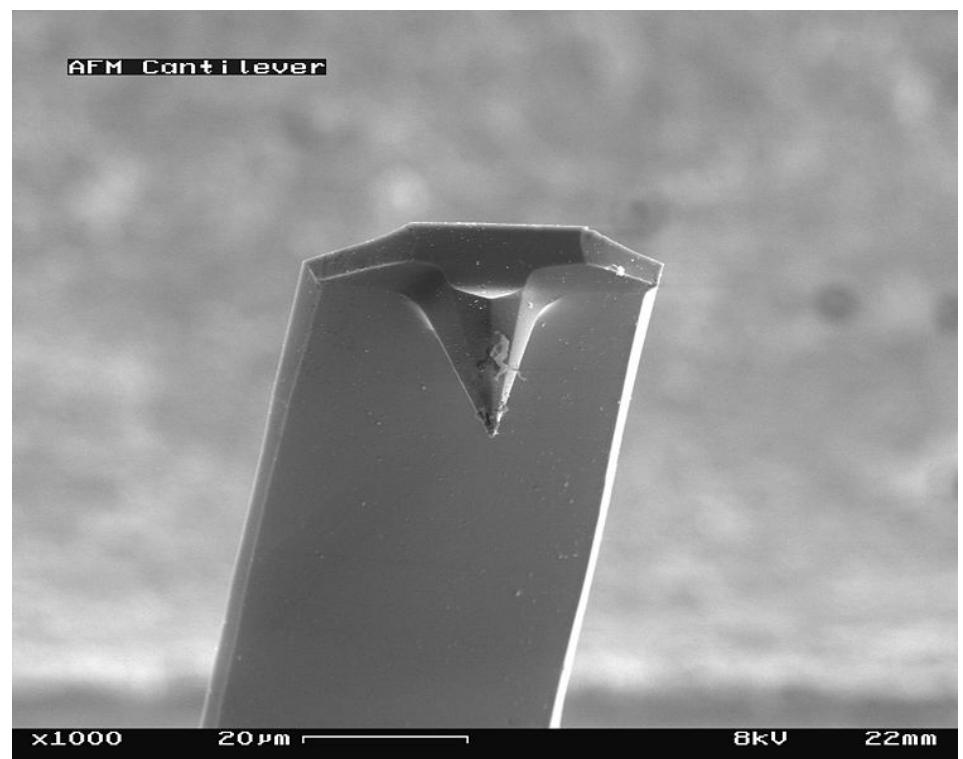
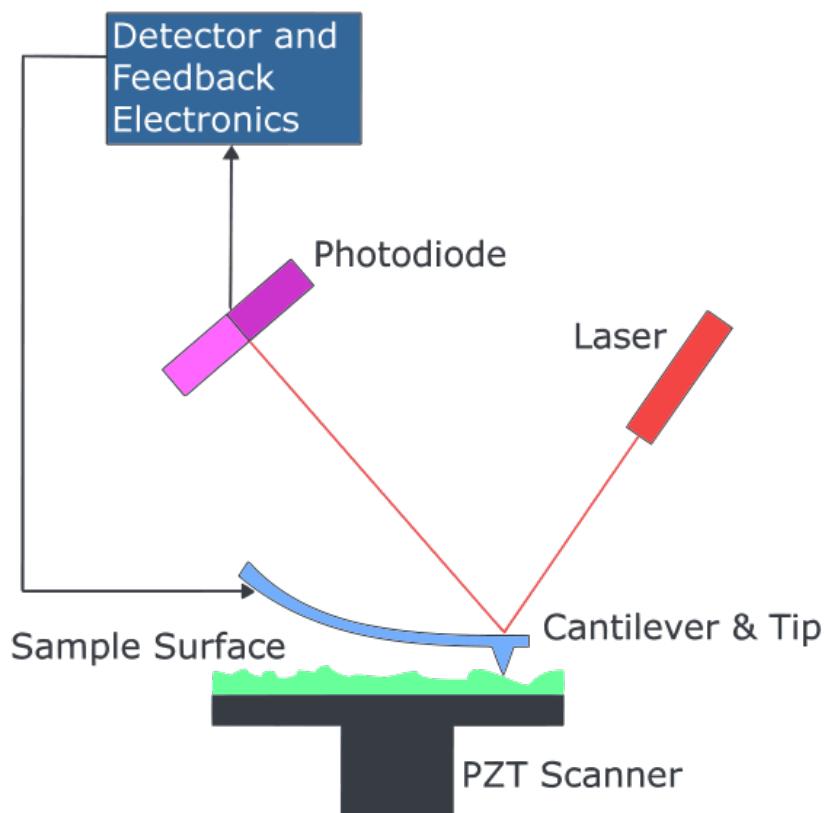
Scanning Transmission X-ray Microscopy  
STXM



# Scanning electron microscopy



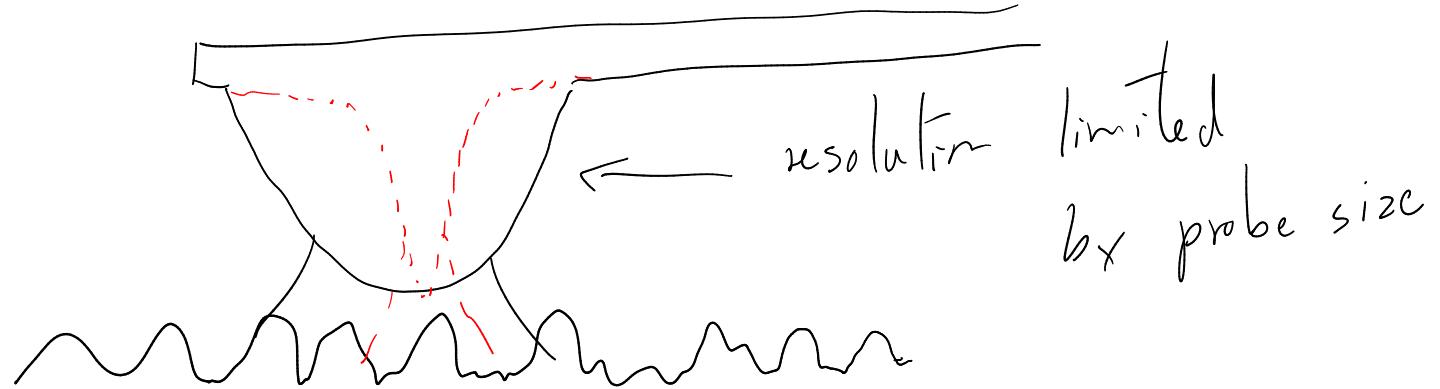
# Atomic force microscopy



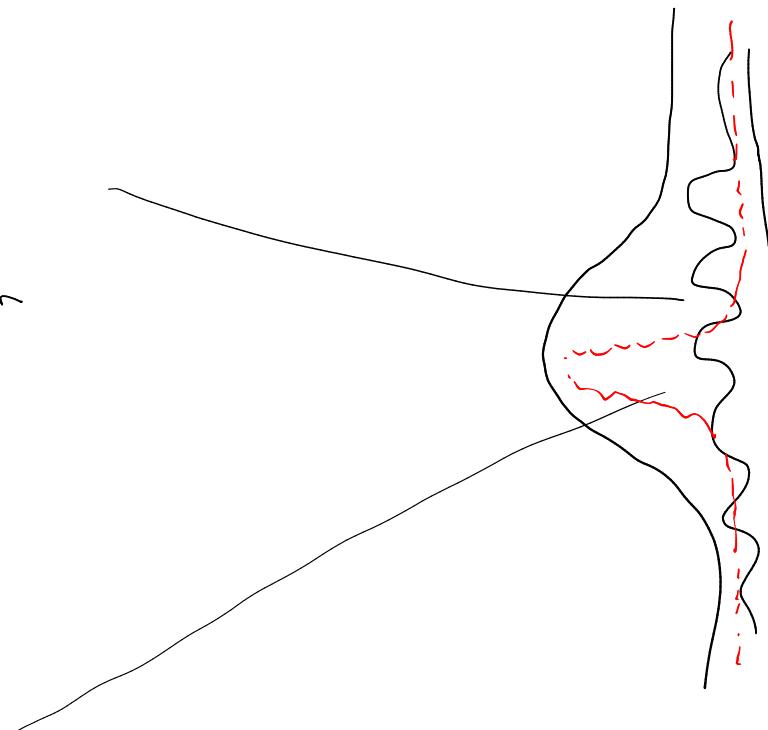
# Resolution in scanning systems

Resolution mainly limited by probe size

e.g. AFM



e.g. transmission



# Scanning vs. full field systems

Transmission probe: the reciprocity theorem

