

Critical bifurcation of shallow microtidal landforms in tidal flats and salt marshes

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Shallow tidal basins are characterized by extensive tidal flats and salt marshes that lie within specific ranges of elevation, whereas intermediate elevations are less frequent in intertidal landscapes. Here we show that this bimodal distribution of elevations stems from the characteristics of wave-induced sediment resuspension and, in particular, from the reduction of maximum wave height caused by dissipative processes in shallow waters. The conceptual model presented herein is applied to the Venice Lagoon, Italy, and demonstrates that areas at intermediate elevations are inherently unstable and tend to become either tidal flats or salt marshes.

intertidal landforms

The distribution of elevations in shallow tidal basins such as the Venice Lagoon in Italy (Fig 1, tidal range of 0.7 m) shows that tidal flats have differences in elevation of few tens of centimeters, with an average elevation between -0.50 and -1.00 m above mean sea level (MSL), whereas salt marshes lie at an average elevation higher than $+0.20$ m, with some variability dictated by local sedimentological and ecological conditions (1–4). Few areas are located at intermediate elevations (i.e., between -0.50 and $+0.20$ m), suggesting that the processes responsible for sediment deposition and erosion produce either tidal flats or marshes but no landforms located at intermediate elevations. In the relatively pristine northern part of the Venice Lagoon, the most frequent bottom elevation is around -0.50 m (Fig. 2), similar to natural conditions in 1901 in the Southern Lagoon (Fig. 1A). During the last century, anthropogenic causes produced consistent bottom erosion in the Southern Lagoon, leading to a median elevation of approximately -1.00 m above MSL (Figs. 1B and 2). Nevertheless, all three distributions of elevations show a relatively low frequency of elevations between 0 and -0.5 m.

Typical conceptual and numerical models of salt-marsh formation envision a gradual transformation of sand flats and mudflats in response to sediment buildup and plant colonization (5–7). However, the evidence points to abrupt transitions to one of two distinct stable outcomes. Salt marshes emerge from tidal flats in locations where sedimentation is enhanced by lower tidal velocities, higher sediment concentrations, or the sheltering effects of splits and barrier islands (1, 8). Alternatively, in areas with consistent sediment resuspension caused by a combination of tidal fluxes and wind waves, tidal flats are dominant. In tidal flats, sediment deposition is balanced by erosion, and the bottom elevation is constantly maintained below MSL (9). Sediment resuspension by wind waves is decisive, because tidal fluxes alone are unable to produce the bottom shear stresses necessary to mobilize tidal-flat sediments (10).

On the basis of a simplified model for wave generation in shallow water (10), we developed a conceptual model to study the distribution of bottom shear stress as a function of elevation. The results are used to explain the bimodal distribution of bathymetry in the Venice Lagoon.

Wind Waves in Shallow Water

Wind waves are created by the transfer of energy from the wind to the water surface. Starting from a flat water surface, wind

stresses generate waves that increase in height until the energy dissipation caused by whitecapping, depth-induced breaking, and bottom friction limit the growth process (10, 11). Equilibrium is reached when the energy generated by the wind action equals the energy dissipated. In this situation, the height of the wave is the maximum possible for the particular bathymetry, meteorological forcing, and fetch length (the distance across which the wind can blow without land obstructions). Thus, wave height is largely controlled by depth and increases in deep waters.

To compute wave height in shallow waters we study the local evolution of the wind-wave energy E , directly related to the wave height by the linear theory. Wind-wave energy is described with an equation for the conservation of wave energy, which, for monochromatic waves, reads (10, 11)

$$\partial E / \partial t + \nabla \cdot \mathbf{c}_g E = S, \quad [1]$$

where \mathbf{c}_g is wave-group celerity and S is a source term. In shallow basins, waves quickly adapt to external forcing (i.e., $\partial E / \partial t$ becomes negligible in a short period). In fact, strong dissipation limits advection, so the wave field is essentially controlled by local energy balance. Moreover, the time required to reach equilibrium is short (10), so we can ignore the transient behavior.

The source term S includes wave growth by wind (S_w) and wave decay by bottom friction (S_{bf}), whitecapping (S_{wc}), and depth-induced breaking (S_b). Therefore, and as a first approximation, the conservation equation can be reduced to

$$S_w = S_{bf} + S_{wc} + S_b. \quad [2]$$

This equation states that equilibrium is reached when the energy generated by the wind action equals the energy dissipation by bottom friction, whitecapping, and breaking. All terms in the equilibrium equation can be expressed as a function of wave energy (10, 11), and the wave height can be calculated with an iterative algorithm. The terms in Eq. 2 are indicated in Table 1 and were derived from widely adopted wave models (11). In our model we implement Eq. 1 with a finite-elements algorithm. To assess the influence of fetch length on wave generation, the advection term in Eq. 1 was retained. The wave height was then calculated along transects with constant bottom elevation, starting from a flat water surface and using Eq. 1 until steady state was reached.

Bottom shear stresses are directly linked to wave height. In our modeling framework, the bottom shear stress (12) is given as

$$\tau_b = 1/2 f_w \rho_w u_m^2 \quad \text{with} \quad u_m = \pi H / [T \sinh(kY)], \quad [3]$$

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Abbreviation: MSL, mean sea level.

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Table 1. Formulation for wave generation and dissipation (11)

Process	Formula	Variable
Wind generation	$S_w = \alpha + \beta \cdot E$ $\alpha(k) = \frac{80\rho_a^2\sigma}{\rho_w^2g^2k^2}c_d^2U^4$ $\beta(k) = 5\frac{\rho_a}{\rho_w}f\left(\frac{U\cos\delta}{c} - 0.90\right)$	<i>k</i> : wave number; $\sigma = 2\pi/T$ (<i>T</i> = wave period); ρ_a : air density; ρ_w : water density; $c_d \cong 0.0012$ drag coefficient; <i>U</i> : the wind speed in m/s; <i>f</i> : wave frequency ($f = 1/T$); δ : angle between wind and wave vector; $c = \sigma/k$ wave celerity
Bottom friction	$S_{bf} = -4c_{bf}\frac{\pi H}{T}\frac{k}{\sin h(kY)\sin h(2kY)}E$	<i>H</i> : significant wave height; <i>Y</i> : water depth; $c_{bf} = 0.015$
White capping	$S_{wc} = -c_{wc}\sigma\left(\frac{\gamma}{\gamma_{PM}}\right)^m E$	γ integral wave-steepness parameter, $(\gamma = E\sigma^4/g^2)$; $\gamma_{PM} = 4.57 \times 10^{-3}$: theoretical value of γ for a Pearson–Moskowitz spectrum; $c_{wc} = 3.33 \times 10^{-5}$
Breaking	$S_b = \frac{2}{T}Q_b\left(\frac{H_{max}}{H}\right)^2 E$	$H_{max} = 0.78 Y$, maximum wave height; Q_b : breaking probability
Wave-induced bottom shear stress	$f_w = 1.39\left[\frac{u_m T}{2\pi(D_{50}/12)}\right]^{-0.52}$	$D_{50} = 20\text{-}\mu\text{m}$ median grain diameter

where *y* is the tidal-flat elevation, *n* is the porosity, and R_D is the average annual deposition rate at that location.

The model assumes a prescribed characteristic, geomorphically dominant wind speed with an average annual duration related to that specific wind condition. Following the procedures outlined in ref. 15, the dominant wind speed is obtained by maximizing the product of wave erosion by the frequency of the related wind conditions. Using 50 years of wind data for the Venice Lagoon, we determine a dominant wind speed of 8 m/s blowing from northeast.

An average annual sedimentation rate that is site-dependent but constant during bottom evolution is also assumed. The tidal flat reaches an equilibrium elevation (i.e., $dy/dt = 0$) when the average annual erosion rate *R* is equal to the average annual deposition rate R_D . From Eq. 5 we obtain the equilibrium condition:

$$\tau_b = \left(\frac{R_D}{A}\right)^{1/\alpha} + \tau_{cr} \quad [6]$$

Thus, the equilibrium depth is the intersection of the shear-stress curve and the horizontal line shown on the right-hand side of Eq. 6 (Fig. 4A).

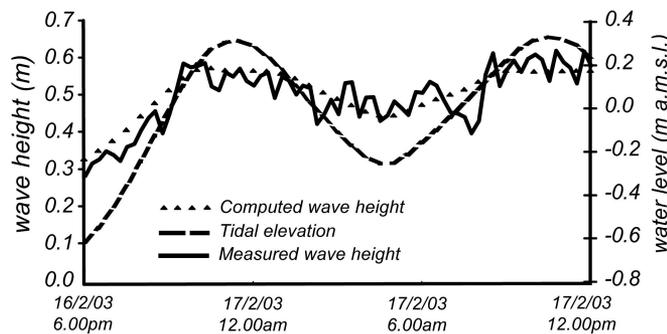


Fig. 3. Tidal and wave elevations (both measured and simulated) in the Venice Lagoon (location indicated in Fig. 1B). The simulated waves were computed by using Eq. 1 with measured wind speeds on February 16–17, 2003. a.m.s.l., above MSL.

If the deposition rate is less than the maximum erosion rate, we have two equilibrium elevations, but only the one on the right is stable. In fact, for elevations between the two equilibrium points, the annual erosion rate is higher than the annual deposition rate (the erosion curve is above the deposition curve) and the tidal flat tends to deepen, whereas for elevations below the equilibrium point on the left and above the equilibrium point on the right, deposition dominates erosion and the tidal flat accretes (horizontal arrows in Fig. 4A). Thus, the point on the right is stable, because a small perturbation in elevation can be easily recovered by the system (a lower elevation decreases erosion, producing sediment accumulation, whereas a higher elevation favors erosion and thus deepening). The equilibrium condition on the left is unstable and persists only if the local deposition rate exactly balances the erosion rate; otherwise, the bottom elevation will evolve toward either a stable tidal flat if the annual deposition is smaller than the equilibrium erosion rate or an emergent salt marsh if the annual deposition rate is higher than the equilibrium erosion rate.

For deposition rates higher than the maximum erosion rate R_{max} , there are not possible equilibrium elevations for tidal flats and the system evolves to salt-marsh elevations (Fig. 4B), whereas for a deposition rate exactly equal to the maximum erosion rate R_{max} , there is only one semistable equilibrium elevation.

The maximum in shear stress represents the boundary between stable and unstable elevations. In fact, the points on the right-hand branch are the equilibrium elevations that a tidal flat can attain as a function of different deposition rates, whereas the left-hand branch of the curve represents all of the unstable equilibrium conditions. The intertidal landscape is then characterized by tidal-flat elevations belonging to the stable branch of the curve, with different elevations depending on local sediment availability, and few areas having elevations higher than the maximum in shear stress representing tidal flats in transition to salt marshes or vice versa.

In intertidal environments it is common to assume a deposition rate that varies as a function of water depth (16, 17), which is particularly true for salt marshes, in which the inundation period and therefore the time available for suspended sediment

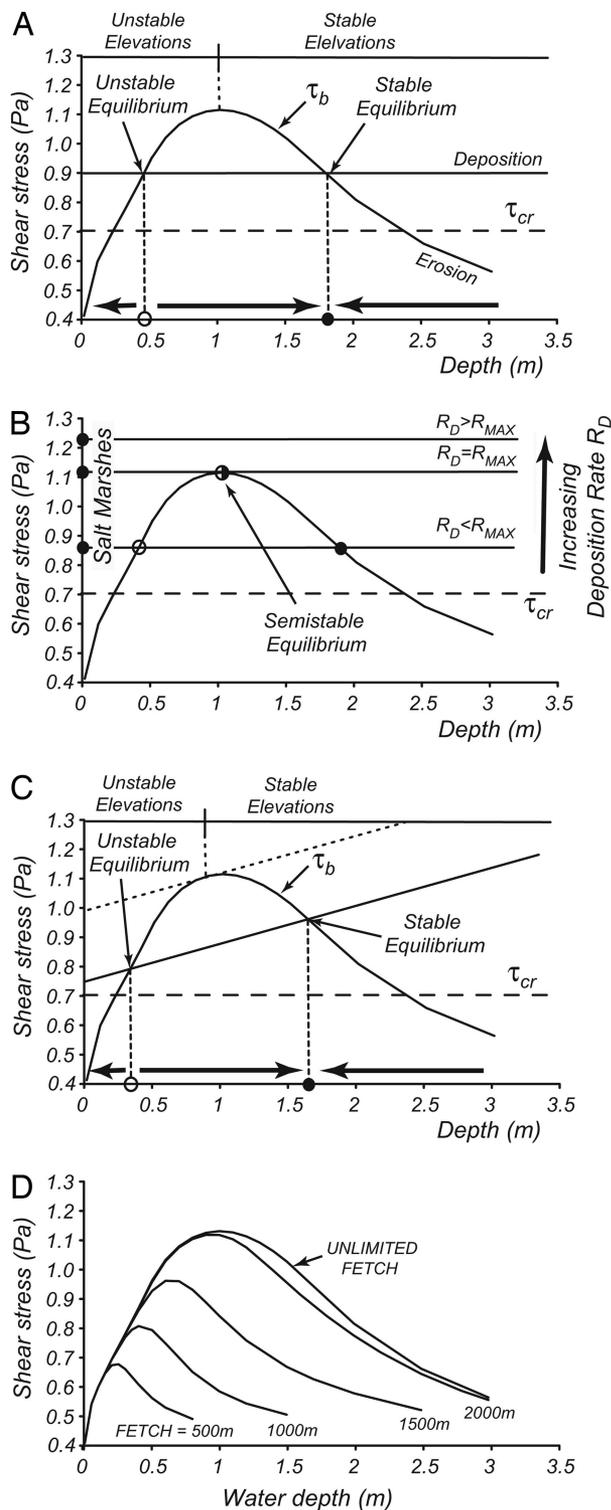


Fig. 4. Tidal flat equilibrium conditions. (A) Distribution of bottom shear stresses produced by wind waves as a function of elevation. The intersections between the shear-stress curve and the horizontal line (Eq. 6) are the equilibrium tidal-flat elevations. The curves are based on the assumption of constant annual deposition and a geomorphologically significant wind speed of 8 m/s, the typical value for tidal flats in the Venice Lagoon. The equilibrium point on the right is stable because small perturbations in elevation can be recovered by the system, whereas the equilibrium point on the left is unstable. (B) Tidal-flat equilibrium conditions as a function of different deposition rates. (C) Tidal-flat equilibrium conditions for sediment deposition decreasing with elevation. The stable branch of the curve extends to the tangent point with the deposition line. (D) Shear-stress curves as a function of fetch length.

to settle decreases with elevation when the marsh becomes emergent. Although this relationship is strictly true for bottom elevations within the tidal range, here we extend this assumption to tidal flats and determine the consequences of a decreasing sedimentation rate on equilibrium conditions. If we assume a constant decrease in sedimentation rate and cohesive sediments ($\alpha = 1$), the right-hand side of Eq. 6 can be graphically described as a sloping line that intersects the shear-stress curve in two points (Fig. 4C). Again, we can separate the curve into two branches (stable and unstable), but now the boundary between the two branches is defined by the tangent point between the sloping line and the shear-stress curve. Because the line describing Eq. 6 decreases with elevation, the separation point between the two branches is located at a lower elevation than that in the constant-deposition case. Similarly, it is possible to determine the tidal-flat equilibrium conditions for different sediment property ($\alpha \neq 1$) and different monotonic relationships between deposition and elevation by substituting the sloping line with the corresponding curve.

Discussion and Conclusions

The presence of an unstable part in the curve of Fig. 4A is a very reasonable explanation for the reduced frequency of areas at intermediate elevations (Fig. 2). However, the unstable region predicted by the model extends to -1.00 m above MSL, whereas field evidence shows that the area frequency decreases only below -0.50 m above MSL. The reasons for this discrepancy are many fold: (i) Short wind fetch limits wave height. The distribution of bottom shear stress as a function of fetch length calculated by using the finite-element model (10) solving Eq. 1 indicates that the peak in shear stress shifts toward shallower depths (as shown in Fig. 4D). The shear stress peaks at -0.5 m for a fetch of 1,000 m, the characteristic value for the Venice Lagoon, where frequent islands and marshes limit the distance over which the wind blows. (ii) Tidal excursions periodically shift the water depth by approximately ± 0.35 m. (iii) Deposition rates may be affected by water depth (Fig. 4C).

The decoupling of erosion and sedimentation in Eq. 5 is partly justified by the fact that the average path of suspended sediment during a tidal cycle is of the same order of magnitude of the basin dimensions so that only a small fraction of eroded sediments is redeposited at the same location. In general, the deposition rate at each point of the basin depends on sediment redistribution driven by tidal currents, on the distance from the main tidal channels, and on allogenic sediment sources such as rivers and inlets. To determine the evolution of the entire system, our point analysis of tidal-flat evolution must be coupled to a spatial description of sediment transport in the basin so that the local sediment availability and average deposition rate are determined.

It is worth noting (see Fig. 2) that the encroachment of halophyte vegetation on salt marshes starts at $+0.05$ m in the Venice Lagoon and that the canopy is fully developed only above $+0.15$ m, as reported in detailed field measurements (18). Thus, halophyte vegetation does not affect the transition from tidal flats to salt marshes for bottom elevations below MSL. Once the tidal flat emerges, the vegetation rapidly colonizes the surface, increasing its elevation by sediment trapping and below-ground organic production. Of particular importance for salt-marsh equilibrium are the feedbacks between vegetation and accretion, including inorganic sediment trapping by vegetation (17, 19, 20). It is then the reduction in wave activity that is ultimately responsible for the bifurcation of tidal landforms.

The bimodal distribution of tidal landforms is well defined for the 1901 Southern Lagoon (see Fig. 2), whereas it is less evident for the 2000 bathymetry, with a less pronounced maximum for salt marshes. This difference is due to the reduction in salt-marsh area occurred in the Venice Lagoon in recent decades but also

