

## CONTROLLED FISSION REACTIONS AND REACTORS

i.e. How can we use the fission to produce energy in a controlled way.

Let's consider a infinitely large mass of Uranium, which for now we assume to be of natural isotopic composition (0,72%  $^{235}\text{U}$ , 99,28%  $^{238}\text{U}$ )

A single fission will produce 2,5 neutrons on average.

Each "second-generation" neutron is capable to produce other fissions producing each time more neutrons. This is called "chain reaction"

Each fission releases  $\approx 200$  MeV in form of kinetic energy and radiation.

It can be convenient to define a neutron reproduction factor  $k_{\infty}$  (for infinite medium  $\Rightarrow$  ignoring the loss of neutron at the surface)

Each thermal neutron produces  $k_{\infty}$  new thermal neutron.

For a reaction chain to continue we must have  $k_{\infty} \geq 1$ .

Although for each reaction there 2.5 n, there are fast neutrons

Neutron lose energy in elastic collisions with nuclei, A popular choice<sup>(1)</sup> for moderator is Carbon in form of graphite blocks.

(Why? C is solid, inexpensive and easy to handle).

A lattice of blocks of U alternated with graphite is called "chain-react pile", and the first one was constructed by Fermi in 1942.

If  $k = 1$   $\Rightarrow$  The pile is critical  $\longrightarrow$  Steady release of energy  
 $k < 1$   $\Rightarrow$  The pile is subcritical  
 $k > 1$   $\Rightarrow$  " supercritical

Let's assume we have  $N$  thermal neutrons at the present generation.

Even if we will not have  $\nu N$  fast fission neutrons immediately available. Some will be absorbed by many processes, mainly  $(n, \gamma)$  in both  $^{235}\text{U}$  and  $^{238}\text{U}$ .

$\eta$  is defined as mean number of fission neutron produced per original thermal neutron.  $\eta < \nu$  in general

If  $\sigma_f$  is <sup>the</sup> fission cross-section, and  $\sigma_a$  the cross-section for absorptive processes the relative probability for a neutron to cause fission is

$$p = \frac{\sigma_f}{\sigma_f + \sigma_a}$$

and then  $\eta = \nu \frac{\sigma_f}{\sigma_f + \sigma_a}$

For  $^{235}\text{U}$   $\sigma_f = 584 \text{ b}$   $\sigma_a = 97 \text{ b}$   $\Rightarrow \eta = 2.08$  fast neutrons are produced per thermal neutron

$^{238}\text{U}$  is not fissionable so  $\sigma_f = 0$  and  $\sigma_a = 2.75 \text{ b}$ . For a natural mixture of Uranium:

$$\sigma_f = \frac{972}{100} \sigma_f(^{235}\text{U}) + \frac{99.28}{100} \sigma_f(^{238}\text{U}) = 4.20 \text{ b}$$

$$\sigma_a = \frac{0,72}{100} \sigma_a(235) + \frac{99,28}{100} \sigma_a(238) = 3,65b$$

$$\Rightarrow \eta_{\text{NAT}} = 1,33$$

Very close to 1, so we should minimize the neutrons to be lost in order to obtain a critical reactor.

If enriched Uranium is used ( $^{235}\text{U} = 3\%$ ) then  $\eta = 1,84$ , allowing more neutrons to be lost by other means to maintain the criticality conditions.

At this point the  $N$  thermal neutrons have been partially absorbed and now there are  $\eta N$  neutrons to slow down to thermal energies.

These fast neutrons can fission with  $^{238}\text{U}$  ( $\sigma \approx 1b$ ), increasing the number of neutrons  $\rightarrow$  A factor  $\epsilon$  (fast fission factor) has to be taken into account  $\rightarrow \eta \epsilon N$  neutrons are present ( $\epsilon = 1,03$  for natural Uranium).

Moderation of  $n$  is accomplished by light moderator.

It takes  $\approx 100$  collisions <sup>in carbon</sup> to moderate a MeV neutron down to thermal energy.

But, in the process,  $n$  must pass through the resonance region with high  $\sigma$  (up to  $1000b \gg \sigma_{\text{fission}}$ )  $\Rightarrow$  If we want thermal neutrons we have to avoid resonance capture at all.

If C and U are mixed in powder this is impossible to achieve, but if there is enough C  $n$  can scatter inside it avoiding resonance region. About 20 cm of C are needed to moderate MeV  $n$  down to  $10^{-3}eV$ .

Nevertheless there will be a probability  $p$  that some  $n$  are captured.

$p \approx 0,9$ . The # of <sup>usable</sup>  $n$  now is  $n_{\text{next}} = \eta \epsilon p N$

Now that  $n$  are thermalized they must interact with  $^{235}\text{U}$ .

Note that  $n$  can still interact with C ( $\sigma_{\text{fission}} = 0,0034b$ ), because there is

a lot of it.  $\Rightarrow$  An additional term must be included.

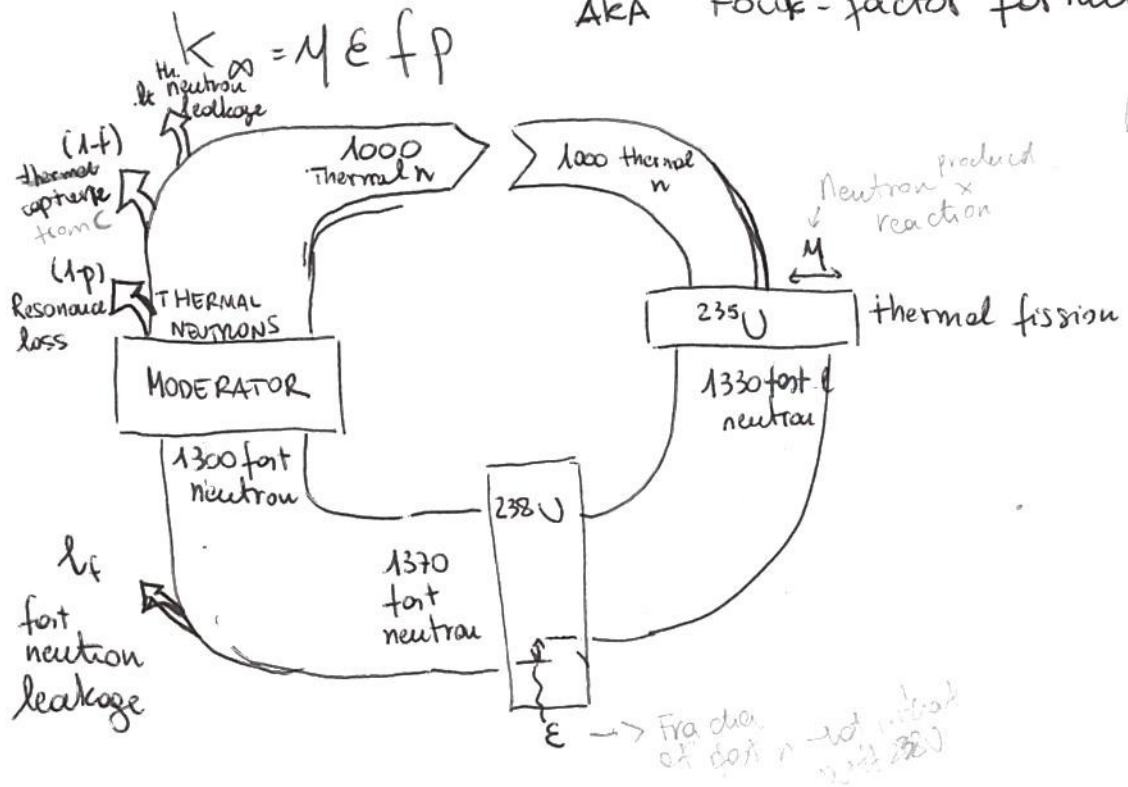
$f$  = thermal utilization factor  $\equiv$  fraction of thermal neutron available to  $^{235}\text{U}$  and  $^{238}\text{U}$ .  $f \approx 0,9$

Find number of  $n$   $N_{\text{neut}} = M \epsilon p f N$  whether this is  $>$  or  $<$  than  $N$  determines the criticality of reactor.

The reproduction factor is

AKA "Four-factor formula"

- $M = 1,33$
- $\epsilon = 1,03$
- $P = 0,9$
- $f = 0,9$
- $\approx 1,11$



$k_{\infty} \approx 1,11 \rightarrow$  which is still not appropriate because we ignored leakage of  $n$  at the surface  $\Rightarrow l_f$  and  $l_t$  are fractions of leakage of fast and thermal neutrons

$$k_{\infty} = M \epsilon p f (1 - l_f) (1 - l_t)$$

The larger the pile, the smaller is Surface/Volume ratio  $\Rightarrow$  the smaller is the fraction of neutrons that leak

If  $l_f, l_t$  are small  $\rightarrow k_{\infty} - k \approx k (l_f + l_t)$

the total leakage decreases as the surface increases.

Leakage will increase if neutrons have to travel for a long distance, called MITIGATION LENGTH  $M$ .

$M$  includes 2 contributors diffusion length  $L_d$  for thermal neutrons and the slowing distance  $L_s$

$$M = (L_d^2 + L_s^2)^{1/2}$$

For graphite  $L_s = 18,7 \text{ cm}$   $L_d = 50,8 \text{ cm}$

If the pile has a dimension  $R$  (radius or side length)

$$(k_{\infty} - k) \propto R^{-2} \quad \text{and} \quad k_{\infty} - k \propto M$$

Are reasonable assumptions

$$\rightarrow k_{\infty} - k \propto \frac{M^2}{R^2}$$

So there will be a critical size  $R_c$  which corresponds to  $k=1$

$$R_c \propto \frac{M}{\sqrt{k_{\infty} - 1}}$$

From spherical arrangement

$$R_c = \frac{\pi M}{\sqrt{k_{\infty} - 1}}$$

For natural uranium-graphite reactor  $R_c = 5 \text{ m}$ . For  $R = 5 \text{ m}$  the "reactor" goes critical. How to decrease the size? Surround the pile with a reflector material for neutrons.

Let's now evaluate now the time needed for the process.

Neutrons are characterized by a time constant  $\tau$  which includes the time to moderate ( $\approx 10^{-6} \text{ s}$ ) and a diffusion time ( $\approx 10^{-3} \text{ s}$ ).

If the reproducing factor is  $k$  and there are  $N$  neutrons at time  $t$ , on average there are  $kN$  neutrons at time  $t + \tau$  and  $k^2N$  at time  $t + 2\tau$

In a short interval  $dt$

$$dN = (kN - N) \frac{dt}{\tau}$$

$$\Rightarrow N(t) = N_0 e^{(k-1)t/\tau}$$

If  $k = 1 \rightarrow N = \text{constant}$ . If  $k < 1$  the number of neutrons decreases <sup>(MS)</sup> exponentially. If  $k > 1$   $N$  increases exponentially, with a time constant  $\tau/k-1$ .

Control. The number of neutrons is essential and can be achieved by ~~by~~ inserting ~~the~~ some bars of materials able to absorb neutrons (like Cadmium).

## BASICS OF NUCLEAR REACTORS

We will cover only the general properties ~~of~~ and categories of reactors.