

STRONG, LIGHT STRUT (when stability under compression is the limit)

F: strut (purlone)

C: L, $F_{CR} > F^*$ $F_{CR} = \frac{n^2 \pi^2 EI}{L^2}$

O: min mass $\rightarrow m = AL\rho$

F.V.: A, material



$$\frac{n^2 \pi^2 EA^2}{12L^2} > F^* \quad A > \left(\frac{12F^* L^2}{n^2 \pi^2 E} \right)^{\frac{1}{2}}$$

$$m > \left(\frac{12F^* L^2}{n^2 \pi^2} \right) L \frac{\rho}{E^{\frac{1}{2}}}$$

$$M = \frac{\rho}{E^{\frac{1}{2}}}$$

CHEAP, STIFF TIE

F: tie

C: L, $S > S^*$ $S = \frac{EA}{L} > S^*$ cost per unit mass

O: min cost $C = AL\rho c_m$

F.V.: A, material

$$C > \frac{LS^*}{E} L \rho c_m$$

$$M_{ic} = \frac{\rho c_m}{E}$$

Slope of a line for a strong, light beam

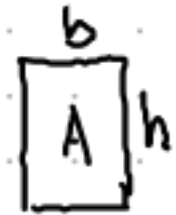
$$M = \frac{\rho}{E^{\frac{1}{2}}}$$

$$\log M = \frac{2}{3} \log \rho - \log E$$

$$\log \rho = \frac{3}{2} \log E + \frac{3}{2} \log M$$

CHANGING FREE VARIABLES

Example: light stiff beam with different free variables



0: min mass $m = hbL\rho$
 C: L, $S > S^*$ $S = \frac{F}{\delta} = \frac{CEI}{L^3} = \frac{CE}{L^3} \frac{bh^3}{12} > S^*$
 F: ?

1) FV: A cross section area (aspect ratio is fixed $\Rightarrow b = \alpha h$)

$M = \frac{P}{E^{1/2}}$

2) FV: b $A = bh$

$b > \frac{12 S^* L^3}{CE h^3} \Rightarrow m > \frac{12 S^* L^3}{C h^3} h L \frac{\rho}{E} \Rightarrow M = \frac{P}{E}$

3) FV: h

$h > \left(\frac{12 S^* L^3}{CE b} \right)^{1/3} \Rightarrow m > \left(\frac{12 S^* L^3}{C b} \right)^{1/3} b L \frac{\rho}{E^{1/3}} \Rightarrow M = \frac{P}{E^{1/3}}$

The choice of the free variable strongly influences materials selection

NOTE: this is the same as the one for the board in bending

