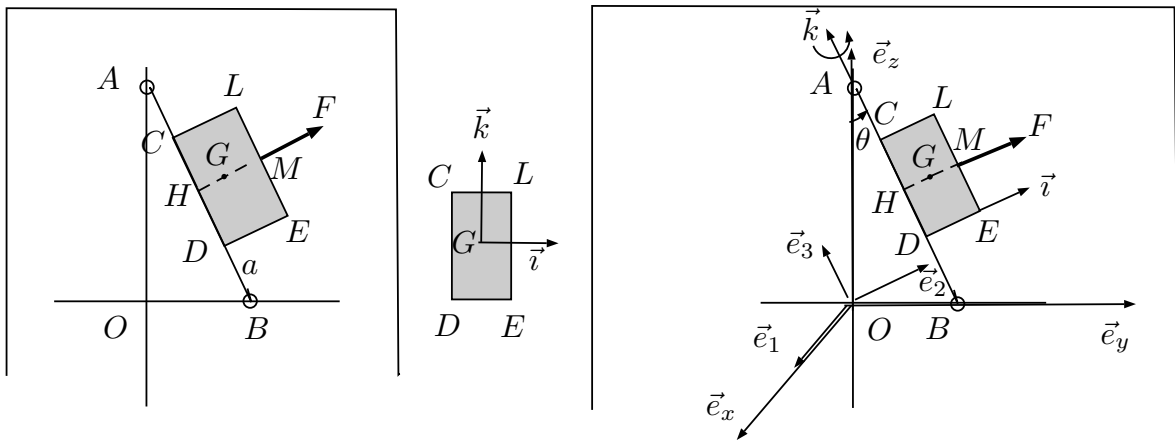


Compito di Meccanica Razionale (9 CFU)

Trieste, 25 gennaio 2019. (G. Tondo)

Un rigido è costituito da una lamina rettangolare omogenea di massa m e lati a e $4a$, saldata, lungo il lato CD , ad un'asta AB di lunghezza $6a$ e di massa trascurabile, in modo che il punto medio H del lato CD coincida con il punto medio di AB . Gli estremi dell'asta sono vincolati, come in figura, a scorrere senza attrito lungo due guide fisse ortogonali, tramite due cerniere sferiche "bucate". Sul rigido agisce il peso proprio opposto ad \vec{e}_z e una forza F diretta come il lato DE e applicata nel punto medio M del lato EL .



Oltre alla terna fissa $(\vec{e}_x, \vec{e}_y, \vec{e}_z)$, si suggerisce di usare anche una terna intermedia formata dai versori $(\vec{e}_1, \vec{e}_2, \vec{e}_3)$, con $\vec{e}_1 = \vec{e}_x$, $\vec{e}_3 = \text{vers}(A - D)$, $\vec{e}_2 = \vec{e}_3 \times \vec{e}_1$. Inoltre, si consiglia di prendere una terna solidale alla lamina $(\vec{i}, \vec{j}, \vec{k})$, con il versore $\vec{i} = \text{vers}(E - D)$, $\vec{k} = \vec{e}_3$ e $\vec{j} = \vec{k} \times \vec{i}$.

Sia $-\pi < \theta \leq \pi$ l'angolo compreso tra \vec{e}_z e \vec{k} , e sia $-\pi < \psi \leq \pi$ quello compreso tra \vec{e}_1 e \vec{i} .

STATICA

Determinare:

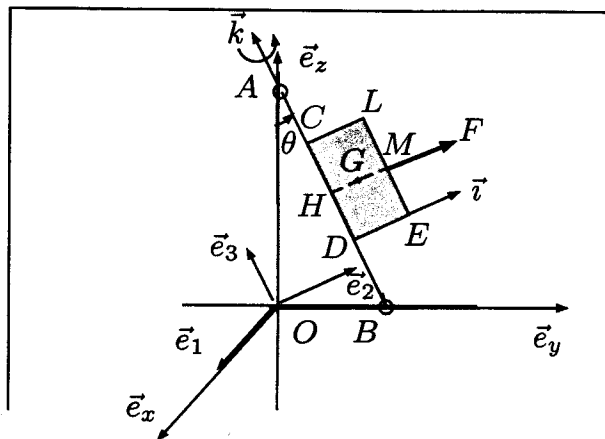
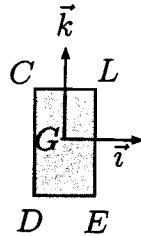
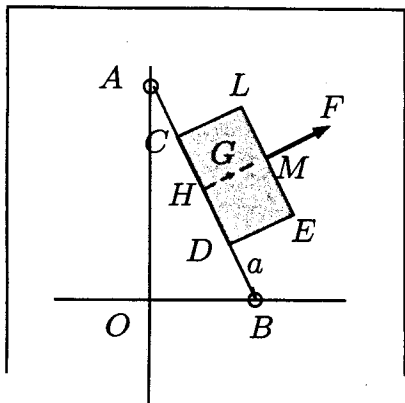
- 1) il valore del parametro $\lambda = \frac{F}{mg}$ necessario all'equilibrio nella configurazione $\theta_e = -\frac{\pi}{6}$, $\psi_e = \frac{\pi}{2}$;
- 2) le reazioni vincolari esterne sul rigido in A , in tale configurazione di equilibrio;
- 3) le reazioni vincolari esterne sul rigido in B , tale configurazione di equilibrio.

DINAMICA

- 4) Scrivere le equazione differenziali pure di moto;
- 5) linearizzare le equazioni di moto intorno alla configurazione di equilibrio suddetta;
- 6) calcolare le reazioni vincolare esterne nei punti A e B , durante il moto.

Tarea del 25/01/2013

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Il modello è formato da un solido rigido vincolato con 2 cerniere sferiche lisce. Con il metodo dei congelamenti meccanici, possiamo osservare che se blocchiamo lo scorrimento del punto B del rigido sull'asse (O, \vec{e}_3) , il rigido può ancora ruotare attorno all'asse (B, \vec{k}) . Dunque, il rigido ha 2 g. l. e, come coordinate libere possiamo prendere gli angoli

$$-\bar{\pi} < \theta \leq \bar{\pi}, \quad -\bar{\pi} < \psi \leq \bar{\pi}$$

Quindi, ogni configurazione del rigido è individuata da

$$\vec{q} = (\theta, \psi)$$

Consideriamo le 3 basi

$$B = (\vec{e}_1, \vec{e}_2, \vec{e}_3) : \text{"fissa"}$$

$$B' = (\vec{i}_1, \vec{i}_2, \vec{i}_3) : \text{"intermediate"}$$

$$B'' = (\vec{i}, \vec{j}, \vec{k}) : \text{solidale al rigido}$$

le equazioni di trasformazione sono

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$$(2.1) \begin{cases} \vec{l}_1 = \vec{l}_x \\ \vec{l}_2 = \cos\theta \vec{l}_y + \sin\theta \vec{l}_z \\ \vec{l}_3 = -\sin\theta \vec{l}_y + \cos\theta \vec{l}_z \end{cases} \quad [\vec{l}_1, \vec{l}_2, \vec{l}_3] = [\vec{l}_x, \vec{l}_y, \vec{l}_z] \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & -\sin\theta \\ 0 & \sin\theta & \cos\theta \end{bmatrix}}_{R_\theta}$$

Quindi,

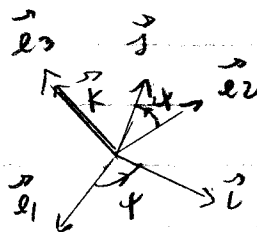
$$R_\theta R_\theta^T = \mathbb{1}$$

$$[\vec{l}_x, \vec{l}_y, \vec{l}_z] = [\vec{l}_1, \vec{l}_2, \vec{l}_3] R_\theta^T = [\vec{l}_1, \vec{l}_2, \vec{l}_3] \underbrace{\begin{bmatrix} 1 & 0 & 0 \\ 0 & \cos\theta & \sin\theta \\ 0 & -\sin\theta & \cos\theta \end{bmatrix}}_{R_\theta^T}$$

cioè:

$$(2.2) \begin{cases} \vec{l}_x = \vec{l}_1 \\ \vec{l}_y = \cos\theta \vec{l}_2 - \sin\theta \vec{l}_3 \\ \vec{l}_z = \sin\theta \vec{l}_2 + \cos\theta \vec{l}_3 \end{cases}$$

Analogamente,



$$(2.3) \begin{cases} \vec{i} = \cos\psi \vec{l}_1 + \sin\psi \vec{l}_2 \\ \vec{j} = -\sin\psi \vec{l}_1 + \cos\psi \vec{l}_2 \\ \vec{k} = \vec{l}_3 \end{cases}$$

$$[\vec{i}, \vec{j}, \vec{k}] = [\vec{l}_1, \vec{l}_2, \vec{l}_3] \underbrace{\begin{bmatrix} \cos\psi & -\sin\psi & 0 \\ \sin\psi & \cos\psi & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{R_\psi}$$

Quindi

$$(2.4) [\vec{l}_1, \vec{l}_2, \vec{l}_3] = [\vec{i}, \vec{j}, \vec{k}] R_\psi^T = [\vec{i}, \vec{j}, \vec{k}] \underbrace{\begin{bmatrix} \cos\psi & \sin\psi & 0 \\ -\sin\psi & \cos\psi & 0 \\ 0 & 0 & 1 \end{bmatrix}}_{R_\psi^T}$$

cioè

$$(2.5) \begin{cases} \vec{l}_1 = \cos\psi \vec{i} + \sin\psi \vec{j} \\ \vec{l}_2 = -\sin\psi \vec{i} + \cos\psi \vec{j} \\ \vec{l}_3 = \vec{k} \end{cases}$$

Componendo le trasformazioni (2.2) e (2.4) o, equivalentemente, moltiplicando le matrici R_θ^T e R_ψ^T , si trova

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$$(3.1) \quad [\vec{e}_x, \vec{e}_y, \vec{e}_z] = [\vec{e}_1, \vec{e}_2, \vec{e}_3] R_\theta^T \stackrel{(2.4)}{=} [\vec{i}, \vec{j}, \vec{k}] R_\psi^T R_\theta^T$$

cioè

$$(3.2) \quad \begin{cases} \vec{e}_x = \cos \psi \vec{i} - \sin \psi \vec{j} \\ \vec{e}_y = \cos \theta (\sin \psi \vec{i} + \cos \psi \vec{j}) - \sin \theta \vec{k} = \cos \theta \sin \psi \vec{i} + \cos \theta \cos \psi \vec{j} - \sin \theta \vec{k} \\ \vec{e}_z = \sin \theta (\sin \psi \vec{i} + \cos \psi \vec{j}) + \cos \theta \vec{k} = \sin \theta \sin \psi \vec{i} + \sin \theta \cos \psi \vec{j} + \cos \theta \vec{k} \end{cases}$$

$$(3.3) \quad \begin{cases} \vec{i} = \cos \psi \vec{e}_x + \cos \theta \sin \psi \vec{e}_y + \sin \theta \sin \psi \vec{e}_z \\ \vec{j} = -\sin \psi \vec{e}_x + \cos \theta \cos \psi \vec{e}_y + \sin \theta \cos \psi \vec{e}_z \\ \vec{k} = -\sin \theta \vec{e}_y + \cos \theta \vec{e}_z \end{cases}$$

$$(3.3) \quad G-H = \frac{a}{2} \vec{i} = \frac{a}{2} (\cos \psi \vec{e}_x + \sin \psi \vec{e}_z) \stackrel{(2.1)}{=} \frac{a}{2} [\cos \psi \vec{e}_x + \sin \psi (\cos \theta \vec{e}_y + \sin \theta \vec{e}_z)]$$

$$(3.4) \quad H-B = 3a \vec{k} = 3a \vec{e}_z = 3a (-\sin \theta \vec{e}_y + \cos \theta \vec{e}_z)$$

$$(3.5) \quad B-O = 6a \sin \theta \vec{e}_y$$

Quindi,

$$(3.6) \quad G-O = (G-H) + (H-B) + (B-O) = \frac{a}{2} \vec{i} + 3a \vec{e}_z + 6a \sin \theta \vec{e}_y$$

$$= \frac{a}{2} \cos \psi \vec{e}_x + \frac{a}{2} \cos \theta \sin \psi \vec{e}_y + \frac{a}{2} \sin \theta \sin \psi \vec{e}_z + 3a (-\sin \theta \vec{e}_y + \cos \theta \vec{e}_z) + 6a \sin \theta \vec{e}_y$$

$$= \frac{a}{2} \cos \psi \vec{e}_x + \left(\frac{a}{2} \cos \theta \sin \psi + 3a \sin \theta \right) \vec{e}_y + \left(\frac{a}{2} \sin \theta \sin \psi + 3a \cos \theta \right) \vec{e}_z$$

Statica

L4

La sollecitazione attiva è data dal peso (conservativa) e da un carico follower. Allora, calcoliamo le forze generalizzate (Q_θ, Q_ψ) . Sappiamo che, per la parte conservativa,

$$Q_\theta^{(peso)} = -\frac{\partial V^{(peso)}}{\partial \theta}, \quad Q_\psi^{(peso)} = -\frac{\partial V^{(peso)}}{\partial \psi}$$

Allora, calcoliamo

$$V^{(peso)} = -m \vec{g} \cdot (\vec{r} - \vec{0}) = m g \vec{e}_z \cdot (\vec{r} - \vec{0}) = m g a \left(\frac{1}{2} \sin \theta \sin \psi + 3 \cos \theta \right)$$

Quindi

$$Q_\theta^{(peso)} = -m g a \left(\frac{1}{2} \cos \theta \sin \psi - 3 \sin \theta \right)$$

$$Q_\psi^{(peso)} = -m g a \left(\frac{1}{2} \sin \theta \cos \psi \right)$$

Ora calcoliamo il contributo alle forze generalizzate dato dal carico follower

$$Q_\theta^{(foll)}, \quad Q_\psi^{(foll)}$$

A tale scopo, scriviamo il LV del carico follower sul rigido

$$LV^{(foll)} = \vec{F} \cdot \delta \vec{x}_H + \vec{M}_H \cdot \vec{e}$$

$$\begin{aligned} \vec{x}_H = H - \vec{0} &= 3a \vec{r} + 6a \sin \theta \vec{e}_y \stackrel{(3,4)}{=} 3a (-\sin \theta \vec{e}_y + \cos \theta \vec{e}_z) + 6a \sin \theta \vec{e}_y \\ &= 3a (\sin \theta \vec{e}_y + \cos \theta \vec{e}_z) \end{aligned}$$

$$\delta \vec{x}_H = 3a (\cos \theta \vec{e}_y - \sin \theta \vec{e}_z) \delta \theta$$

Daunque,

$$\begin{aligned}
 (5.1) \quad \Delta V &= \vec{F} \cdot \delta \vec{x}_M = F \vec{u} \cdot 3a (\cos \theta \vec{e}_y - \sin \theta \vec{e}_z) \delta \theta = \\
 &= 3a F (\cos \psi \vec{e}_x + \cos \theta \sin \psi \vec{e}_y + \sin \theta \sin \psi \vec{e}_z) \cdot (\cos \theta \vec{e}_y - \sin \theta \vec{e}_z) \delta \theta = \\
 &= 3Fa (\cos^2 \theta \sin \psi - \sin^2 \theta \sin \psi) \delta \theta = \\
 &= 3Fa \sin \psi (\cos^2 \theta - \sin^2 \theta) \delta \theta = 3Fa \sin \psi \cos 2\theta \delta \theta
 \end{aligned}$$

Allora,

$$(5.2) \quad Q_\theta^{(pot)} = 3Fa \sin \psi \cos 2\theta, \quad Q_\psi^{(pot)} = 0$$

Quindi, le forze generalizzate sono

$$\begin{aligned}
 (5.3) \quad Q_\theta &= Q_\theta^{(pot)} + Q_\theta^{(roz)} = -mga \left(\frac{1}{2} \cos \theta \sin \psi - 3 \sin \theta \right) + 3Fa \sin \psi \cos 2\theta \\
 Q_\psi &= Q_\psi^{(pot)} + Q_\psi^{(roz)} = -\frac{mga}{2} \sin \theta \cos \psi
 \end{aligned}$$

La configurazione assegnata $\vec{q}_e = \left(\theta_e = -\frac{\pi}{6}, \psi_e = \frac{\pi}{2} \right)$ è di equilibrio se e solo se

$$(5.4) \quad 0 = Q_\theta|_{\vec{q}_e} = -mga \left(\frac{1}{2} \frac{\sqrt{3}}{2} + \frac{3}{2} \right) + \frac{3}{2} Fa$$

$$(5.5) \quad 0 = Q_\psi|_{\vec{q}_e} \quad \text{O.K.}$$

Allora, la (5.4) è soddisfatta se e solo se

$$(5.6) \quad \frac{3}{2} F = \frac{mga}{2} \left(\frac{\sqrt{3}}{2} + 3 \right) \Leftrightarrow \lambda = \frac{F}{mg} = \frac{1}{3} \left(3 + \frac{\sqrt{3}}{2} \right) = 1 + \frac{1}{2\sqrt{3}} > 0$$

2) + 3) Reazioni all'equilibrio in A e B

L7/8

Le cerniere sferiche sono, per ipotesi, non dissipative e bilaterali. Quindi, eserciteranno una reazione attiva data da

$$(7.1) \quad \mathcal{L}^{(reat)} = \{ (A, \vec{\Psi}), (B, \vec{\Phi}) \} \text{ con } \vec{\Psi}_A \cdot \vec{e}_2 = 0, \vec{\Phi}_B \cdot \vec{e}_4 = 0$$

Per calcolare $\vec{\Psi}_A$ e $\vec{\Phi}_B$, scriviamo le ECS in tutto il rigido

$$(7.2) \quad \begin{cases} \vec{R}^{(ext, att)} + \vec{\Psi}_A + \vec{\Phi}_B = 0 \\ \vec{M}_B^{(ext, att)} + (A-B) \times \vec{\Psi}_A = 0 \end{cases}$$

Calcoliamo il risultante delle forze esterne attive:

$$\begin{aligned} \vec{R}^{(ext, att)} &= -mg \vec{e}_2 + \vec{F} = -mg \vec{e}_2 + F \vec{c} = \\ &= -mg \vec{e}_2 + F (\cos \varphi \vec{e}_x + \cos \theta \sin \varphi \vec{e}_y + \sin \theta \sin \varphi \vec{e}_z) \\ &= F \cos \varphi \vec{e}_x + F \cos \theta \sin \varphi \vec{e}_y + (F \sin \theta \sin \varphi - mg) \vec{e}_z \end{aligned}$$

Quindi, proiettando la I ECS (7.2) nella base fissa B

$$(7.3) \quad \begin{cases} (\vec{\Psi}_A + \vec{\Phi}_B) \cdot \vec{e}_x = -F \cos \varphi \\ \vec{\Psi}_A \cdot \vec{e}_y = -F \cos \theta \sin \varphi \\ \vec{\Phi}_B \cdot \vec{e}_z = -(F \sin \theta \sin \varphi - mg) \end{cases}$$

Dunque, nelle configurazioni di equilibrio angolate $\vec{q}_e = \left(\frac{\pi}{6}, \frac{\pi}{2} \right)$ si trova

$$(7.4) \quad \begin{cases} (\vec{\Psi}_A + \vec{\Phi}_B) \cdot \vec{e}_x = 0 \\ \vec{\Psi}_A \cdot \vec{e}_y = -F \frac{\sqrt{3}}{2} = -mg \lambda \frac{\sqrt{3}}{2} = -mg \frac{\sqrt{3}}{2} \left(1 + \frac{1}{2\sqrt{3}} \right) = -\frac{mg}{2} \left(\frac{\sqrt{3}+1}{2} \right) \\ \vec{\Phi}_B \cdot \vec{e}_z = \frac{F}{2} + mg = \frac{mg \lambda}{2} + mg = mg \left(\frac{\lambda}{2} + 1 \right) = \frac{mg}{2} \left(3 + \frac{1}{2\sqrt{3}} \right) \end{cases}$$

Restano da determinare $\vec{\Psi}_A \cdot \vec{e}_x$ e $\vec{\phi}_B \cdot \vec{e}_x$. A tale scopo, osserviamo che, nella configurazione di equilibrio \vec{q}_e , il rigido giace nel piano $\Pi_x = (0, \vec{e}_1, \vec{e}_2)$ insieme con tutte le forze attive a cui è soggetto. Dunque,

$$\vec{R} \stackrel{(ext, act)}{\in} \Pi_x, \quad \vec{M}_P \stackrel{(ext, act)}{\perp} \Pi_x \quad \forall P \in \Pi_x$$

Dalle ECS, segue che

$$\vec{R} \stackrel{(ext, react)}{\in} \Pi_x, \quad \vec{M}_P \stackrel{(ext, react)}{\perp} \Pi_x \quad \forall P \in \Pi_x$$

La I equivale alla I delle (7.4), la II implica che

$$\vec{M}_B \stackrel{(ext, react)}{=} (A-B) \times \vec{\Psi}_A \perp \Pi_x$$

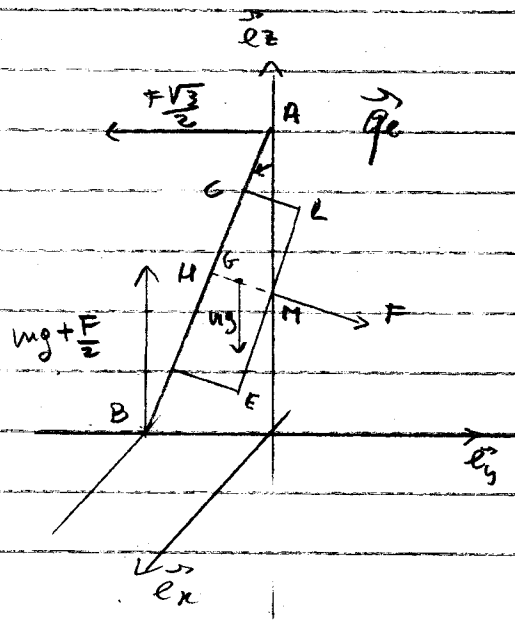
Dunque, $\vec{\Psi}_A \in \Pi_x$, quindi

$$\vec{\Psi}_A \cdot \vec{e}_x = 0 \quad \text{et} \quad \vec{\phi}_B \cdot \vec{e}_x \stackrel{(2.4)}{=} 0$$

In conclusione,

$$\vec{\Psi}_A = -\frac{mg}{2} \left(\sqrt{3} + \frac{1}{2} \right) \vec{e}_y$$

$$\vec{\phi}_B = \frac{mg}{2} \left(3 + \frac{1}{2\sqrt{3}} \right) \vec{e}_z$$



4) Scriviamo le 2 EL relative a θ e ψ . A tale scopo calcoliamo l'energia cinetica del rigido.

$$(10.1) K = \frac{1}{2} m |\vec{v}_H|^2 + \frac{1}{2} \vec{\omega} \cdot \mathbf{I}_H(\vec{\omega}) + m \vec{v}_H \cdot \vec{\omega} \times (\mathbf{G} - \mathbf{H})$$

Dalle (3.4) e (3.5) segue che

$$(10.2) \mathbf{H} - \mathbf{O} = (\mathbf{H} - \mathbf{B}) + (\mathbf{B} - \mathbf{O}) = 3a \vec{k} + 6a \sin \theta \vec{e}_y = 3a (\sin \theta \vec{e}_y + \cos \theta \vec{e}_z)$$

Quindi,

$$(10.3) \vec{v}_H = \frac{d}{dt} (\mathbf{H} - \mathbf{O}) = 3a (\cos \theta \vec{e}_y - \sin \theta \vec{e}_z) \dot{\theta}$$

$$(10.4) |\vec{v}_H|^2 = 9a^2 (\cos^2 \theta + \sin^2 \theta) \dot{\theta}^2 = 9a^2 \dot{\theta}^2$$

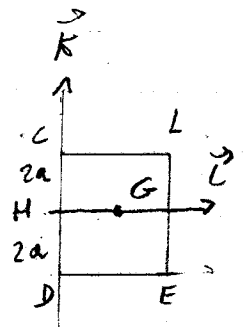
Dal Teo. di Fermi segue che

$$(10.5) \vec{\omega} = \dot{\theta} \vec{e}_z + \dot{\psi} \vec{k} \stackrel{(2.5)}{=} \dot{\theta} (\cos \psi \vec{i} - \sin \psi \vec{j}) + \dot{\psi} \vec{k}$$

la terma $(\mathbf{H}, \vec{i}, \vec{j}, \vec{k})$ è una TPI(H) (perché?)

quindi

$$(10.6) \mathbf{I}_H^{(B'')} = ma^2 \begin{bmatrix} \frac{16}{3} & & \\ & \frac{5}{3} & \\ & & \frac{1}{3} \end{bmatrix} = \frac{ma^2}{3} \begin{bmatrix} 4 & & \\ & 5 & \\ & & 1 \end{bmatrix}$$



Dunque

$$(10.7) \frac{1}{2} \vec{\omega} \cdot \mathbf{I}_H(\vec{\omega}) = \frac{1}{2} \vec{\omega} \cdot \frac{ma^2}{3} \begin{bmatrix} 4 & & \\ & 5 & \\ & & 1 \end{bmatrix} \begin{bmatrix} \dot{\theta} \cos \psi \\ -\dot{\theta} \sin \psi \\ \dot{\psi} \end{bmatrix} = \frac{ma^2}{6} [\dot{\theta} \cos \psi, -\dot{\theta} \sin \psi, \dot{\psi}] \begin{bmatrix} 4\dot{\theta} \cos \psi \\ -2\dot{\theta} \sin \psi \\ \dot{\psi} \end{bmatrix} =$$

$$= \frac{ma^2}{6} (4\dot{\theta}^2 \cos^2 \psi + 5\dot{\theta}^2 \sin^2 \psi + \dot{\psi}^2) =$$

$$= \frac{ma^2}{6} [(4 + \sin^2 \psi) \dot{\theta}^2 + \dot{\psi}^2]$$

$$\vec{\omega} \times (G-H) = (\dot{\theta} \cos \psi \vec{i} - \dot{\theta} \sin \psi \vec{j} + \dot{\psi} \vec{k}) \times \frac{a}{2} \vec{i} =$$

$$= \frac{a}{2} (\dot{\theta} \sin \psi \vec{k} + \dot{\psi} \vec{j})$$

(11)

Inoltre, riscrivendo \vec{v}_H nella base solidale B^a , si ottiene

$$\vec{v}_H = 3a\dot{\theta} (\cos \theta \vec{e}_y - \sin \theta \vec{e}_z) = 3a\dot{\theta} [\cos \theta (\sin \psi \vec{i} + \cos \psi \vec{j}) - \sin \theta \vec{k}] \cos \theta +$$

$$- 3a\dot{\theta} [\sin \theta (\sin \psi \vec{i} + \cos \psi \vec{j}) + \cos \theta \vec{k}] \sin \theta$$

$$= 3a\dot{\theta} [(\cos^2 \theta - \sin^2 \theta) (\sin \psi \vec{i} + \cos \psi \vec{j}) - \sin 2\theta \cos \theta \vec{k}] =$$

$$= 3a\dot{\theta} [\cos 2\theta (\sin \psi \vec{i} + \cos \psi \vec{j}) - \sin 2\theta \vec{k}]$$

Quindi, il termine misto delle (10.1) vale

$$\vec{v}_H \cdot \vec{\omega} \times (G-H) = \frac{3a^2 \dot{\theta}}{2} [-\dot{\theta} \sin 2\theta \sin \psi + \cos 2\theta \cos \psi \dot{\psi}]$$

Dunque,

$$K = \frac{1}{2} m g a^2 \dot{\theta}^2 + \frac{1}{6} m a^2 [(4 + \sin^2 \psi) \dot{\theta}^2 + \dot{\psi}^2] + \frac{3a^2 \dot{\theta}}{2} [-\sin 2\theta \sin \psi \dot{\theta} + \cos 2\theta \cos \psi \dot{\psi}]$$

$$= m a^2 \left[\left(\frac{31}{6} + \frac{1}{6} \sin^2 \psi - \frac{3}{2} \sin 2\theta \sin \psi \right) \dot{\theta}^2 + \frac{1}{6} \dot{\psi}^2 + \frac{3}{2} \cos 2\theta \cos \psi \dot{\theta} \dot{\psi} \right]$$

$$= \frac{1}{9} m a^2 [\dot{\theta}, \dot{\psi}] \begin{bmatrix} \frac{31}{3} + \frac{1}{3} \sin^2 \psi - 3 \sin 2\theta \sin \psi & \frac{3}{2} \cos 2\theta \cos \psi \\ \frac{3}{2} \cos 2\theta \cos \psi & \frac{1}{3} \end{bmatrix} \begin{bmatrix} \dot{\theta} \\ \dot{\psi} \end{bmatrix}$$

5) Linearizzazione nelle configurazioni di eq. $\vec{q}_e = (\theta_e = -\frac{\pi}{6}, \psi_e = \frac{\pi}{2})$

Poiché la rotazione non è conservativa, dobbiamo usare la formula

$$(13.1) \quad A(\vec{q}_e) \ddot{x} + B \dot{x} + C x = 0 \quad \vec{x} = \vec{q}(t) - \vec{q}_e$$

dove $B_{is} = -\frac{\partial Q_i}{\partial \dot{q}_s} |_{\vec{q}_e} = 0$, $C_{is} = -\frac{\partial^2 Q_i}{\partial q_s^2} |_{\vec{q}_e}$. Quindi

$$(13.2) \quad m a^2 \begin{bmatrix} \frac{2l}{3} + \frac{1}{3} \sin^2 \psi_e - 3 \sin 2\theta_e \sin \psi_e & \frac{3}{2} \cos 2\theta_e \cos \psi_e \\ \frac{3}{2} \cos 2\theta_e \cos \psi_e & \frac{1}{3} \end{bmatrix} = A(\vec{q}_e) = \begin{bmatrix} \frac{32 + 3\sqrt{3}}{3} & 0 \\ 0 & \frac{1}{3} \end{bmatrix} m a^2$$

$$C = - \begin{bmatrix} \frac{\partial^2 Q_\theta}{\partial \theta^2} & \frac{\partial^2 Q_\theta}{\partial \theta \partial \psi} \\ \frac{\partial^2 Q_\psi}{\partial \theta \partial \psi} & \frac{\partial^2 Q_\psi}{\partial \psi^2} \end{bmatrix} |_{\vec{q}_e} = - \begin{bmatrix} +mga \left(\frac{1}{2} \sin 2\theta_e \sin \psi_e + 3 \cos 2\theta_e \right) & -\frac{mga \cos 2\theta_e \cos \psi_e}{2} \\ -6Fa \sin \psi_e \sin 2\theta_e & +3Fa \cos \psi_e \cos 2\theta_e \\ -\frac{mga \cos 2\theta_e \cos \psi_e}{2} & \frac{mga \sin 2\theta_e \sin \psi_e}{2} \end{bmatrix}$$

$$= - \begin{bmatrix} +\frac{mga}{2} \left(-\frac{1}{2} + 3\sqrt{3} \right) + 3\sqrt{3} Fa & 0 \\ 0 & -\frac{mga}{4} \end{bmatrix} = mga \begin{bmatrix} \frac{1}{2} \left(\frac{1 - 3\sqrt{3}}{2} \right) - 3\sqrt{3} \lambda & 0 \\ 0 & +\frac{1}{4} \end{bmatrix}$$

Di qui, tenendo conto che $\lambda = 1 + \frac{1}{2\sqrt{3}}$, si trova

$$m a^2 \begin{bmatrix} \frac{32 + 3\sqrt{3}}{3} & 0 \\ 0 & \frac{1}{3} \end{bmatrix} \begin{bmatrix} \ddot{x}_1 \\ \ddot{x}_2 \end{bmatrix} + mga \begin{bmatrix} -\left(\frac{5}{4} + \frac{9}{2}\sqrt{3} \right) & 0 \\ 0 & +\frac{1}{4} \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} 0 \\ 0 \end{bmatrix}$$

$$\frac{\partial K}{\partial \dot{\theta}} = 2m\alpha^2 \left(\frac{3l}{6} + \frac{1}{6} \sin^2 \psi - \frac{3 \sin 2\theta \sin \psi}{2} \right) \dot{\theta} + \frac{3}{2} \cos 2\theta \cos \psi \dot{\psi}$$

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{\theta}} \right) = 2m\alpha^2 \left(\frac{1}{3} \sin \psi \cos \psi \dot{\psi} - 3 \cos 2\theta \sin \psi \dot{\theta} \frac{3 \sin 2\theta \cos \psi \dot{\psi}}{2} \right) \dot{\theta} +$$

$$+ 2m\alpha^2 \left(\frac{3l}{6} + \frac{1}{6} \sin^2 \psi - \frac{3 \sin 2\theta \sin \psi}{2} \right) \ddot{\theta} +$$

$$+ \left(-3 \sin 2\theta \ddot{\theta} \right) \cos \psi \dot{\psi} - \frac{3}{2} \cos 2\theta \sin \psi \dot{\psi}^2 + \frac{3}{2} \cos 2\theta \cos \psi \ddot{\psi}$$

$$\frac{\partial K}{\partial \theta} = m\alpha^2 \left(-3 \cos 2\theta \sin \psi \dot{\theta}^2 - 3 \sin 2\theta \cos \psi \dot{\theta} \dot{\psi} \right)$$

$$EL_{\theta} = 2m\alpha^2 \left[\left(\frac{1}{3} \sin \psi - \frac{3 \sin 2\theta}{2} \right) \cos \psi \dot{\theta} \dot{\psi} - \frac{3 \cos 2\theta \sin \psi}{2} \dot{\theta}^2 + \right.$$

$$\left. + \left(\frac{3l}{6} + \frac{1}{6} \sin^2 \psi - \frac{3 \sin 2\theta \sin \psi}{2} \right) \ddot{\theta} - \frac{3 \cos 2\theta \sin \psi \dot{\psi}^2 + 3 \cos 2\theta \cos \psi \ddot{\psi}}{4} \right] =$$

$$= -m g \alpha \left(\frac{1}{2} \cos \theta \sin \psi - 3 \sin \theta \right) + 3 F \alpha \sin \psi \cos 2\theta$$

$$\frac{\partial K}{\partial \dot{\psi}} = m\alpha^2 \left[\frac{1}{3} \dot{\psi} + \frac{3}{2} \cos 2\theta \cos \psi \dot{\theta} \right]$$

$$\frac{d}{dt} \left(\frac{\partial K}{\partial \dot{\psi}} \right) = m\alpha^2 \left[\frac{1}{3} \ddot{\psi} + \left(-3 \sin 2\theta \cos \psi \dot{\theta}^2 \right) + 3 \cos 2\theta \left(-\sin \psi \dot{\theta} \dot{\psi} + \cos \psi \ddot{\theta} \right) \right]$$

$$\frac{\partial K}{\partial \psi} = m\alpha^2 \left[\left(\frac{1}{3} \sin \psi \cos \psi - \frac{3 \sin 2\theta \cos \psi}{2} \right) \dot{\theta}^2 - \frac{3}{2} \cos 2\theta \sin \psi \dot{\theta} \dot{\psi} \right]$$

$$EL_{\psi} = m\alpha^2 \left[\frac{1}{3} \ddot{\psi} - \left(\frac{1}{3} \sin \psi - \frac{3 \sin 2\theta}{2} \right) \cos \psi \dot{\theta}^2 + \frac{3 \cos 2\theta \cos \psi}{2} \ddot{\theta} \right] = -m g \alpha \left(\frac{1}{2} \sin 2\theta \cos \psi \right)$$

Quindi, il sistema delle EL linearizzate intorno a $\vec{q}_e = \left(\frac{\pi}{6}, \frac{\pi}{2}\right)$ ¹⁴

$$\left\{ \begin{aligned} m_1 a \left(\frac{32}{3} + \frac{3}{2} \sqrt{3} \right) \ddot{x}_1 - m_1 g \left(\frac{5}{4} + \frac{3}{2} \sqrt{3} \right) x_1 &= 0 \end{aligned} \right.$$

$$\left\{ \begin{aligned} m_1 a \frac{1}{3} \ddot{x}_2 + \frac{m_1 g}{4} x_2 &= 0 \end{aligned} \right.$$

cioè

$$\left\{ \begin{aligned} a \left(\frac{32}{3} + \frac{3}{2} \sqrt{3} \right) \ddot{x}_1 - \frac{g}{2} \left(\frac{5}{2} + 3\sqrt{3} \right) x_1 &= 0 \end{aligned} \right.$$

$$\left\{ \begin{aligned} \frac{a}{3} \ddot{x}_2 + \frac{g}{4} x_2 &= 0 \end{aligned} \right.$$

Scriviamo le 2 ECD, scegliendo come polo per la II il punto $O \in B$

$$(15.1) \begin{cases} \vec{R}^{(ext, ext)} + \vec{\Psi}_A + \vec{\Phi}_B = m \vec{a}_G \\ \vec{H}_O^{(ext, ext)} + (A-B) \times \vec{\Psi}_A = \frac{d\vec{L}_O}{dt} + \vec{v}_O \times \vec{p} \end{cases}$$

Proiettando la I ECD nella base fissa \mathcal{B} , poniamo ricorso subito $\vec{\Psi}_A \cdot \vec{e}_x$ e $\vec{\Phi}_B \cdot \vec{e}_x$.

$$(15.2) \vec{\Psi}_A \cdot \vec{e}_x + \vec{\Phi}_B \cdot \vec{e}_x = m g \vec{e}_z \cdot \vec{e}_x - F \vec{i} \cdot \vec{e}_x + m \vec{a}_G \cdot \vec{e}_x$$

$$(15.3) \vec{\Psi}_A \cdot \vec{e}_y = m g \vec{e}_z \cdot \vec{e}_y - \vec{\Phi}_B \cdot \vec{e}_y + m \vec{a}_G \cdot \vec{e}_y - F \vec{i} \cdot \vec{e}_y$$

$$(15.4) \vec{\Phi}_B \cdot \vec{e}_z = m g \vec{e}_z \cdot \vec{e}_z - \vec{\Psi}_A \cdot \vec{e}_z + m \vec{a}_G \cdot \vec{e}_z - F \vec{i} \cdot \vec{e}_z$$

Quindi, dobbiamo calcolare le componenti di \vec{a}_G in \mathcal{B} .

Facciamolo derivando 2 volte ss. al tempo le (3.6)

$$(15.5) \begin{aligned} \vec{v}_G &= \frac{d}{dt}(G-O) = a \left[-\frac{1}{2} \sin \psi \dot{\psi} \vec{e}_x + \left(-\frac{1}{2} \sin \theta \sin \psi \dot{\theta} + \frac{1}{2} \cos \theta \cos \psi \dot{\psi} + 3 \sin \theta \dot{\theta} \right) \vec{e}_y \right. \\ &\quad \left. + \left(\frac{1}{2} \cos \theta \sin \psi \dot{\theta} + \frac{1}{2} \sin \theta \cos \psi \dot{\psi} - 3 \sin \theta \dot{\theta} \right) \vec{e}_z \right] \\ &= a \left\{ -\frac{1}{2} \sin \psi \dot{\psi} \vec{e}_x + \left[\left(-\frac{1}{2} \sin \theta \sin \psi + 3 \cos \theta \right) \dot{\theta} + \frac{1}{2} \cos \theta \cos \psi \dot{\psi} \right] \vec{e}_y + \right. \\ &\quad \left. + \left[\left(\frac{1}{2} \cos \theta \sin \psi - 3 \sin \theta \right) \dot{\theta} + \frac{1}{2} \sin \theta \cos \psi \dot{\psi} \right] \vec{e}_z \right\} \end{aligned}$$

$$\vec{a}_G = a \left\{ -\frac{1}{2} (\cos \psi \dot{\psi}^2 + \sin \psi \ddot{\psi}) \vec{e}_x + \right. \\ \left. + \left[\left(-\frac{1}{2} (\cos \theta \sin \psi \ddot{\theta} + \sin \theta \cos \psi \dot{\psi}) - 3 \sin \theta \dot{\theta} \right) \ddot{\theta} + \left(-\frac{1}{2} \sin \theta \sin \psi + 3 \cos \theta \right) \ddot{\theta} \right. \right. \\ \left. \left. + \frac{1}{2} (-\sin \theta \cos \psi \ddot{\theta} + \cos \theta \sin \psi \dot{\psi}) \dot{\psi} + \frac{1}{2} \cos \theta \cos \psi \ddot{\psi} \right] \vec{e}_y \right.$$

$$(16.1) \quad \left. + \left[\left(\frac{1}{2} (-\sin \theta \sin \psi \ddot{\theta} + \cos \theta \cos \psi \dot{\psi}) - 3 \cos \theta \dot{\theta} \right) \ddot{\theta} + \left(\frac{1}{2} \cos \theta \sin \psi - 3 \sin \theta \right) \ddot{\theta} \right. \right. \\ \left. \left. + \frac{1}{2} (\cos \theta \cos \psi \ddot{\theta} - \sin \theta \sin \psi \dot{\psi}) \dot{\psi} + \frac{1}{2} \sin \theta \cos \psi \ddot{\psi} \right] \vec{e}_z \right\}$$

$$= a \left\{ -\frac{1}{2} (\cos \psi \dot{\psi}^2 + \sin \psi \ddot{\psi}) \vec{e}_x + \right. \\ \left. + \left[-\left(\frac{1}{2} \cos \theta \sin \psi + 3 \sin \theta \right) \ddot{\theta}^2 - \sin \theta \cos \psi \dot{\theta} \dot{\psi} + \left(-\frac{1}{2} \sin \theta \sin \psi + 3 \cos \theta \right) \ddot{\theta} \right. \right. \\ \left. \left. - \frac{1}{2} \cos \theta \sin \psi \dot{\psi}^2 + \frac{1}{2} \cos \theta \cos \psi \ddot{\psi} \right] \vec{e}_y + \right. \\ \left. + \left[-\left(\frac{1}{2} \sin \theta \sin \psi + 3 \cos \theta \right) \ddot{\theta}^2 + \cos \theta \cos \psi \dot{\theta} \dot{\psi} + \left(\frac{1}{2} \cos \theta \sin \psi - 3 \sin \theta \right) \ddot{\theta} \right. \right. \\ \left. \left. - \frac{1}{2} \sin \theta \sin \psi \dot{\psi}^2 + \frac{1}{2} \sin \theta \cos \psi \ddot{\psi} \right] \vec{e}_z \right\}$$

Inoltre, proiettiamo il carico follower su B

$$\vec{F} \cdot \vec{e}_x = F \vec{c} \cdot \vec{e}_x = F \cos \psi$$

$$\vec{F} \cdot \vec{e}_y = F \vec{c} \cdot \vec{e}_y = F \cos \theta \sin \psi$$

$$\vec{F} \cdot \vec{e}_z = F \vec{c} \cdot \vec{e}_z = F \sin \theta \sin \psi$$

Dunque, le (15.3) e (15.4) forniscono

$$(17.1) \vec{\Psi}_A \cdot \vec{e}_y = ma \left[- \left(\frac{1}{2} \cos \theta \sin \psi + 2 \sin \theta \right) \ddot{\theta}^2 - \sin \theta \cos \psi \dot{\theta} \dot{\psi} + \right. \\ \left. + \left(-\frac{1}{2} \sin \theta \sin \psi + 2 \cos \theta \right) \ddot{\theta} - \frac{1}{2} \cos \theta \sin \psi \dot{\psi}^2 + \frac{1}{2} \cos \theta \cos \psi \ddot{\psi} \right] + \\ - F \cos \theta \sin \psi$$

$$(17.2) \vec{\Phi}_B \cdot \vec{e}_z = mg + ma \left[- \left(\frac{1}{2} \sin \theta \sin \psi + 2 \cos \theta \right) \ddot{\theta}^2 + \cos \theta \cos \psi \dot{\theta} \dot{\psi} + \right. \\ \left. + \left(\frac{1}{2} \cos \theta \sin \psi - 2 \sin \theta \right) \ddot{\theta} - \frac{1}{2} \sin \theta \sin \psi \dot{\psi}^2 + \frac{1}{2} \sin \theta \cos \psi \ddot{\psi} \right] + \\ - F \sin \theta \sin \psi$$

Inoltre, la (15.2) fornisce la somma delle reazioni lungo \vec{e}_x

$$(17.3) (\vec{\Psi}_A + \vec{\Phi}_B) \cdot \vec{e}_x = -\frac{m a \alpha}{2} (\cos \psi \dot{\psi}^2 + \sin \psi \ddot{\psi}) - F \cos \psi$$

Per determinare ognuna delle 2 incognite $\vec{\Psi}_A \cdot \vec{e}_x$, $\vec{\Phi}_B \cdot \vec{e}_x$ dobbiamo usare la II ECD (15.1). Osserviamo che

$$(17.4) (A-B) \times \vec{\Psi}_A = 6a \vec{k} \times (\psi_x \vec{e}_x + \psi_y \vec{e}_y) = \\ = 6a (-\sin \theta \vec{e}_y + \cos \theta \vec{e}_z) \times (\psi_x \vec{e}_x + \psi_y \vec{e}_y) \\ = 6a (\psi_x \sin \theta \vec{e}_z + \psi_x \cos \theta \vec{e}_y - \psi_y \cos \theta \vec{e}_x)$$

Allora, se proiettiamo la II ECD lungo \vec{e}_y , otteniamo

$$(17.5) 6a \cos \theta \psi_x = - (G-B) \times m \vec{g} \cdot \vec{e}_y + \frac{d \vec{L}_B}{dt} \cdot \vec{e}_y + \vec{v}_B \times \vec{p} \cdot \vec{e}_y \quad \vec{v}_B \parallel \vec{e}_y$$

$$- (M-B) \times \vec{F} \cdot \vec{e}_y$$

Il momento delle forze preso a quello del carico follower sono

$$\begin{aligned}
 (G-B) \times m\vec{g} &= \left(\frac{a}{2} \vec{i} + 3a\vec{k} \right) \times (-mg\vec{e}_z) = -mg \left(\frac{a}{2} \vec{i} \times \vec{e}_z + 3a\vec{k} \times \vec{e}_z \right) \\
 &= -mg \left[\frac{a}{2} (\cos\psi \vec{e}_x + \cos\theta \sin\psi \vec{e}_y) \times \vec{e}_z + 3a(-\sin\theta) \vec{e}_y \times \vec{e}_z \right] \\
 &= -mga \left[-\frac{1}{2} \cos\psi \vec{e}_y + \cos\theta \sin\psi \vec{e}_x - 3 \sin\theta \vec{e}_x \right] \\
 &= -mga \left[(\cos\theta \sin\psi - 3 \sin\theta) \vec{e}_x - \frac{1}{2} \cos\psi \vec{e}_y \right]
 \end{aligned}$$

$$(M-B) \times \vec{F} = 3Fa \vec{j} = 3Fa (-\sin\psi \vec{e}_x + \cos\theta \cos\psi \vec{e}_y + \sin\theta \cos\psi \vec{e}_z)$$

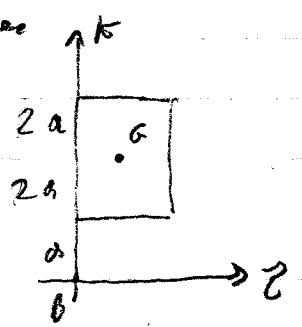
Inoltre

$$\frac{d\vec{L}_B}{dt} \cdot \vec{e}_y = \frac{d}{dt} (\vec{L}_B \cdot \vec{e}_y)$$

$$\vec{L}_B \cdot \vec{e}_y = I_B(\vec{\omega}) \cdot \vec{e}_y + (G-B) \times m \vec{v}_B \cdot \vec{e}_y \quad \vec{v}_B \parallel \vec{e}_y$$

Determiniamo I_B con il Teo di Huygens-Steiner

$$[I_B]^{B''} = [I_G]^{B''} + m \begin{bmatrix} y^2+z^2 & -xy & -xz \\ -xy & x^2+z^2 & -yz \\ -xz & -yz & x^2+y^2 \end{bmatrix}$$



dove con (x, y, z) abbiamo indicato le coordinate di G e. a (B, B'')

$$[I_B]^{B''} = m a^2 \begin{bmatrix} \frac{16}{12} & & \\ & \frac{17}{12} & \\ & & \frac{1}{12} \end{bmatrix} + m \begin{bmatrix} 9a^2 & 0 & -\frac{a \cdot 3a}{2} \\ 0 & \frac{37a^2}{4} & 0 \\ -\frac{3a^2}{2} & 0 & \frac{a^2}{4} \end{bmatrix} = m a^2 \begin{bmatrix} \frac{31}{3} & 0 & -\frac{3}{2} \\ 0 & \frac{37}{4} & 0 \\ -\frac{3}{2} & 0 & \frac{1}{4} \end{bmatrix}$$

Allora

$$I_B(\vec{\omega}) = m a^2 [\vec{i}, \vec{j}, \vec{k}] \begin{bmatrix} \frac{31}{3} & 0 & -\frac{3}{2} \\ 0 & \frac{32}{3} & 0 \\ -\frac{3}{2} & 0 & \frac{1}{3} \end{bmatrix} \begin{bmatrix} \dot{\theta} \cos \psi \\ -\dot{\theta} \sin \psi \\ \dot{\psi} \end{bmatrix} =$$

$$= m a^2 [\vec{i}, \vec{j}, \vec{k}] \begin{bmatrix} \frac{31}{3} \cos \psi \dot{\theta} - \frac{3}{2} \dot{\psi} \\ -\frac{32}{3} \sin \psi \dot{\theta} \\ -\frac{3}{2} \cos \psi \dot{\theta} + \frac{1}{3} \dot{\psi} \end{bmatrix}$$

Quindi,

$$I_B(\vec{\omega}) = m a^2 \left[\left(\frac{31}{3} \cos \psi \dot{\theta} - \frac{3}{2} \dot{\psi} \right) \vec{i} + \left(-\frac{32}{3} \sin \psi \dot{\theta} \right) \vec{j} + \left(-\frac{3}{2} \cos \psi \dot{\theta} + \frac{1}{3} \dot{\psi} \right) \vec{k} \right]$$

$$\stackrel{(3.3)}{=} m a^2 \left[\left(\frac{31}{3} \cos \psi \dot{\theta} - \frac{3}{2} \dot{\psi} \right) (\cos \psi \vec{e}_x + \cos \theta \sin \psi \vec{e}_y + \sin \theta \sin \psi \vec{e}_z) + \right. \\ \left. - \frac{32}{3} \sin \psi \dot{\theta} (-\sin \psi \vec{e}_x + \cos \theta \cos \psi \vec{e}_y + \sin \theta \cos \psi \vec{e}_z) + \right. \\ \left. + \left(-\frac{3}{2} \cos \psi \dot{\theta} + \frac{1}{3} \dot{\psi} \right) (-\sin \theta \vec{e}_y + \cos \theta \vec{e}_z) \right]$$

$$= m a^2 \left[\left(\frac{31}{3} \cos \psi \dot{\theta} - \frac{3}{2} \dot{\psi} \right) \cos \psi + \frac{32}{3} \sin^2 \psi \dot{\theta} \right] \vec{e}_x +$$

$$+ \left[\left(\frac{31}{3} \cos \psi \dot{\theta} - \frac{3}{2} \dot{\psi} \right) \cos \theta \sin \psi - \frac{32}{3} \dot{\theta} \cos \theta \sin \psi \cos \psi - \sin \theta \left(-\frac{3}{2} \cos \psi \dot{\theta} + \frac{1}{3} \dot{\psi} \right) \right] \vec{e}_y$$

$$+ \left[\left(\frac{31}{3} \cos \psi \dot{\theta} - \frac{3}{2} \dot{\psi} \right) \sin \theta \sin \psi - \frac{32}{3} \dot{\theta} \sin \theta \sin \psi \cos \psi + \left(-\frac{3}{2} \cos \psi \dot{\theta} + \frac{1}{3} \dot{\psi} \right) \cos \theta \right] \vec{e}_z$$

$$I_B(\vec{\omega}) \cdot \vec{e}_y = m a^2 \left[\cos \psi \dot{\theta} \left(-\frac{1}{3} \cos \theta \sin \psi + \frac{3}{2} \sin \theta \right) - \left(\frac{1}{3} \sin \theta - \frac{3}{2} \cos \theta \sin \psi \right) \dot{\psi} \right]$$

Da qui,

$$\begin{aligned}
 \frac{d}{dt} (\vec{L}_B \cdot \vec{e}_y) &= - \frac{d}{dt} (\vec{I}_O(\vec{\omega}) \cdot \vec{e}_y) = \\
 &= m a^2 \left[-\sin \psi \dot{\psi} \left(-\frac{1}{3} \cos \theta \sin \psi + \frac{3}{2} \sin \theta \right) + \cos \psi \ddot{\theta} \left(-\frac{1}{3} \cos \theta \sin \psi + \frac{3}{2} \sin \theta \right) + \right. \\
 (20.1) \quad &+ \cos \psi \ddot{\theta} \left(\frac{1}{3} \sin \theta \sin \psi + \frac{3}{2} \cos \theta \cos \psi \dot{\psi} + \frac{3}{2} \cos \theta \ddot{\psi} \right) + \\
 &\left. - \left(\frac{1}{3} \cos \theta \ddot{\theta} - \frac{3}{2} \sin \theta \sin \psi \dot{\theta} + \frac{3}{2} \cos \theta \cos \psi \dot{\psi} \right) \dot{\psi} - \left(\frac{1}{3} \sin \theta + \frac{3}{2} \cos \theta \sin \psi \right) \ddot{\psi} \right] \\
 &= m a^2 \left[\left(\frac{1}{3} \cos \theta (\sin^2 \psi - \cos^2 \psi) - \frac{1}{3} \cos \theta \right) \dot{\psi} \dot{\theta} + \cos \psi \left(\frac{3}{2} \sin \theta - \frac{1}{3} \cos \theta \sin \psi \right) \ddot{\theta} + \cos \psi \left(\frac{1}{3} \sin \theta \sin \psi + \frac{3}{2} \cos \theta \right) \ddot{\psi} \right. \\
 &\quad \left. - \frac{3}{2} \cos \theta \cos \psi \dot{\psi}^2 - \left(\frac{1}{3} \sin \theta + \frac{3}{2} \cos \theta \sin \psi \right) \dot{\psi} \ddot{\psi} \right]
 \end{aligned}$$

Allora, da (17.5) si scrive:

$$\begin{aligned}
 6 \cos \theta \psi_x &= - \frac{m g a \cos \psi}{2} + m a^2 \left[-\frac{1}{3} \cos \theta (\cos 2\psi + 1) \dot{\psi} \dot{\theta} + \cos \psi \left(\frac{3}{2} \sin \theta - \frac{1}{3} \cos \theta \sin \psi \right) \ddot{\theta} \right. \\
 (20.2) \quad &+ \cos \psi \left(\frac{1}{3} \sin \theta \sin \psi + \frac{3}{2} \cos \theta \right) \ddot{\psi} - \frac{3}{2} \cos \theta \cos \psi \dot{\psi}^2 - \left. \left(\frac{1}{3} \sin \theta + \frac{3}{2} \cos \theta \sin \psi \right) \dot{\psi} \ddot{\psi} \right]
 \end{aligned}$$

Quindi, se $\cos \theta \neq 0 \Leftrightarrow \theta \neq \pm \pi/2$, si trova

$$\begin{aligned}
 (20.3) \quad \psi_x &= - \frac{m g}{12} \frac{\cos \psi}{\cos \theta} + \frac{m a}{6 \cos \theta} \left[-\frac{1}{3} \cos \theta (1 + \cos 2\psi) \dot{\psi} \dot{\theta} + \cos \psi \left(-\frac{1}{3} \cos \theta \sin \psi + \frac{3}{2} \sin \theta \right) \ddot{\theta} \right. \\
 &+ \left. \left(\frac{1}{6} \sin \theta \sin 2\psi + \frac{3}{2} \cos \theta \right) \ddot{\psi} - \frac{3}{2} \cos \theta \cos \psi \dot{\psi}^2 - \left(\frac{1}{3} \sin \theta + \frac{3}{2} \cos \theta \sin \psi \right) \dot{\psi} \ddot{\psi} \right] + \\
 &= \frac{1}{2} F a \cos \psi.
 \end{aligned}$$

Sostituendo nella (17.3), otteniamo

$$\begin{aligned}
 (20.4) \quad \phi_x &= - \frac{m a}{2} (\cos \psi \dot{\psi}^2 + \sin \psi \ddot{\psi}) + \frac{m g}{12} \frac{\cos \psi}{\cos \theta} + \\
 &- \frac{m a}{6} \left[\frac{2}{3} \cos^2 \psi \dot{\theta} \dot{\psi} + \cos \psi \left(-\frac{1}{3} \sin \psi + \frac{3}{2} \tan \theta \right) \ddot{\theta} + \frac{1}{6} \left(\tan \theta \sin 2\psi + \frac{3}{2} \right) \ddot{\psi} - \frac{3}{2} \cos \psi \dot{\psi}^2 + \right. \\
 &\quad \left. - \left(\frac{1}{3} \tan \theta + \frac{3}{2} \sin \psi \right) \dot{\psi} \ddot{\psi} \right] + \frac{1}{2} F a \cos \psi
 \end{aligned}$$