

MECCANICA Razionale

Corpo rigido \rightarrow 6 gradi di libertà $\underline{R^3}$



$$\frac{x}{p} = \frac{x_0}{p} + R \cdot \frac{X_p}{p}$$

\uparrow \uparrow
 (x_0, y_0) φ

Coordinate libere

↳ vincoli (obblighi)

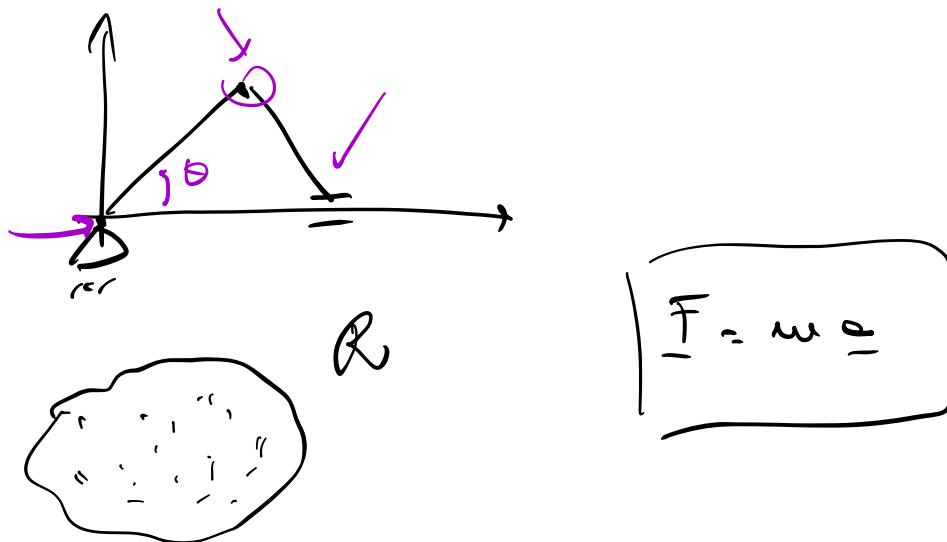
$$f(q_1, \dots, q_n) = 0$$

$$\left[f(x_0, y_0, \varphi) = 0 \right]$$

$$d_0 = 1 - x_0, y$$

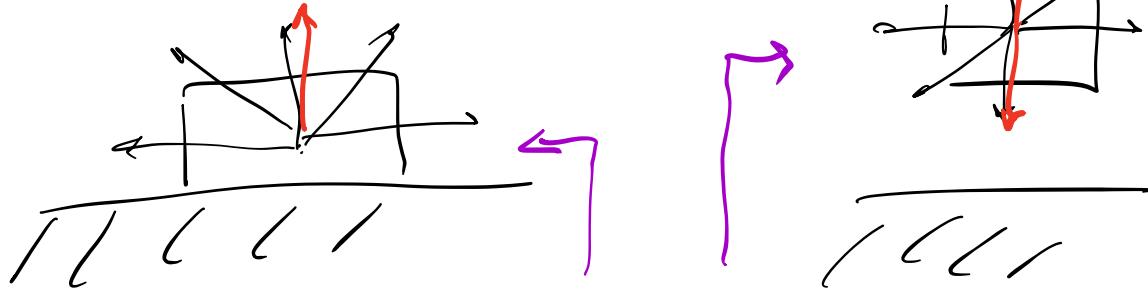
→ Sommoposizione dei Vincoli

→ Sistemi articolati



Principio dei lavori virtuali.

Spontaneo virtuale



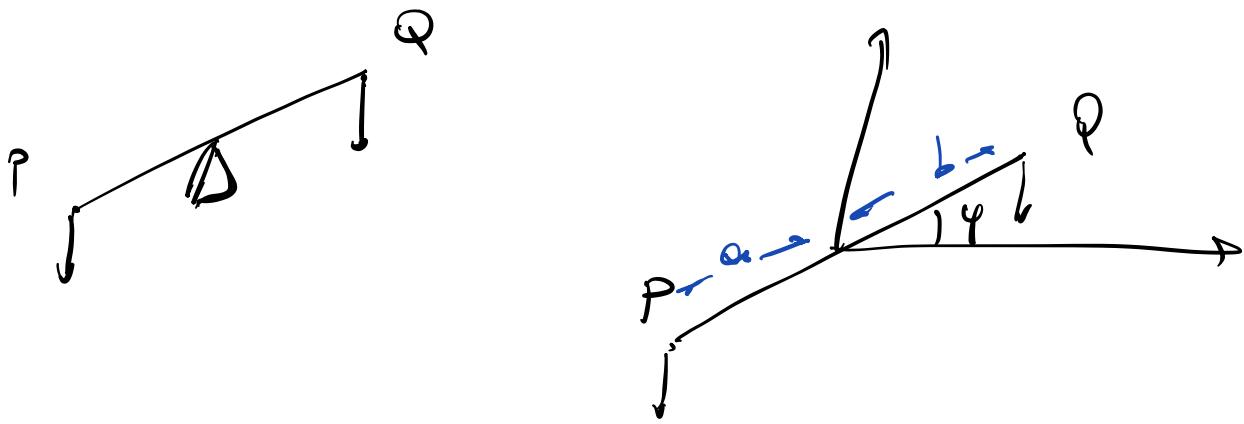
$$\delta x_B$$



invertito (- δx_B)

PLV : $\sum B F_B \cdot \delta x_B \leq 0$
(= 0)

\Leftrightarrow equilibrio



$$\delta x_Q = (-b \sin \varphi \xi_1 + b \cos \varphi \xi_2) \delta \varphi$$

$$\delta x_P = (a \sin \varphi \xi_1 - a \cos \varphi \xi_2) \delta \varphi$$

LV $\underline{F}_P \cdot \delta x_P + \underline{F}_Q \cdot \delta x_Q = \dots$

$$= (-q b \cos \varphi + p a \cos \varphi) \boxed{\delta \varphi} \quad \text{invariante}$$

$$p a \cos \varphi < q b \cos \varphi$$

Reihe:

S Systeme abweichen

B punts die auf die Schiene
feste aktive $\underline{F}_B^{\text{active}}$

δx_B spontaneit. virtuali (= spontanei linearizzati concernenti i vincoli)

Equilibrio di S $\Leftrightarrow \sum_{B \in S} F_B^{\text{attive}} \cdot \delta x_B = 0$

per ogni istante
di δx_B virtuali
(invertibili)

$$x_Q(\varphi) = b \cos \varphi \ \xi_1 + b \sin \varphi \ \xi_2$$

$$x_Q(\varphi + \delta\varphi) = \dots$$

$$\delta x_Q = x_Q(\varphi + \delta\varphi) - x_Q(\varphi)$$

$\delta\varphi$

$$= x_Q(\varphi) + \underset{\text{primo ordine}}{+} \underset{\text{secondo ordine}}{+} \dots$$

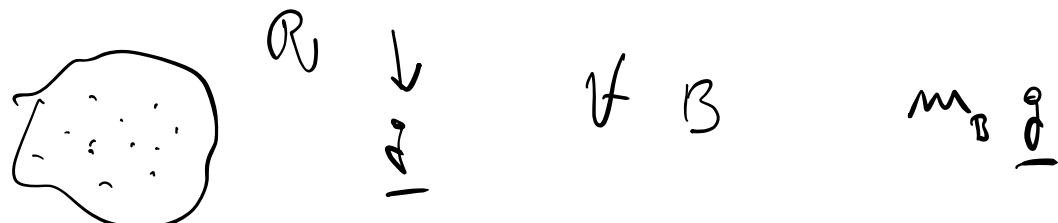
$$- x_Q(\varphi)$$

Irreversibile

$$\delta x_Q = \frac{d x_Q}{d \varphi} \delta \varphi \quad \equiv \text{linearizzato}$$

Sistemi materiali soggetti al solo peso

S risente punti materiali



$$LV = \sum_{B \in S} m_B g \cdot \delta x_B =$$

$$\left[\int \int \rho(x) \dots \right]$$

$$LV = (\) \underbrace{\delta q_1}_{=0} + () \underbrace{\delta q_2}_{=0} + \dots$$

$$= \sum_{B \in S} m_B g \cdot \delta x_B = g \cdot \left(\sum_{B \in S} m_B \delta x_B \right)$$

$$= g \cdot \left(\sum_{B \in S} \delta(m_B x_B) \right)$$

$$= \underline{g} \cdot \delta \left(\sum_B m_B x_B \geq 0 \right)$$

$$\Gamma \quad M = \sum_{B \in S} m_B$$

$$x_G = \frac{\sum_{B \in S} m_B x_B}{M}$$

$$= \underline{g} \cdot \delta (M x_G)$$

$$= M \underline{g} \cdot \delta x_G$$

$$\Rightarrow LV = \sum_{B \in S} m_B \underline{g} \cdot \delta x_B = M \underline{g} \cdot \delta x_G$$

Principio dei lavori virtuali per

sistemi avendo uno stato di liberar

S , virtuali obietti , bloccati , lasci

+ grado di libertà \rightarrow q

$$x_B = x_B(q)$$

$\forall B \in S$

↑
funzione
regolare \Rightarrow $\delta x_B(q) := \frac{dx_B(q)}{dq} \delta q$

\rightarrow spontaneo virtuale
invertibile

F_B^* \rightarrow lo risultato delle forze
attive in T

$$\text{LV} = \sum_{B \in S} F_B^* \cdot \delta x_B =$$

$$= \sum_{B \in S} F_B^* \cdot \frac{dx_B}{dq} \delta q$$

$$= \left(\sum_{B \in S} F_B^* \cdot \frac{dx_B}{dq} \right) \delta q$$

$$= Q \delta q$$

$$Q := \sum_{B \in S} F_B^a \cdot \frac{d x_B}{d q}$$

Forze
generatrici
relative
a q

$$PLV \quad LV = \sum_{B \in S} F_B^a \cdot \underline{dx_B} = 0$$

$$Q \underline{dq} = 0$$

Tutti gli iposposti
virtuali dicono

che \underline{dq}

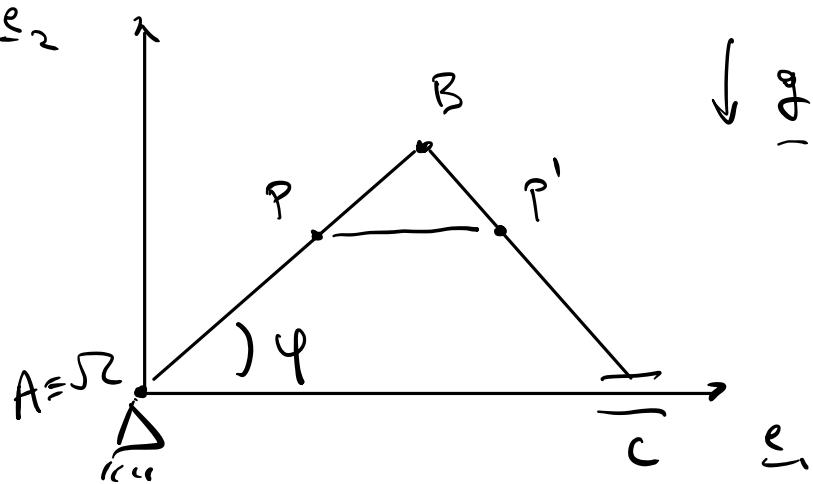
Condizione
di equilibrio $\Leftrightarrow Q = 0$

$$Q = p_a \cos \varphi - q \dot{\theta} \cos \varphi$$

esempio sopra.

Esempio Problema diretto in statica:

dato l'equilibrio determinare le
forze che lo costituiscono.



due arc zifide
 $\overline{AB} = \overline{BC}$
 soggette al peso
 all' eq. $\varphi = \alpha$

Quale è la Tensione delle fune
 per ottenere eq. per α

$$\underline{T} = \textcircled{\underline{T}} (\underline{x}_{P'} - \underline{x}_P)$$

fondo in
 P

$$\tau > 0$$

Principio di azione & reazione: in
 P' la fune esercita una forza $-\underline{T}$

Dati: $\overline{AB} = \overline{BC} = l$ omogenee

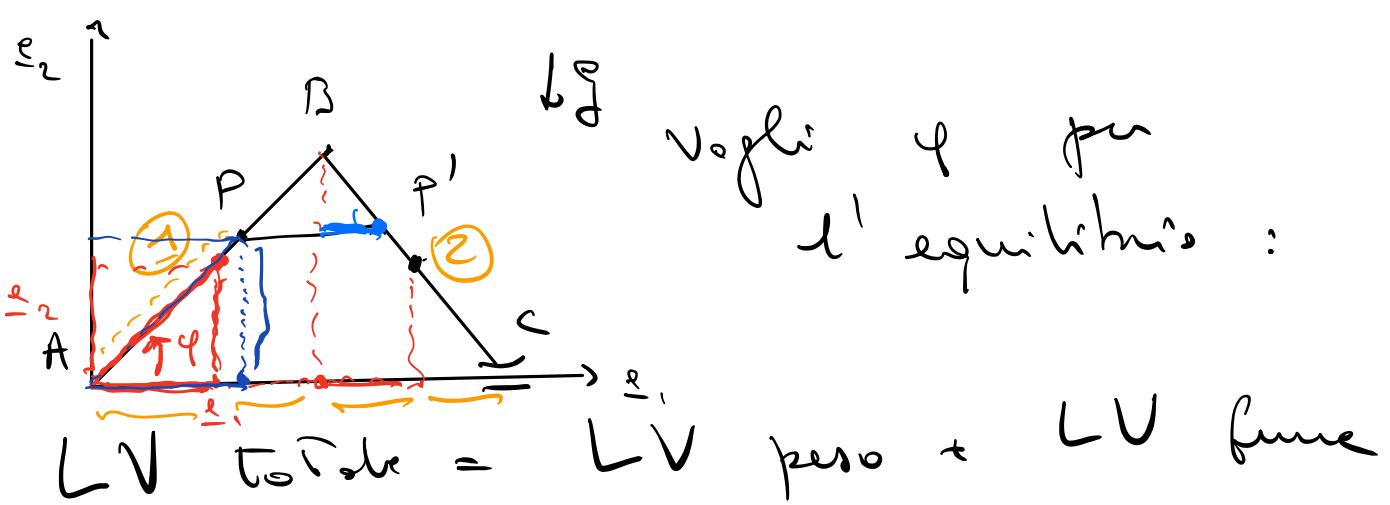
$$m_{AB} = 2 m_{BC} = 2 \underline{m}$$

$$m_{BC} = \underline{m}$$

$$\overline{BP} = \overline{B P'} = \frac{2}{3} l$$

$$\overset{\wedge}{BAC} = \alpha = \frac{\pi}{3}$$

$$\overline{AP} = \overline{P'C} = \frac{1}{3} l$$



$$\underline{x}_{G_1} = \underbrace{\frac{l}{2} \cos \varphi \underline{x}_1 + \frac{l}{2} \sin \varphi \underline{x}_2}$$

$$\underline{x}_{G_2} = \underbrace{\left(l \cos \varphi + \frac{l}{2} \cos \varphi \right)}_{\frac{3}{2} l \cos \varphi} \underline{x}_1 + \frac{l}{2} \sin \varphi \underline{x}_2$$

$$\underline{x}_P = \frac{1}{3} l \cos \varphi \underline{x}_1 + \frac{1}{3} l \sin \varphi \underline{x}_2$$

$$\underline{x}_{P'} = \left(l + \frac{2}{3} l \right) \cos \varphi \underline{x}_1 + \frac{1}{3} l \sin \varphi \underline{x}_2$$

$$\text{LV}_{\text{peso}} = m_{AB} \underbrace{g \underline{x}_2}_{\perp} \cdot \delta \underline{x}_{G_1} + m_{BC} \underbrace{g \underline{x}_1}_{\perp} \cdot \delta \underline{x}_{G_2}$$

$$= m_{AB} \left(- g \underbrace{\underline{x}_2}_{\perp} \right) \cdot \delta \left(\frac{l}{2} \cos \varphi \underline{x}_1 + \frac{l}{2} \sin \varphi \underline{x}_2 \right)$$

$$+ m_{BC} \left(- g \underbrace{\underline{x}_2}_{\perp} \right) \cdot \delta \left(\frac{3}{2} l \cos \varphi \underline{x}_1 + \frac{l}{2} \sin \varphi \underline{x}_2 \right)$$

$$\underline{e}_1 \cdot \underline{e}_2 = 0 \quad \underline{e}_1 \cdot \underline{e}_1 = 1$$

$$\underline{e}_2 \cdot \underline{e}_2 = 1$$

$$= -g(m_{AB} + m_{BC}) \underline{e}_2 \cdot \delta\left(\frac{l}{2} \sin \varphi\right) \underline{e}_2$$

$$= -g 3m \left[\frac{l}{2} \cos \varphi \right] \delta \varphi$$

$$\Delta V_{\text{pero}} = -g \frac{3}{2} m l \cos \varphi \delta \varphi$$

$$\Delta V_{\text{free}} = \overline{I} \cdot \delta \underline{x}_p + (-\overline{I}) \cdot \delta \underline{x}_{p'}$$

$$= \overline{I} \cdot (\delta \underline{x}_p - \delta \underline{x}_{p'}) =$$

$$= \overline{I} (\underline{x}_{p'} - \underline{x}_p) \cdot (\delta \underline{x}_p - \delta \underline{x}_{p'})$$

$$\underline{x}_p = \frac{1}{3} l \cos \varphi \underline{e}_1 + \frac{1}{3} l \sin \varphi \underline{e}_2$$

$$\delta \underline{x}_p = -\frac{1}{3} l \sin \varphi \delta \varphi \underline{e}_1 + \frac{1}{3} l \cos \varphi \delta \varphi \underline{e}_2$$

$$\underline{x}_{p'} = \left(l + \frac{2}{3} l \right) \cos \varphi \underline{e}_1 + \frac{1}{3} l \sin \varphi \underline{e}_2$$

$$\delta \underline{x}_{p'} = -\frac{5}{3} l \sin \varphi \delta \varphi \underline{e}_1 + \frac{1}{3} l \cos \varphi \delta \varphi \underline{e}_2$$

$$\underline{x}_p \cdot \underline{d}\underline{x}_{p'} = \left(-\frac{5}{9} + \frac{1}{9} \right) \underline{l}^2 \cos \varphi \sin \varphi \delta \varphi$$

$$\underline{x}_p \cdot \underline{d}\underline{x}_p = \left(-\frac{1}{9} + \frac{1}{9} \right) \underline{l}^2 \cos \varphi \sin \varphi \delta \varphi$$

$$\underline{x}_{p'} \cdot \underline{d}\underline{x}_{p'} = \left(-\frac{25}{9} + \frac{1}{9} \right) \underline{l}^2 \cos \varphi \sin \varphi \delta \varphi$$

$$\underline{x}_p \cdot \underline{d}\underline{x}_p = (\) \underline{\varepsilon}_1 \cdot \underline{\varepsilon}_1 + (\) \cancel{\underline{\varepsilon}_1 \cdot \underline{\varepsilon}_2} +$$

$$+ (\) \cancel{\underline{\varepsilon}_2 \cdot \underline{\varepsilon}_1} + (\) \underline{\varepsilon}_2 \cdot \underline{\varepsilon}_2$$

$$= -\frac{5}{3} \underline{l}^2 \frac{1}{3} \cos \varphi \sin \varphi \delta \varphi + \frac{1}{9} \underline{l}^2 \sin \varphi \cos \varphi \delta \varphi$$

$$= -\frac{4}{9} \underline{l}^2 \cos \varphi \sin \varphi \delta \varphi$$

$$\tau (\underline{x}_p \cdot \underline{d}\underline{x}_p - \underline{x}_p \cdot \underline{d}\underline{x}_{p'} - \underline{x}_{p'} \cdot \underline{d}\underline{x}_p + \underline{x}_{p'} \cdot \underline{d}\underline{x}_{p'})$$

$$= (\underline{x}_{p'} - \underline{x}_p) \cdot (\underline{d}\underline{x}_p - \underline{d}\underline{x}_{p'}) =$$

$$= -\left(-\frac{4}{9} + \frac{25}{9} - \frac{4}{9} \right) \underline{l}^2 \cos \varphi \sin \varphi \delta \varphi$$

$$= \tau - \frac{16}{9} l^2 \cos \varphi \sin \varphi \dot{\varphi}$$

$$LV_{\text{ext}} = \left(-\frac{3}{2} mg l \cos \varphi + \tau \frac{16}{9} l^2 \cos \varphi \sin \varphi \right) \dot{\varphi}$$

$$= Q(\varphi) \dot{\varphi}$$

$$Q(\varphi) = \left(-\frac{3}{2} mg + \frac{16}{9} l \tau \sin \varphi \right) + \cos \varphi$$

dato $\varphi = \frac{\pi}{3}$ di eq. , qual è vede
 τ ?

$$Q\left(\frac{\pi}{3}\right) = 0 \Rightarrow$$

$$\left(-\frac{3}{2} mg + \frac{16}{9} l \tau \sin \frac{\pi}{3} \right) \underbrace{l \cos \frac{\pi}{3}}_{\neq 0} = 0$$

$$\frac{16}{9} l \tau \sin \frac{\pi}{3} = \frac{3}{2} mg$$

$$\boxed{\tau = \frac{3}{2} mg \quad \frac{9}{16} \frac{l}{\ell} \sqrt{3}}$$

Principio dei buoni viziosi per sistemi a l gradi di libertà

$$\underline{q} = (q_1, \dots, q_l)$$

$$\underline{x}_B(\underline{q}) = x_B(q_1, \dots, q_l)$$

$$\delta x_B(q_1, \dots, q_l)$$

$$x_B(\underline{q} + \delta \underline{q}) = x_B(\underline{q}) + \sum_{i=1}^l \left(\frac{\partial}{\partial q_i} x_B(\underline{q}) \right) \cdot \delta q_i$$

+ Termini
di ordine superiore

$$x_B(\underline{q} + \delta \underline{q}) - x_B(\underline{q}) = \sum_{i=1}^l \left(\frac{\partial}{\partial q_i} x_B(\underline{q}) \right) \delta q_i$$

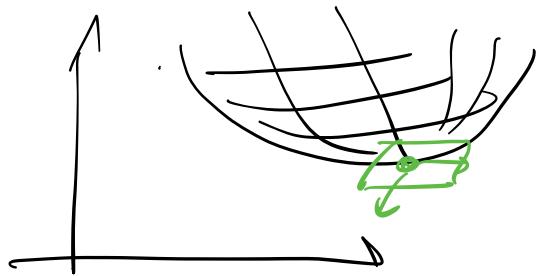
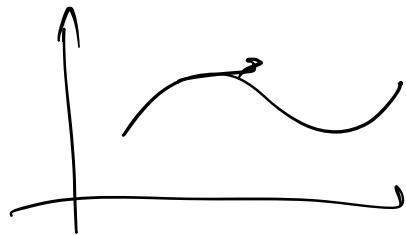
↑ al primo ordine

ad esempio

$$x_B(q_1 + \delta q_1, q_2, \dots, q_l) - x_B(q_1, q_2, \dots, q_l)$$

+ +

$$= \frac{\partial}{\partial q_i} \Sigma_B \delta q_i + \text{ordine superiore}$$



$$\mathcal{L}V = \sum_{B \in S} F_B^e \cdot \delta x_B = \sum_{B \in S} F_B^e \cdot \left(\sum_{i=1}^l \frac{\partial x_B}{\partial q_i} \delta q_i \right)$$

$$= \sum_{i=1}^l \left(\sum_{B \in S} F_B^e \cdot \frac{\partial x_B}{\partial q_i} \right) \delta q_i$$

$\overbrace{\hspace{10em}}$ $=: Q_i$

$$= \sum_{i=1}^l Q_i \delta q_i$$