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INDUSTRIAL PLANTS II

Chapter two ó part 3 Maintenance of Industrial Plants Maintenance Policies

DOUBLE DEGREE MASTER IN õPRODUCTION ENGINEERING AND MANAGEMENTÖ

> CAMPUS OF PORDENONE UNIVERSITY OF TRIESTE



BRIEF HISTORY OF MAINTENANCE



CORRECTIVE MAINTENANCE





BRIEF HISTORY OF MAINTENANCE











MAINTENANCE POLICIES





- ⁷ The maintenance activity is carried out only when the unit reaches a state of critical deterioration such as to interrupt functionality.
- If the system has two operating states (faulty and functioning), this type of maintenance is performed only when the fault state occurs..
- The costs associated with using the system over a useful life span are function of the probabilities of state transition. Ccm = f()





- ^{\sim} We suppose to have a batch of all the same elements, subject to wear, with a probability distribution of normal or Gaussian type failure, which is characterized by an average time between MTBF₀ faults and a σ_0 dispersion.
- ^{\sim} If only the non-functioning elements are replaced (most of the breakages will occur around MTBF₀), the new devices, while mixing with the previous ones, belong to another lot with higher MTBF₁ and higher dispersion σ_1 .
- ^{*x*} Subsequently, some surviving devices of both the first and second generation fail, a third generation must be introduced which will transform the previous batch into one with a higher MTBF₂ and higher σ_2 , and so on and on.

 $MTBF_0 < MTBF_1 < MTBF_2$

 $\sigma_0 < \sigma_1 < \sigma_2$







PROCEDURE

		Work instructions		Workflow				
				Workshop	Maintenance	Spare Part	Maintenance	
		Activity	Operator	supervisor	Planning Dept.	Warehouse	technician	
	1	Breakdown						
	2	warning n. 1						
	3	warning n. 2		L				
	4	Priority evaluation						
	5	Decision to repair						
	6	to the machine						
	7	Failure analisys						
	9	Root cause						
	10	Disassembly						
	11	Part removal					└╺┝┣╪═┤	
		Movement to spare part						
	12	Warehouse						
	13	spare part pick-up						
		Movement from spare part						
	14	Warehouse						
	15	Part replacement					<u>」</u> ┌─ ₽ ┥─┘	
	16	Assembly						
	17	Testing						
Materiale riservato					10			

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WHEN IS IT SUITABLE TO USE CORRECTIVE MAINTENANCE?

Mainly when:

- 1) System and its components have a decreasing failure rate, like in the infant mortality phase (defects of design, manufacture, assembly, start-up or operation)
- 2) the failures are easily repairable and the machine stop does not provoke sensible damage to the general output of the production operations
- 3) There are the possibility to duplicate the machines inside the same process. In this way, if one machine stops, its role in the production process can be done by another asset.



WHEN IS IT SUITABLE TO USE CORRECTIVE MAINTENANCE?

Possible negative points:

- 1) Loss of profit for medium/long time stops due to machines breakdowns
- 2) Problems to organize an alternative material flow in case of breakdowns
- 3) The cumulative repair costs could become high because the failure or bad performance of a component for a long time can damage some more component of the machine.



Summary

OBJECTIVES	TOOLS	PARAMETERS	TRENDS
	INTERVENTION SPEED	MEAN TIME OF	
	DIAGNOSYS SPEED	INTERVENTION	Ļ
REDUCTION OF FAILURE	ACTION SPEED	MEAN TIME TO	
MACHINE)	SPARE PARTS AVAILABILITY	REPAIR	Ļ
	MODIFICATIONS		1
	IMPROVEMENT		
FREQUENCY	TRAINING	FAILURE	
	PLANT FLEXIBILITY		
	REDUNDANT SYSTEMS		
COSTS	FINISHED PRODUCTS INVENTORIES	MAINTENANCE	







MAINTENANCE STRATEGIY





AT CONSTANT AGE



In constant age preventive maintenance, the replacement operation takes place after the component or system has reached a certain operating time T (preventive replacement age) or before that age in case of failure (Corrective Maintenance).

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- Preventive maintenance is scheduled in order to limit the casual behavior of the system.
- ["] The level of system reliability varies over time according to a certain distribution of probability and with a predetermined frequency and by this activity the system is brought back to a better state of functionality because we assume (classical theory) that the preventive maintenance brings the state of the system back to a "good as new" condition.
- In other words, we assume that all the properties of the system are restored as new, that is, to restore the original distribution of probability of failure. Possible actions may be the replacement of components before the failure. The aim is to reduce the probability of failure with an associated cost recovery over the useful life of the system.



AT CONSTANT AGE

It is assumed that the following hypotheses will be satisfied:

- The average preventive maintenance time of the system is very short compared with the average time to failure and therefore can be neglected
- ["] Regardless of the maintenance policy, failures will occur according to a certain distribution function.
- The equipment can be considered "as good as new" after the intervention of corrective / preventive maintenance
- ["] The period T must be chosen so that within T there can be at most one failure only.
- ["] The cost of preventive maintenance must be less than the cost of maintenance corrective, because otherwise a preventive action would be useless.
- Once restored / replaced, the entity always follows the same law of reliability R (T) while, when the failure occurs, productivity is 0
- The state of the component or system does not present the possibility of a progressive decline in its performance, but only considers the two extreme states (functioning or broken)



AT CONSTANT AGE

Let suppose that:

 $N_{c}(t)$ = number of failures in the interval (0, t);

 $N_{p}(t)$ = number of preventive maintenance interventions in the interval (0, t);

- C_c = cost of a corrective maintenance intervention (emergency intervention) "/intervention, which takes into account both the replacement cost and the ones provokes by the the unit stop;
- C_p = cost of a preventive maintenance intervention with replacement of the unit without the event of failure) "/intervention;

T = Preventive Maintenance Time Cycle).T [1, 22 22]

22 22 = Maximum Preventive Maintenance Time Cycle, where the unit is operating without failure

2* = Optimal Period of Preventive Maintenance optimizing the pertinent Maintenance cost

222 (2) = Expected Cost Maintenance Per Period

222 2* (2) = optimal Expected Cost Maintenance Per Period

②(②) = Function of Density of Probability of failure

 $\mathbb{Q}(\mathbb{Q}) = \text{Unreliability at time T}(\text{Cumulative probability of failure }\mathbb{Q}(\mathbb{Q}))$

 $\mathbb{Q}(\mathbb{Q}) = \text{Reliability at T time } (1 \mathbb{Q}(\mathbb{Q}))$

2 (2)= Expected time of maintenance cycle if we do corrective maintenance due to a failure within 0 and T

???????????????Mean time between maintenance



PREVENTIVE MAINTENANCE AT CONSTANT AGE

Therefore we use the model to determine the optimal time T* that minimizes the maintenance costs 22 2* (2). The mean time before maintenance cycle when T varies can be calculated as follows:

????(?) = ?(?) * ? + ?(?) * ? (?)

Where:

- R (T): represents the probability that age T is reached without the occurrence of a fault and therefore represents the probability of carrying out a regular preventive replacement
- F (T): represents the probability that age T is not reached and therefore the probability of carry out corrective maintenance
- T: Time of the maintenance cycle if preventive maintenance is performed

M(T): Expected time of maintenance cycle if we are forced to perform corrective maintenance due to a failure in the interval (0, T] 20



PREVENTIVE MAINTENANCE AT CONSTANT AGE

????(?) = ?(?) * ? + ?(?) * ? (?)

Let B calculate the value of 2 (2)

And, substituting M(T), we get

? ????(?) = ?(?) * ? + ¶? * ?(?)?t 0

Where the integrals are between 0 and T



iaintenance multiplied by the probability of the failure occurs before 1, plus the cost of preventive maintenance by the

AT CONSTANT AGE

After defining MTBM(T), we have to define the cost function ECMP(T) Expected Cost Maintenance Per Period.

??*?(?)+??*?(?)
(?)?*?(?)
(?)????(?)

That is, ECMP(T) will be the cost of corrective maintenance multiplied by the probability of the failure occurs before T, added to the cost of preventive maintenance by the probability that the entity survives until time T. The whole is divided by the expected duration of the cycle of maintenance. Then for each T [1, Tmax], MTBM (T) and the pertinent ECMP (T) are calculated, and as in the case of preventive maintenance on a constant date, the optimum age T * which minimizes the ECMP*(T*) is found.

The ECMP (T) function should be a convex function, which first decreases to T * and then increases to Tmax. In case it is a function monotone decreasing of ECMP (T), the meaning is that we do not need any preventive maintenance but corrective maintenance because it is more convenient in terms of Materiale riservato Raffaele Campanella costs



will be a cost of corrective maintenance multiplied by the probability of the failure occurs before 1, plus the cost of preventive maintenance by the probability that the en

PREVENTIVE MAINTENANCE AT CONSTANT AGE

2?? 2(?) = [?? * 2(?) + ?? * 2(?)] / ? ??? (?)

Consider a component of a system having a failure probability density f(t) uniformly distributed between 0 and 8 weeks:

$$f(t) = \begin{cases} \frac{1}{8} & (0 \le t \le 8) \\ 0 & \text{otherwise} \end{cases}$$

Furthermore, the costs of intervention are known:

- estimate: C_p = 10 kÖintervention

- on failure: $\dot{C}_c = 50$ kÖintervention



PREVENTIVE MAINTENANCE AT CONSTANT AGE ?????(?) = ??*?(?) + ??*?(?) / ?????(?)

Consider a component of a system having a failure probability density f(t) uniformly distributed between 0 and 8 weeks:

Note the expression of f(t) we get:
$$f(t) = \begin{cases} \frac{1}{8} & (0 \le t \le 8) \\ 0 & \text{otherwise} \end{cases}$$

- probability of failure

$$F(t) = \begin{cases} \int_0^t \frac{1}{8} dt = \frac{1}{8} t & (0 \le t \le 8) \\ 1 & t > 8 \end{cases}$$

$$R(t) = 1 - F(t) = \begin{cases} 1 - \frac{1}{8} t & (0 \le t \le 8) \\ 0 & t > 8 \end{cases}$$

$$\lambda(t) = \frac{f(t)}{R(t)} = \frac{\frac{1}{8}}{1 - \frac{1}{8}t} = \frac{1}{8 - t}$$





AT CONSTANT DATE

If we decide to implement a constant date preventive maintenance strategy, the system will be subjected to preventive maintenance every period T, and corrective maintenance every time a failure occurs within the interval T, as shown in the figure below. This maintenance policy consists of the systematic replacement of the component or system at a pre-established deadline, regardless of the age of the same, or at the time of its failure This model determines the optimal T* interval of preventive intervention that minimizes the maintenance cost (ECMP





AT CONSTANT DATE

We give for granted the following assumptions:

i The average preventive maintenance time is very short compared to the average failure time and therefore can be neglected.

i The equipment can be considered "as good as new" after corrective / preventive maintenance

; The period T must be chosen so that within T a single fault can occur at most.

The cost of preventive maintenance must be less than the cost of corrective maintenance, because otherwise a preventive action would be useless.

; Once restored / replaced, the entity always follows the same law of reliability R (T)

["] Only two states are considered (functioning or broken) and when the failure occurs, productivity is 0

Availability of continuous information on the status of the component or system;
 and the label



AT CONSTANT DATE

Let suppose that:

H(t) = Expected number of failures in the interval (0, t);

C_c = cost of a corrective maintenance intervention (emergency intervention) "/intervention, which takes into account both the replacement cost and the ones provokes by the the unit stop;

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- ②(②) = Function of Density of Probability of failure
- $\mathbb{Q}(\mathbb{Q}) =$ Unreliability at time T(Cumulative probability of failure $\mathbb{Q}(\mathbb{Q})$)
- $\mathbb{Q}(\mathbb{Q}) = \text{Reliability at T time} (1 \mathbb{Q}(\mathbb{Q}))$



PREVENTIVE MAINTENANCE AT CONSTANT DATE

First of all, we need to define a function that determines the expected cost for each maintenance interval T:

?????(?) = [?? + ?? * ? (?)] / ?

That is, the expected cost for period T can be determined as the cost of preventive maintenance, added to the cost of corrective maintenance for the **number of failures that occurred in the interval (0, T]**. Once the cost function has been described, the following step is to determine the expected number of failures in the cyclic maintenance period T as follows:

$$\mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}_{i=0}^{T-1} = \begin{bmatrix} 1 + \mathbb{P}_{i=0} \\ \mathbb{P}_{i=0} \end{bmatrix} \mathbb{P}$$



PREVENTIVE MAINTENANCE AT CONSTANT DATE

Therefore for each period T [1, Tmax], the expected number of failures H (T) is calculated, and knowing the costs 22 and 22 it is possible to calculate the expected maintenance cost for each ECMP maintenance cycle (T). The optimal period T *, corresponds to the period where the ECMP (T) is minimum.

In general the ECMP (T) depends on the costs 22 and 22 and also on the probability density function 2 (2). Once all ECMPs have been computed for T [1, Tmax], the function should be a convex function, which first decreases to T * and then increases to Tmax.

In the event of a monotonous decreasing function, the model foresees that no preventive maintenance is necessary but corrective maintenance is more convenient in terms of costs.



AT A DETERMINED LEVEL OF RELIABILITY

In this policy, maintenance activities are carried out when the probability of breakdowns falls below a predetermined level.

The periods of preventive replacement are determined starting from the cumulative distribution of probability of failure.

This maintenance policy is mainly aimed at ensuring high levels of reliability, as well as the safety of the system used (figure)





AT A DETERMINED LEVEL OF RELIABILITY

This maintenance is applied to those components where reliability and safety are predominant with respect to the economic criteria.

If the system consists of a batch of equal components, characterized by a normal or Gaussian type of density of probability of failure f(t), a maximum value of the probability of failure is established a priori and, consequently, a minimum reliability value not to be overcome.

Once this limit has been reached and, consequently, the optimal intervention interval has been determined, the whole lot is replaced with an identical one.

If the characteristics of the lots do not change as they are replaced, the intervention interval is defined by the systematic analysis on the probability density.



AT A DETERMINED LEVEL OF RELIABILITY

This maintenance strategy implies the possibility to act deeply in the design of the machine in order to improve the adherence to the Customer^B needs and minimize the quality problems.

Many times they are caused by the misuse done by the Customers because the performances are not according the expectations.

QUALITY FUNCTION DESIGN, FMEA and FTA are the most used techniques to act preventively on the technical specifications of the products



QUALITY FUNCTION DEPLOYMENT

- Late 1960s: Shigero Mizuno Ë Yoji Akao first development
- First large scale application Bridgestone (fishbone)
- 1970 Kobe Shipyards Ë House of Quality
- 1970s Ë Japanese Car manufacturers and other industries
- 1985 Ë first applications in the USA
- 1990s Ë large application in the USA and first applications in Europe



QUALITY FUNCTION DEPLOYMENT

OVERALL OBJECTIVE

The purpose of **QUALITY FUNCTION DEPLOYMENT** is to develop a quality assurance method that would design customer satisfaction into a product *before* it is manufactured.

Before QFD, quality control methods were primarily aimed at fixing a problem during or after manufacturing.

In other words: The voice of the customer translated into the voice of the engineer since the beginning of the product development.



QUALITY FUNCTION DEPLOYMENT

OBJECTIVES

DEFINE THE RIGHT PRODUCT TECHNICAL CHARACTERISTICS

GUARANTEE THE COHERENCE BETWEEN NEEDS AND TECHICAL CHARACTERISTICS

BENCHMARK THE COMPETITION

FOCUS ON THE FIRST PHASE OF PRODUCT DEVELOPMENT

*"***INCREASE THE PRODUCT INFORMATION LEVEL**

GUARANTEE THE COHERENCE BETWEEN THE DESIGN AND PRODUCTION

« **KEEP THE INFORMATION ON STRUCTURED AND FORMAL DOCUMENTS**


QUALITY FUNCTION DEPLOYMENT RISKS

- **UNCOHERENCE**
- **COMPLEXITY**
- " MANY DETAILS
- " CORRELATION DIFFICULTIES
- **TIME EXPENDITURE**



QUALITY FUNCTION DEPLOYMENT HOUSE OF QUALITY 9 Correlati on among 4 the tech,. 3 2 characte ristics 1 **Product technical** characteristics **Relationship matrix** CustomersDmeeds Benchmarking with the competition Importance Numerical figures 6 5 **Technical mportance** 7 Techinical

Benchmarking with

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8



CAR SAFETY BELTS













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QUALITY FUNCTION DEPLOYMENT

STEP N. 4



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STEP N.6

STEP N.7

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Benchmarking Tecnico con la Cconcorrenza



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Each of the phases in the product development uses a QFD matrix to translate customer requirements from initial planning stages through production control

Customer requirements











Predictive maintenance is based on inspections and measurement in the system, after setting the performance levels, in order to establish the level of deterioration.

Predictive maintenance is carried out when the critical level is reached. This not excludes that accidental failures can occur between one inspection and the next.

It depends strongly on the accuracy of measurements of parameters related to the unit's operating states, trying to predict the time of the fault occurrence.





Predictive maintenance is also called Í on conditionî or Í condition basedî maintenance which provides for the real-time programming of maintenance interventions according the to conditions of the unit and the requirements to be respected, allowing to avoid unexpected downtime or chain catastrophic reactions. improving the overall reliability of the system at a reduced cost.

This is possible using the nondestructive techniques to test the selected components or systems It depends strongly on the accuracy of measurements of parameters related to the unit's operating states, trying to Materiale remedict the time of the fault occurrence. Raffaele Campanella





This maintenance policy is mainly suitable for the systems with high hourly cost of operations, with complex and technologically advanced systems, where a plant shutdown would do particularly expensive.

In predictive maintenance the intervention is no longer linked to the time of operation, but to the actual conditions of the component and the reliability of the system.

It combines the advantages of corrective and preventive policies; it constitutes an action done before the fault, supported by a high knowledge of the structure and the real state of the individual components of the machine or system, identifying important parameters to be measured during operation, and the pertinent tolerances ranges.



PREDICTIVE MAINTENANCE

TECHNOLOGIES



OBSERVATION



PREDICTIVE MAINTENANCE

Method	Too1	Application
Visual	Endoscope	Internal parts of machines accessible through small inspection holes
	Optical fibers	Identical to the previous one, more flexible tool
	Strobe	Belts, joints, gears, each part in relative movement
	Penetrant liquids	Superficial cracks
	Thermographic paints	Surface and condensate drains temperature
	Fluorescent liquids	Surface cracks, in particular for light alloys
Temperature	Instant thermometer	Bearings, condensate drains, all cases of rapid measurement
	Infrared thermometer	Surface temperature, flame
	Infrared thermography	Refractory condition, insulating coatings, HV lines, gas pipes,
		hydraulic systems, heat losses, cleanliness of the exchangers
Noises/ultrasound	Stethoscope	Audible band amplifier, mechanical noise
	Sound Level Meter	Noise measurement in environments, machine
	Ultrasound	Search for leaks of fluids under pressure, vacuum, compressor valves,
		piston rings, chains
	Emissione acustica	Crack propagation and other structural defects
Vibrations	Vibrometer	Total vibration measurement
	Analyzer	Frequency analysis for diagnosis of facts
	Phase indicator	Analyzer accessories for balancing
	Real time	Frequency analyzer for analysis of transients and complex cases
	Monitor	Continuous measurement and control with alarm and lockout
	Spn	Specification for rolling bearings
	Acoustic emission	Condition of rolling bearings
Non destructive tests	X-ray	Thicknesses, corrosions, cracks, inclusions, blowholes, emissions
	γ-rays	Identical to the previous one
	Ultrasound	Identical to the previous one
	Eddy currents	Surface and skin defects, condition of the heat exchanger pipes
Wear particles	Magnetic plugs	Identification of magnetic parts, their shape
	Automatic counters	Counting of wear particles and their size
	Absorption and emission	Damper metal particle quantification of the metal present
	spectrophotometry	
	Ferropraphy	Quantification of particles according to their size
Lubricating oils	Lubrisensor	Coarse determination of a lubricant
	Owner Tbn	Determination of the Total basic number to evaluate the influence of
		the sulfur content in diesel oils
	Setaflash	Determination of the presence of pollutants (diesel, water) in the
	Control of the state of the sta	lubricant
Others	Spark gap	Dielectric constant of transformer oils
	Gas Chromatography	Titration of gases present in transformer oils to trace the state of
		insulating materials
	Mobil elektronik com-	Diagnosis of Otto and Diesel engine status
	pression tester	





VIBRATIONS MONITORING AND ANALYSIS

Vibrations monitoring and analysis are two of the most useful tool for predicting incipient mechanical, electrical and process-related problems within plant equipment, machinery, and continous-process sytems.

Therefore they are also the most often-used predictive maintenance technologies.

They are not used alone but in conjunction with other process-related measurements, such as flow, pressure, temperatureÅ

Vibrations monitoring and analysis can be used in many alternative applications such as:

- . Accepting testing/Installation testing
- . Quality Control
- . Loose part detenction
- . Abnormal noise control
- Leak detenction



VIBRATIONS MONITORING AND ANALYSIS



- DISPLACEMENT : The actual change in position of an object from a fixed referencepoint is expressed as displacement
- ["] AMPLITUDE: Amplitude is the distance from the stationary position to the extreme position on either side. The intensity of vibration depends on amplitude.
- **FREQUENCY:** The time rate of change of displacement is velocity (energy generated by vibrations)
- ["] ACCELERATION: Acceleration is a measure of how quickly speed changes with time. The speed of a vibrating object varies from zero to a maximum during each cycle of vibration. (force generated by vibrations)
- ["] PHASE: It is used to define the relationship of harmonic vibration components. Changes of phase can bringto resonance.

RESONANCE: Every object tends to vibrate at one particular frequency called the natural frequency. The measure Materiale riservato Raffaele Camparenatural frequency depends on the composition of the object, its size, structure, weight and shape.



VIBRATIONS MONITORING AND ANALYSIS





THERMOGRAPHY

- Thermography is the process of using an instrument designed to monitor the emission of infrared energy to look for abnormally hot or cold areas on a component operating under normal conditions. It is a viable nondestructive evaluation technique for the characterization of corrosion in metallic materials and is the simplest of all thermal inspection techniques.
- Thermography is the simplest method for predictive maintenance and it is widely used in industry. It can practically be used in all the processes for the detection of
 - Mechanical problems
 - ["] Electrical problems
 - ⁷⁷ Corrosion/erosion damage in plants operating at elevated temperatures.
 - ["] Fouling or internal plugging of piping systems
 - ²⁷ Quality problems of refractory materials.
 - Components faiures
 - ^{⁷ Load problems}

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TRIBOLOGY

TRIBOLOGY is the study of friction, wear, lubrication, fatigue and, more generally, the science of interacting surfaces in relative motion.

Several tribology techniques can be used for predictive maintenance:

- Lubricating oil analysis
 - ⁷ Viscosity
 - ["] Contamination
 - ["] Fuel dilution
 - " Solid content
 - ["] Fuel soot
 - **Oxidation**
 - Nitration
 - Control of Acidity and Basicity
 - " Particle count
- Spectrographic analysis for oil analysis and part analysis
- Ferrography for oil analysis and worn part analysis
- Wear particle analysis due to several types of problems due to wear (Rubbing, Cutting, Rolling fatigue...

....



OTHER NON-DESTRUCTING TESTING TECHNIQUES

As a part od a predictive maintenance program, ultrasonic instruments are used mainly for the following applications:

- ⁷ Airborne noise analysis
- ["] Leak detention
- ⁷ Material testing

All the electromechanical equipment produce a broad range of vibration and therefore sound. The high-frequency ultrasonic components of these sounds are extremely short-wave in nature. A short wave signal tends to be fairly directional and localized, which allows to separate these signal from background noise and to lacalise the source. Further applications are link to:

- [~] The electrical circuits status, because ultrasounds detect ionization produced by arcing, tracking, corona effect..., while infrared is better to locate overheating due to too high corrents;
- As a condition based lubrication because a ultrasound noise exceeding a certain limit is a signal of lubrication need.



HYPOTESYS/CONDITIONS

The system must be inspectable during operation

> The state of the machine or its component is known only due to the results of the inspections, except for the condition Í out of serviceÎ

Materiale riservato Raffaele Campanella The system evolves from conditions of perfect functionality to those of out of service through several intermediate stages characterized by the progressive worsening of some parameters The function of distribution of failure is known and the inspection cost C_i must be lower than both the corrective investment cost C_c and the planned preventive intervention cost C_p .

$$C_i < C_c \ddot{E} C_p$$

and:







WHAT IS NECESSARY





FREQUENCY OF PERIODIC INSPECTION

complexity of the systems

many elementary units/components /parts technical-operational problems, mixed to an economic problem

economic point of view (few or many inspections?)

failure rate for each component/system



PREDICTIVE MAINTENANCE FREQUENCY OF PERIODIC INSPECTION DIFFICULTY FACTORS

- É In fact, as the time interval between two subsequent inspections decreases (increase in inspection frequency), the control of the state of the component or system increases and the reliability as well.
- As the inspection frequency increases, the cost resulting from accidental breakdowns decreases, however leading to higher direct inspection costs.
- The problem that arises is then to determine the optimal inspection frequency, such as to minimize the sum of the inspection costs and those associated with the out of operation of the machinery.



SIMPLIFIED MODELS FOR FREQUENCY OF PERIODIC INSPECTION DEFINITION



This is sequence of inspection intervals $t_1, t_2, ..., t_n$ where the function of distribution of the failure times between two successive inspections remain constant over time. Under this assumption the intervals are

 $t_i = i \cdot t$ with i = 1, 2, ..., n

therefore sufficient to know t to determine the complete sequence of inspection

Systems with components subject to random faults

The optimal inspection frequency, in the case of accidental failures, can be determined with an approximate method: this can be obtained by minimizing the cost function, which can be expressed as:

$$\mathbf{C} = \mathbf{C}_{i} \cdot \mathbf{f} + \mathbf{C}_{c} \cdot \mathbf{p} + \mathbf{C}_{p} \cdot (1 - \mathbf{p})$$

where:

 C_i = cost of an inspection that is supposed to be constant;

C_c = overall cost of the failure maintenance intervention;

 C_p = overall cost of the preventive intervention;

f = average number of inspections up to and including maintenance;

p = conditional probability of failure between two successive inspections which is considered constant and can be expressed by the ratio:

$$p = \frac{F(t_i) - F(t_{i-1})}{R(t_{i-1})}$$

with: $F(t_i)$ = cumulative probability of failure at time t_i ; R (t_i) = reliability at the time t_i .



Systems with components subject to random faults

The probability that the fault occurs in the inspection interval (i, i+1) can be expressed by the relation between the probability that the fault did not occur before and the probability that the fault occurs at the i-th inspection, that is:

(1 Ë p)ⁱ⁻¹ · p

The average number of inspections until failure can be expressed by the report:

$$f = \sum_{i=1}^{\infty} i \cdot (1-p)^{i-1} \cdot p = \frac{1}{p}$$



Systems with components subject to random faults

 $\mathbf{C} = \mathbf{C}_{i} \cdot \mathbf{f} + \mathbf{C}_{c} \cdot \mathbf{p} + \mathbf{C}_{p} \cdot (1 - p)$

Substituting in the cost function, we obtain:

 $\frac{c_i}{p} + C_c \cdot p + C_p \cdot (1-p)$

and, minimizing it, that is, deriving it with respect to p and equaling it to zero, we obtain:

$$-\frac{C_i}{p^2} + C_c - C_p = 0$$

from which:

$$\boldsymbol{p} = \sqrt{\frac{\boldsymbol{c}_i}{(\boldsymbol{c}_c - \boldsymbol{c}_p)}}$$



Systems with components subject to random faults

For λ constant, applying an exponential type of system fault law, we have:

$$\frac{t}{MTBF} = -\ln(1-p)$$

from which the optimal inspection interval can be obtained by knowing the overall costs and the average time between failures (MTBF). By means of a simple data processing program or the use of suitable tables (see next slide), it is possible to determine the optimal inspection frequency and therefore from the sequence of inspection times.



Systems with components subject to random faults

Table for calculating the optimal inspection frequency in the event of accidental failures

$$\boldsymbol{p} = \sqrt{\frac{\boldsymbol{c}_i}{(\boldsymbol{c}_c - \boldsymbol{c}_p)}}$$

$$\frac{t}{MTBF} = -\ln(1-p)$$

1	$C_i/(C_c-C_p)$	р	t _i /MTBF
	0,001	0,03162	0,03213
	0,002	0,04472	0,04575
	0,003	0,05477	0,05632
	0,004	0,06324	0,06532
	0,005	0,07071	0,07343
	0,006	0,07745	0,08061
[0,007	0,08366	0,08737
	0,008	0,08944	0,09369
	0,009	0,94861	0,09967
	0,010	0,10000	0,10536
	0,020	0,14142	0,15247
[0,030	0,17340	0,19019
[0,040	0,20000	0,22314
	0,050	0,22360	0,25308
[0,060	0,24425	0,28097
[0,070	0,26437	0,30729
[0,080	0,28284	0,33245
[0,090	0,30000	0,33667
<u>۱</u>	0,100	0,31672	0,38011
) 🗖	0,200	0,44721	0,59277
	0,300	0,54772	0,79545
	0,400	0,63245	1,00089
[0,500	0,70710	1,22729
[0,600	0,77459	1,48983
[0,700	0,83666	1,81192
	0,800	0,89442	2,24828
[0,900	71 0,94868	2,96967



Systems with components subject to random faults

Example

If the inspection cost on a machine is 1000 Ö, an emergency intervention cost of Ö 20,000, a preventive intervention cost of Ö 15.000 with a mean time before failure MTBF of 200 hours, you will have:

$$\frac{C_i}{(C_c - C_p)} = \frac{1000}{20000 - 15000} = \frac{1.000}{5000} = 0, 2$$

for which we will obtain:

$$\frac{t}{MTBF} = 0,59277 \quad and \quad t_1 = 0,59277 \cdot 200 = 118,5 \cong 119 \ hours$$


Systems with components subject to random faults

Example:

The sequence of inspection times, taking into account that the component fails after 450 hours and is changed, is as follows:

 $t_1 = 119$ hours $t_2 = 238$ hours $t_3 = 357$ hours $t_g = 450$ hours (failure) $t_4 = 569$ hours $t_5 = 688$ hours

and so you go until a new fault occurs or until the inspection gives results such as to recommend the scheduled intervention.



Systems with components subject to wear failure





Conditional probability of failure increase over time

the intervals between two next inspections are different and decrease over time.



Systems with components subject to wear failure

The determination of the inspection time sequence ti (i = 1, 2, ..., n) is carried out when are known:

the value of the ratio between the inspection cost Ci and the difference between the overall costs of the maintenance intervention at fault Cc and the preventive one Cp

Ci/(Cc-Cp)

- ["] the values of p, the probability of failure between an inspection and the next one
- ["] the values of the normalized variable time Ui expressed by the ratio

$$U_i = \frac{(t_i - MTBF)}{\sqrt{FTV}}$$

where:

MTBF = mean time before failure;

FTV = variance of the distribution of the failure times related to the machine



Systems with components subject to wear failure

$$U_i = \frac{(t_i - MTBF)}{\sqrt{FTV}}$$

These values were obtained as a function of the ratio

 $C_i/(C_c-C_p)$

as shown in the table and allowing to get the sequence of inspection times according to the relationship:

$$t_i = U_i \cdot \sqrt{FTV} + MTBF$$



Systems with components subject to wear failure

Calculation of the optimal inspection times for components subject to wear

$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	$C_i/(C_c-C_p)$	р	U_1	U_2	U3	U_4	U ₅	U ₆	U7
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0,001	0,03162	-1,80	-1,54	-1,39	-1,15	-1,04	-0,93	-0,84
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0,002	0,04472	-1,70	-1,36	-1,13	-0,97	-0,80	-0,71	-0,66
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0,003	0,05477	-1,60	-1,25	-1,01	-0,84	-0,69	0,56	-0,45
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0,004	0,06324	-1,53	-1,16	-0,92	-0,74	-0,59	-0,46	-0,34
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0,005	0,07071	-1,47	-1,10	-0,85	-0,66	-0,50	-0,37	-0,25
$\begin{array}{ c c c c c c c c c c c c c c c c c c c$	0,006	0,07746	-1,42	-1,04	-0,79	-0,60	-0,44	-0,30	-0,17
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0,007	0,08367	-1,38	-0,99	-0,74	-0,54	-0,37	-0,23	-0,11
$\begin{array}{c c c c c c c c c c c c c c c c c c c $	0,008	0,08944	-1,34	-0,95	-0,69	-0,49	-0,32	-0,17	-0,05
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,009	0,09487	-1,31	-0,91	-0,65	-0,45	-0,27	-0,12	+0,01
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,010	0,10000	-1,24	-0,88	-0,60	-0,40	-0,23	-0,07	+0,06
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,020	0,14142	-1,08	-0,63	0,34	-0,11	+0,08	+0,26	+0,40
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,030	0,17321	-0,94	-0,48	-0,19	+0,08	+0,29	+0,47	+0,63
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,040	0,20000	-0,84	-0,36	-0,03	+0,23	+0,45	+0,64	+0,81
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,050	0,22361	-0,76	-0,26	+0,08	+0,35	+0,58	+0,78	+0,95
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,060	0,24495	-0,69	-0,18	+0,17	+0,45	+0,69	+0,90	+1,08
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,070	0,26458	-0,63	-0,10	+0,26	+0,54	+0,79	+1,00	+1,19
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,080	0,28284	-0,57	-0,04	+0,34	+0,63	+0,88	+1,10	+1,30
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,090	0,30000	-0,52	+0,03	+0,41	+0,71	+0,96	+1,19	+1,39
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,100	0,31623	-0,48	+0,08	+0,47	+0,78	+1,04	+1,27	+1,48
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,200	0,44721	-0,13	+0,51	+0,96	+1,30	+1,63	+1,90	+2,15
$\begin{array}{c ccccccccccccccccccccccccccccccccccc$	0,300	0,54772	+0,12	+0,83	+1,30	+1,73	+2,08	+2,38	+2,66
(0,500) $0,70711$ $(+0,55)$ $(+1,37)$ $(+1,95)$ $(+2,44)$ $(+2,85)$ $(+3,22)$ $(+3,$	0,100	0,63246	+0,34	+1,10	+1,65	+2,09	+2,47	+2,81	+3,10
0.77460 0.77460 0.70 0.00 0.000 0.000	(0,500)	0,70711	(+0,55) +1,37	+1,95	+2,44	+2,85	+3,22	+3,59
$0,000$ $0,7/400$ $\pm 0,70$ $\pm 1,04$ $\pm 2,27$ $\pm 2,80$ $\pm 5,14$ $\pm 3,04$ $\pm 4,$	0,600	0,77460	+0,76	+1,64	+2,27	+2,80	+3,14	+3,64	+4,02
0,700 0,83666 +0,98 +2,00 +2,62 +3,19 +3,68 +4,12 +4,	0,700	0,83666	+0,98	+2,00	+2,62	+3,19	+3,68	+4,12	+4,39
0,800 0,89443 +1,25 +2,28 +3,04 +3,66 +4,20 +4,65 +4,	0,800	0,89443	+1,25	+2,28	+3,04	+3,66	+4,20	+4,65	+4,78
0,900 0,94868 +1,63 +2,79 +3,56 +4,26 +4,80 +4,91 +4,	0,900	0,94868	+1,63	+2,79	+3,56	+4,26	+4,80	+4,91	+4,99



Systems with components subject to wear failure

Example:

- We have a machine subject to wear failures, characterized by a function of failure time distribution having MTBF = 5,000 hours and FTV = 1,000 hours.
- We want to apply a predictive maintenance policy,, which entails an inspection cost of 1,000 Ö, a cost of the emergency intervention of Ö 20,000 and the preventive intervention of Ö 18,000.
- It is possible to calculate the ratio value from the above table:

$$\frac{C_i}{(C_c - C_p)} = \frac{1.000}{(20.000 - 18.000)} = \frac{1.000}{2.000} = 0,5$$

 $U_1 = +0,55$ $U_2 = +1,37$ $U_3 = +1,95$ $U_4 = +2,44$
 $U_5 = +2,85$ $U_6 = +3,22$ $U_7 = +3,59$

Systems with components subject to wear failure

Example:

Known from U_1 to U_7 , the consequent inspection times are determined and, if a preventive intervention is foreseen at time t_4 , we have:

$$\begin{split} t_1 &= U_1 \cdot \sqrt{FTV} + MTBF = 0,55 \cdot \sqrt{1.000} + 5.000 = 5.017 \ hours \\ t_2 &= U_2 \cdot \sqrt{FTV} + MTBF = 1,37 \cdot \sqrt{1.000} + 5.000 = 5.043 \ hours \\ t_3 &= U_3 \cdot \sqrt{FTV} + MTBF = 1,95 \cdot \sqrt{1.000} + 5.000 = 5.062 \ hours \\ t_4 &= U_4 \cdot \sqrt{FTV} + MTBF = 2,44 \cdot \sqrt{1.000} + 5.000 = 5.077 \ hours \\ t_5 &= t_4 + U_1 \cdot \sqrt{FTV} + MTBF = 5.077 + 0,55 \cdot \sqrt{1.000} + 5.000 = 10.094 \ hours \\ t_6 &= t_4 + U_2 \cdot \sqrt{FTV} + MTBF = 5.077 + 1,37 \cdot \sqrt{1.000} + 5.000 = 10.120 \ hours \end{split}$$

thus continuing until a fault arises or until the inspection gives results such that the scheduled intervention is recommended.



Other systems

Other authors have proposed models to support the determination of the optimal inspection frequency which are reported:

a) Inspection scheduling model for single machine

If there is a component of a system, whose status is identifiable by monitoring appropriate indicators, if a fault is repaired with a maintenance intervention, the component returns to a good state.

It is therefore necessary to determine the optimal scheduling of the inspection interventions such as to minimize the cost per unit of time associated with the inspection, corrective maintenance and the consequent non-identification of the fault.



Other systems

b) profit maximization model (breakeven inspection)

The aim of the model is to establish the optimal periodic inspection interval by maximizing the profit function, where:

p = the profit per unit of time associated with the operation of the machine

- T the duration of the operating cycle (time interval in which the inspection is carried out until a break can be detected manifested in an instant t, with t < T)
- **P(T)** = the expected profit for the operating cycle
- $P_1(T)$ = the profit related to an operating cycle without failure,
- $P_2(T)$ = the profit related to an operating cycle with failure,
- UP(T) = the total profit per unit of time
- F(t) = the probability of failure,

the following cost relations associated with an operating cycle can be written:

$$P_1(T) = p \cdot T - C_i$$
 $P_2(T) = \frac{\int_0^T p \cdot t \cdot f(t) dt}{F(T)} - C_i - C_r$



Other systems

b) profit maximization model (breakeven inspection)
 Also in this case the component must be as good as new in the face of a maintenance intervention.

$$P_1(T) = p \cdot T - C_i$$
 $P_2(T) = \frac{\int_0^T p \cdot t \cdot f(t) dt}{F(T)} - C_i - C_r$

The expected profit over a cycle is:

$$P(T) = P_1(T) \cdot R(T) + P_2(T) \cdot F(T)$$

$$P(T) = (p \cdot T - C_i) \cdot R(T) + \int_0^T p \cdot t \cdot f(t) \, dt - (C_i + C_r) \cdot F(T)$$

$$P(T) = (p \cdot T - C_i) \cdot R(T) - [1 - R(T)] \cdot (C_i + C_r) + p \int_0^T t \cdot f(t) \, dt$$

$$P(T) = p \int_0^T R(t) \, dt + C_r \cdot R(T) - C_i - C_r$$



Other systems

b) profit maximization model (breakeven inspection) The unit profit to be maximized is:

$$UP(T) = \frac{p \int_0^T R(t) dt + C_r \cdot R(T) - C_i - C_r}{T}$$

That function with one variable can be solved deriving it and equalling it to zero.



Other systems

b) profile maximization model (breakeven inspection) Example:

Consider a component of a system having a failure probability density f(t) uniformly distributed between 0 and 8 weeks:

$$f(t) = \begin{cases} \frac{1}{8} & (0 \le t \le 8) \\ 0 & otherwise \end{cases}$$

Furthermore we know:

- repair costs: C_r
- inspection costs: C_i
- profit per unit of time associated with the operation of the machine: p = Öweek



Other systems

b) profit maximization model (breakeven inspection) Reliability is as follows:

$$R(t) = 1 - F(t) = \begin{cases} 1 - \frac{1}{8} t & (0 \le t \le 8) \\ 0 & t > 8 \end{cases}$$

The unitary profit is:

$$UP(T) = \frac{p \int_0^T R(t)dt + C_r \cdot R(T) - C_i - C_r}{T} = \frac{p \int_0^T \left[1 - \frac{1}{8}t\right]dt + C_r \cdot \left[1 - \frac{1}{8}T\right] - C_i - C_r}{T}$$

$$UP(T) = \frac{p \cdot \left(T - \frac{1}{8}T^2\right) - \frac{C_r}{8} \cdot T - C_i}{T} = \frac{p \cdot \left(8 \cdot T - T^2\right) - C_r \cdot T - 8 \cdot C_i}{10 \cdot T}$$

The values of the unitary profit when T changes are shown in the table, calculated by applying the exhaustive

method:



Trend of UP(T) [€/week]

Materiale riservato Raffaele Campanella he optimal period in which to carry out the inspection visit is 2 weeks with a unit profit is Ö2,000;



INTERVENTION PLANS







Raffaele Campanella



MAINTENANCE EVOLUTION

