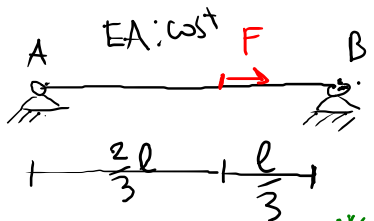


METODO DELLE FORZE PER LA RISOLUZIONE DELLE STR IPERSTATICHE

2/12/22



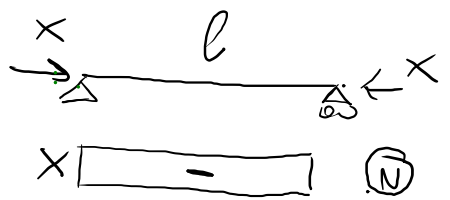
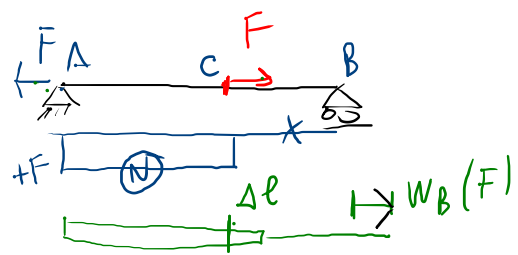
STR IPERST. (1 V. IPER)



← INCOGNITA IPERST.
STR. PRINCIPALE (SP)
(STR. ISOSTATICA)
(o, meglio, STAT. DETERM.)

$w_B = 0$ EQ. DI CONGRUENZA $\Rightarrow$ (X) $\Rightarrow$ X DIVENTA UNA FORZA NOTA PER LA S.P.

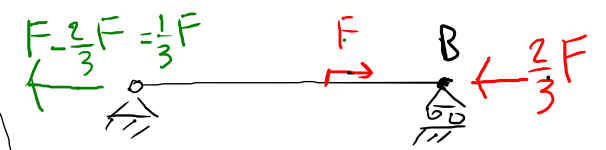
$w \leftrightarrow +$



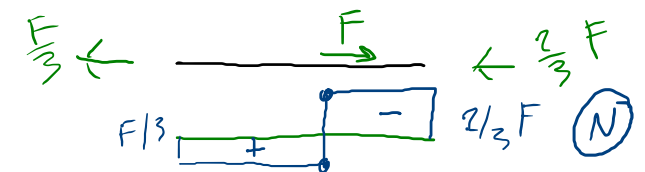
$$w_B(F) + w_B(X) = 0$$

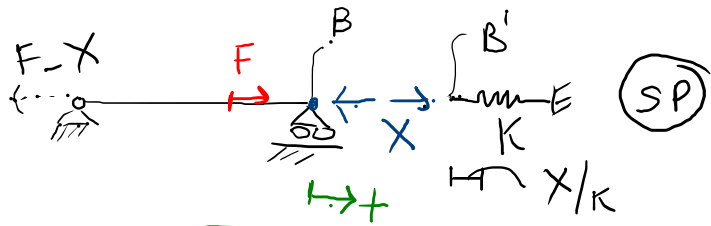
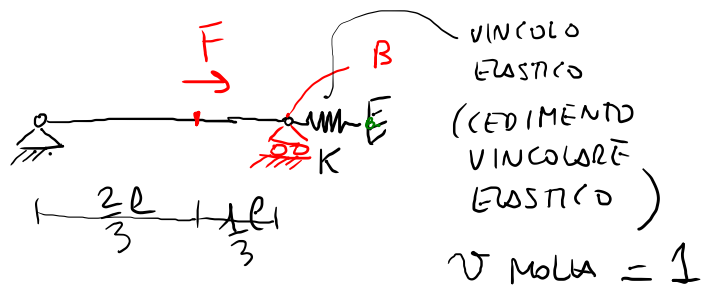
$$\frac{+F \frac{2}{3}l}{EA} - \frac{Xl}{EA} = 0$$

Segno !!
Vero conf.
 $X = \frac{2}{3}F$



SP CON X RISOLTA.
DIVENTA UN' ISOSTATICA "NORMALE"
 $\rightarrow$ E' EQUIVALENTE ALLA STR. IPERST. INIZIALE

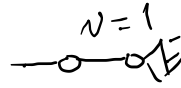




$$\boxed{W_B = W_{B'}} \quad \text{EQ. DI CONGR.}$$

$$W_B(F, X) = W_{B'}(X)$$

$$\frac{F \frac{2}{3} l}{EA} - \frac{X l}{EA} = + \frac{X}{K} \quad (*)$$



$$\frac{X l}{EA} + \frac{X}{K} = \frac{2}{3} \frac{F l}{EA}$$

$$X \left(\frac{l}{EA} + \frac{1}{K} \right) = \frac{2}{3} \frac{F l}{EA}$$

$$X = \frac{2}{3} F \frac{l/EA}{\frac{l}{EA} + \frac{1}{K}} \quad (+)$$

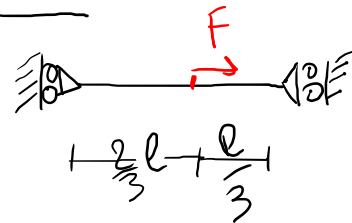
$$K \rightarrow \infty ; \frac{1}{K} \rightarrow 0 ; X \rightarrow \frac{2}{3} F \quad \text{LIMITE SUP DI } X.$$

$$K = 0 \quad (*) : K \left[\quad \right] = X$$

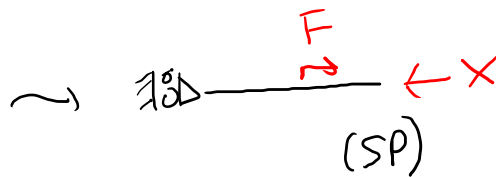
$$\boxed{0 = X}$$

$$\frac{l}{EA} \sim \frac{1}{K} \Rightarrow \text{CEDIMENTO ELASTICO} = \frac{1}{\text{RIGIDEZZA}}$$

oss.

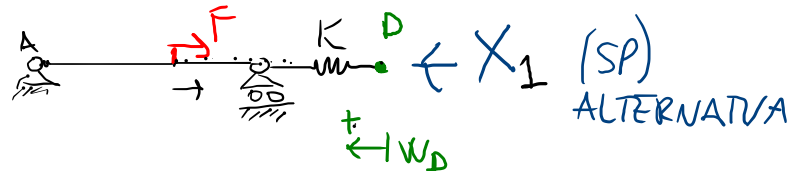


STR LABILE
PR STAT. INDET.



STR LABILE

PR. STAT. DETERMINATO



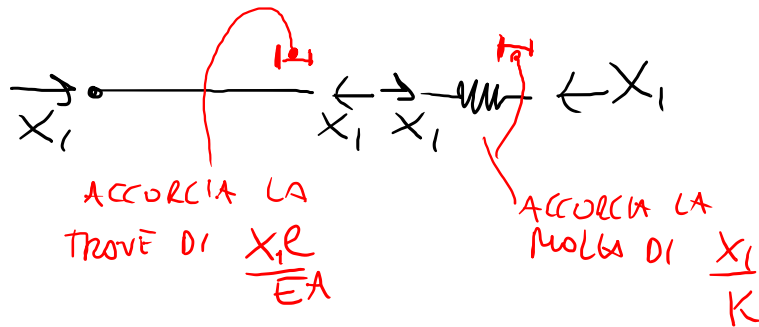
$$w_D = 0$$

$$w_D(F) + w_D(X_1) = 0$$

$$- \frac{F \frac{2}{3} l}{EA} + \frac{X_1 l}{EA} + \frac{X_1}{K} = 0$$

STESSO DI
PRIMA

$$X_1 = X \text{ di prima}$$

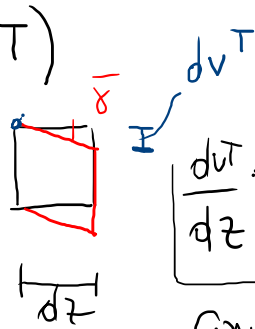


LINEA ELASTICA (EFFETTI DI M, T)



$$\frac{d\varphi}{dz} = \chi = \frac{M}{EI}$$

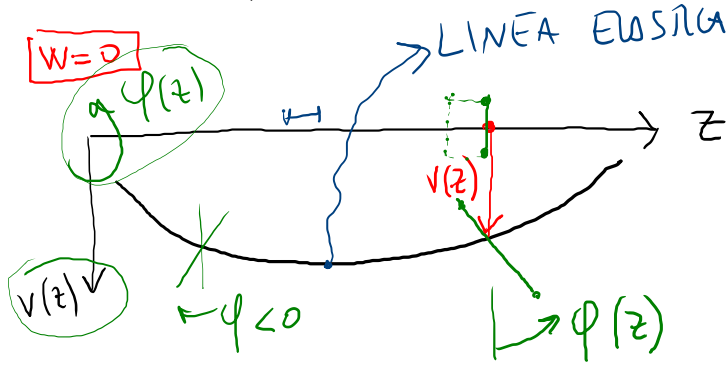
CONGRUENZA
INTERNA



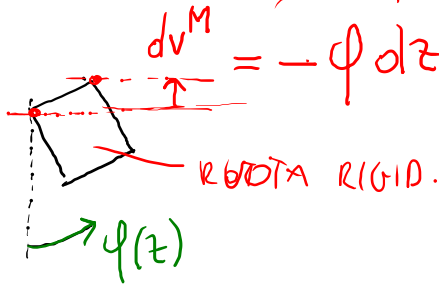
$$\frac{dv^T}{dz} = \bar{\gamma} = \frac{\kappa T}{GA}$$

CONGR. INTERNA

$$W=0$$



CONGR. I ORDINE
IN φ



ROTTA RIGID.

$$\frac{d\varphi}{dz} = \frac{M}{EI}$$

$$\frac{dv}{dz} = \frac{\kappa T}{GA} - \varphi$$

4

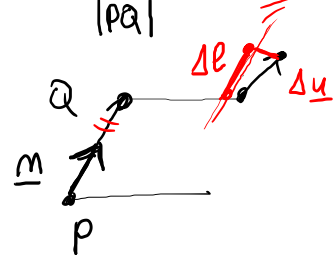
$\varphi(z), v(z)$

ACCOLE

$$dv = dv^T + dv^M$$

$$= \frac{\kappa T}{GA} dz - \varphi dz$$

$$\frac{\Delta \ell}{|PQ|} = \epsilon_m = \underline{\epsilon}_m \cdot \underline{m}$$



$$\Delta \ell = \underline{\Delta u} \cdot \underline{m}$$

$$= \underline{\epsilon} \cdot \underline{PQ} \cdot \underline{m}$$

$$PQ = |PQ| \underline{m}$$

$$\Delta \ell = \underline{\epsilon} \cdot \underline{m} \cdot \underline{m} \quad |PQ|$$

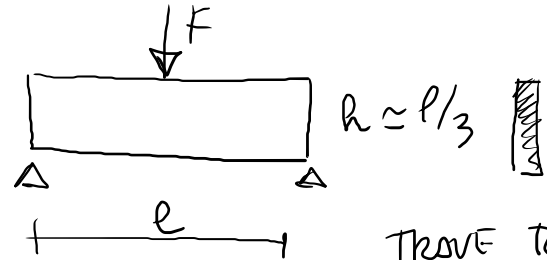
$$\epsilon_m = \frac{\Delta \ell}{|PQ|} = \underline{\epsilon}_m \cdot \underline{m}$$

$$\epsilon_m = \underline{\epsilon} \cdot \underline{e}_1 \cdot \underline{e}_1$$

EQ LINEA ELASTICA (ALLA TIMOSHENKO) [TEORIA DELLA TIMOSHENKO]

$$\begin{cases} \frac{d\varphi(z)}{dz} = \frac{M(z)}{EI(z)} \\ \frac{dv(z)}{dz} = \frac{K T(z)}{GA(z)} - \varphi(z) \end{cases} \Rightarrow + 2 \text{ CONDIZ. AI LIMITI}$$

(*) EFFETTO DEL TAGLIO SULLA DEFORMAZIONE



TRAVE TOZZA

$$\frac{l}{h} < 6 \div 8$$

(*) È IMPORTANTE

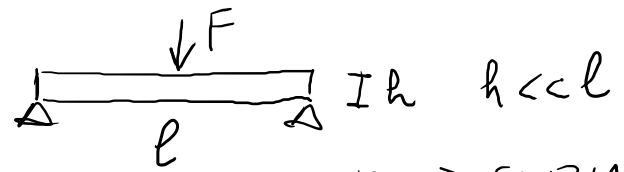
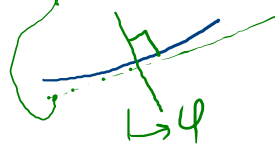
TRAVI SNELLE (ALLA EULERO-BERNOULLI) - NAVIER

$$\begin{cases} \frac{d\varphi}{dz} = \frac{M}{EI} \\ \frac{dv}{dz} = -\varphi \end{cases} \Rightarrow \boxed{\frac{d^2 v}{dz^2} = -\frac{M}{EI}}$$

EQ. DELLA LINEA ELASTICA DEL II ORDINE

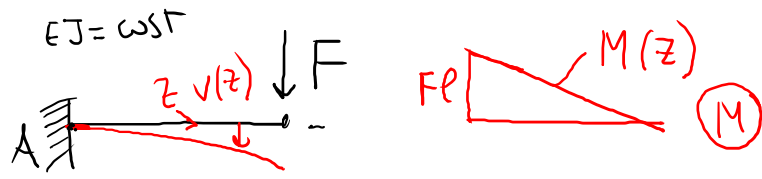
↳ 2

CONDIZ. AI LIMITI



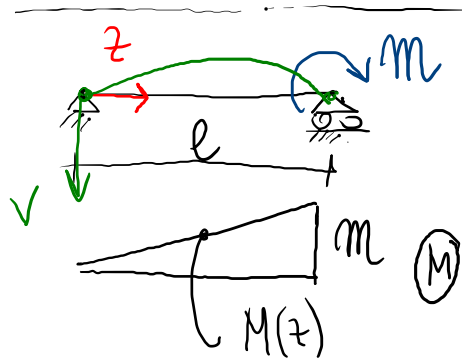
TRAVE SNELLA

(*) È TRASCURABILE



$$\begin{cases} v''(z) = -\frac{M(z)}{EJ} \\ v(0) = 0 \\ v'(0) = 0 \end{cases}$$

$$v(z) \Rightarrow \phi(z) = -v'(z)$$



$$(v(z) < 0)$$

$$\begin{cases} v''(z) = -\frac{M(z)}{EJ} \\ v(0) = 0 \\ v(l) = 0 \end{cases}$$