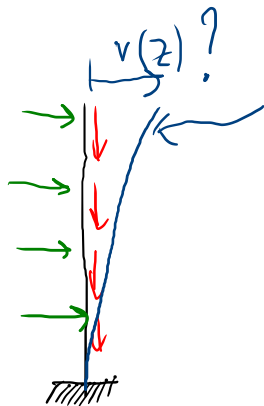


.... $\Pi(u)$, NELLA TEORIA LINEARE 'SOLITA' DELLA S.D.C.

7/10/22

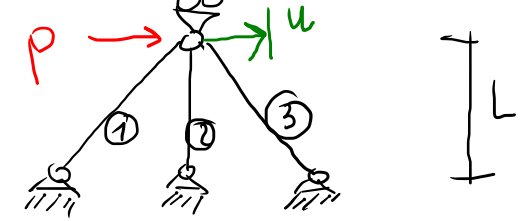
LA SOLUZ. DEL PROBLEMA ELASTICO È UNICA E COINCIDE
CON UN MINIMO DELL' E. POTENZIALE TOTALE.



STUDIO EQUILIBRIO
RISPETTO ALLA CONFIG.
DEFORMATA

(PROBL. NON LINEARE)

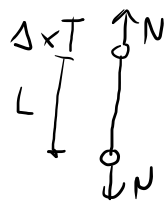
LES



u: INCOGNITA DEL PROBLEMA

$\Pi(u)$

EA
cost



$$E_e = \frac{1}{2} K \Delta x^2$$

$$K = \frac{EA}{L}$$

$$\Delta x = \frac{N}{K}$$

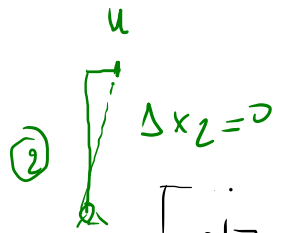
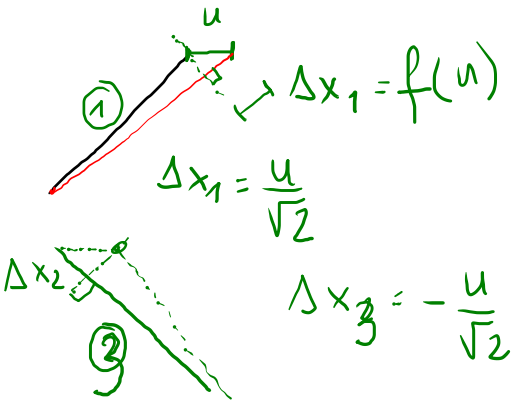
$$E_e = \frac{1}{2} \frac{EA}{L} \Delta x^2$$

$$\Pi(u) = EN \cdot E \cos \alpha - Pu$$

$$\Pi(u) = \frac{1}{2} \sum_{i=1}^3 \left(\frac{EA}{L} \Delta x_i^2 \right) - Pu$$

$$\Pi(u) = \frac{1}{2} EA \left(\frac{u^2}{L\sqrt{2} \cdot 2} + 0 + \frac{u^2}{L\sqrt{2} \cdot 2} \right) - Pu$$

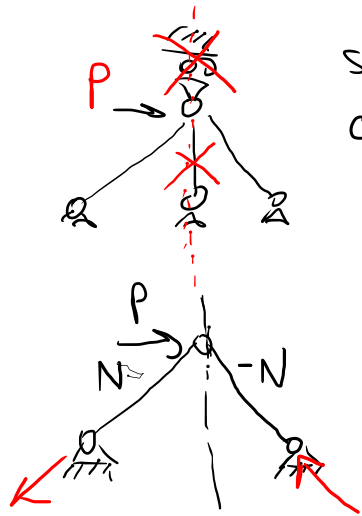
$$\Pi(u) = \frac{1}{2} EA \frac{u^2}{L\sqrt{2}} - Pu$$



$$\frac{d\Pi}{du} = 0 ; \quad EA \frac{u}{L\sqrt{2}} - P = 0 \Rightarrow$$

$$u = \frac{P L \sqrt{2}}{EA}$$

... CON LA SIMM.



STR SIMM

CORIC ANTISIMM

RISP. STR.
ANTISIMM.

ISOST.

DELL' STRUTTURE.

DEGLI SPOSTAMENTI PER LA RIS.

$$\delta \Pi(\underline{u}) = 0$$

\underline{u} SPOST. INCOGNITI

LA STAZION. DELL' E, POT.

TOTALE CONDUCE ALLA

FORMULA. DEL METODO

RICORDIAMOCI CHE ESISTE U' EN POT. COMPLEMENTARE

$$\Pi = \frac{1}{2} \int_B \underline{\sigma} \cdot \underline{\varepsilon} dV - \int_B \underline{b} \cdot \underline{u} dV - \int_{\partial B} \underline{p} \cdot \underline{u} dS \quad \Pi = \Pi^c \quad \underline{\sigma} = \underline{C} \underline{\varepsilon}$$

$$\Pi(\underline{u}) = \frac{1}{2} \int_B \underline{C} \underline{\varepsilon} \cdot \underline{\varepsilon} dV - \dots \quad \Pi^c(\underline{\sigma}) = \frac{1}{2} \int_B \underline{\sigma} \cdot \underline{C}^{-1} \underline{\sigma} dV - \dots$$

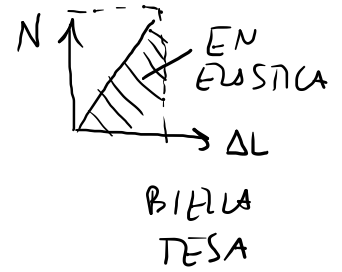
EN POT. TOTALE PER STR. INFLESSE (EULERO-BERNOULLI)

$$\Pi = \frac{1}{2} \int_V \sigma_e \varepsilon dV = \dots$$

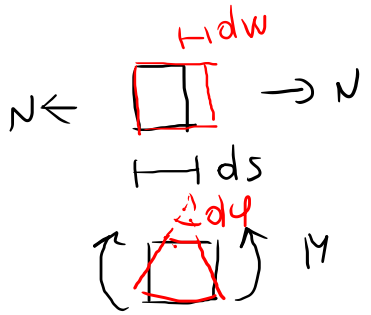
ENERGIA POTENZIALE
 Φ ELASTICA DEL CORPO

$$\Phi = \frac{1}{2} \int_s N \varepsilon + M \chi ds$$

DEF. ASSIALE
 CURV.

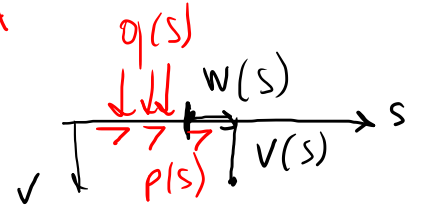


$$\Phi(\varepsilon, \chi) = \frac{1}{2} \int EA \varepsilon^2 + EI \chi^2 ds$$



$$\frac{dw}{ds} = \varepsilon = \frac{N}{EA}$$

$$\frac{d\phi}{ds} = \chi = \frac{M}{EI}$$



TRAVI SNELLE

$$\varepsilon = w'(s)$$

$$\chi = -v''(s)$$

solo FLESSIONE

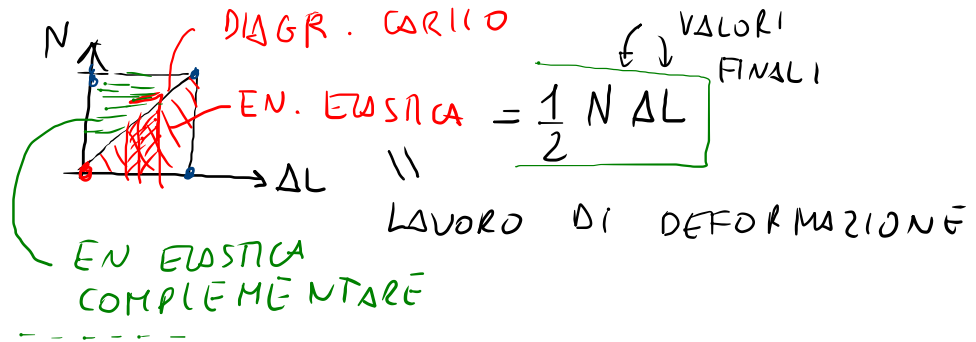
$$\Phi(w, v) = \frac{1}{2} \int_s EA (w')^2 + EI (v'')^2 ds$$

$$\Pi(w, v) = \frac{1}{2} \int_s EA (w')^2 + EI (v'')^2 ds - \int_s (q v + p w) ds$$

TEOREMI ENERGETICI (O DEL LAVORO DI DEFORMAZIONI)



$$\Delta L = \frac{NL}{EA}$$

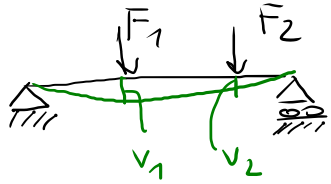


$$\left(\bar{\Phi} = \frac{1}{2} \int_S \frac{N^2}{EA} + \frac{M^2}{EI} ds \right) = \bar{\Phi}^C$$

$\bar{\Phi}$ COMPLEMENTARE

TEOREMA DI CLAPEYRON

ENUNCIATO



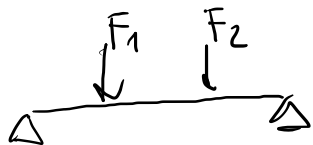
- CARICAMENTO QUASI-STATICO
 - MATERIALE ELASTICO LINEARE
 - VINCOLI PERFETTI
- } IPOTESI

$$\Phi = \frac{1}{2} (F_1 v_1 + F_2 v_2) \quad \text{TESI}$$

DIM. (CON IL PLU)



ϵ, χ : CINEM.
AMMISSIBILE
(CONGRUENTE)



N, M : STAT. AMMISS
(EQUILIBRATO)

$$L_{ve} = L_{vi}$$

$$L_{ve} = F_1 v_1 + F_2 v_2$$

$$L_{vi} = \int_s N \epsilon + M \chi \, ds = \int_s \frac{N^2}{EA} + \frac{M^2}{EI} \, ds$$

$$L_{ve} = L_{vi}$$

$$\frac{1}{2} (F_1 v_1 + F_2 v_2) = \frac{1}{2} \int_s \frac{N^2}{EA} + \frac{M^2}{EI} \, ds$$

" = Φ

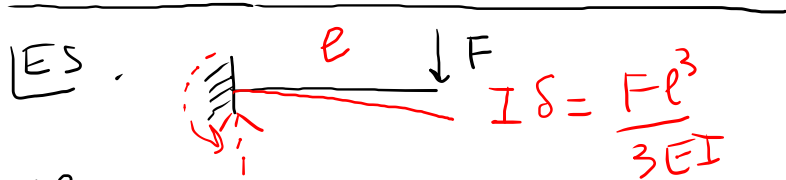
OSSERVAZ.

— $\Phi \rightarrow$ VIA INTERNA $= \frac{1}{2} \int \dots$

— VIA ESTERNA $= \frac{1}{2} (F_1 u_1 + \dots)$ (CLAPEYRON)

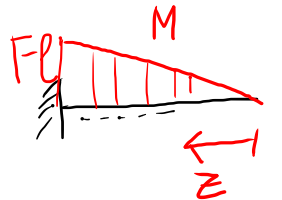
— UTILIZZO DEL TEOREMA PER CALCOLORE E

$$\Phi = \frac{1}{2} \int \frac{N^2}{EA} + \frac{M^2}{EI} ds \Rightarrow E$$



δ ? CON TH. DI CLAPEYRON

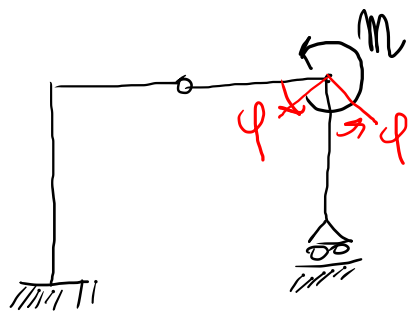
$$\frac{1}{2} F \delta = \frac{1}{2} \int \frac{M^2}{EI} ds$$



$$M(z) = -Fz$$

$$FS = \frac{1}{EI} \int_0^l (Fz)^2 dz$$

$$FS = \frac{Fl^3}{3EI} ; \delta = \frac{Fl^3}{3EI}$$



CON THI DI CLAPYRON

POSSO SOLO COLLOCARE $\varphi \Leftrightarrow M$

