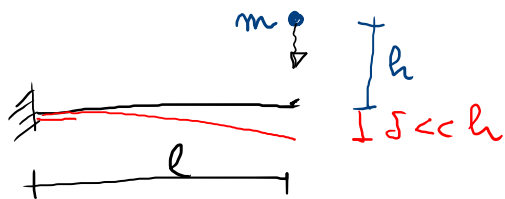


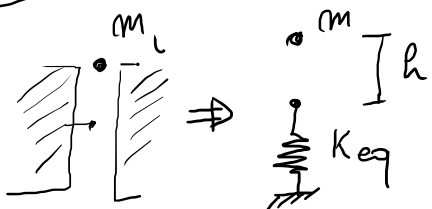
...TEOREMI ENERGETICI

17/11/2022



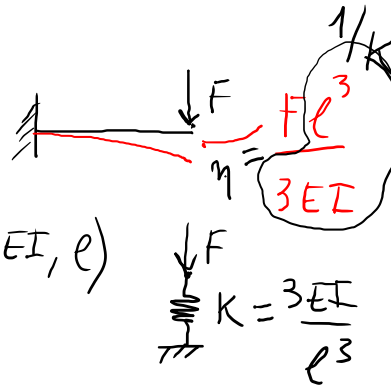
LASCIO LA MASSA E VOGLIO CALCOLARE δ (MASSIMO SPOST. TRAVE)
 $(\delta \ll h) \quad E_{pot} = mgh$

I METODO



$E_{pot} = E_{elast}$

$mgh = \frac{1}{2} K_{eq} \delta^2 \Rightarrow \delta = f(K_{eq}) = f(EI, l)$



$K_{eq} = \frac{3EI}{l^3}$

EN ELASTICA
 IMMAGINATA
 NELLA STRUTTURA

$E_{pot} = \Phi \rightarrow M(s) \Rightarrow M(\delta)$
 $mgh = \frac{1}{2} \int_{str} \frac{M^2}{EI} ds$

II METODO

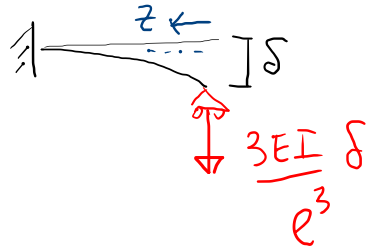
IN UNA STR.
 INFLESSA

$\Phi = \frac{1}{2} \int_{str} \frac{M^2}{EI} ds$





$$\delta = \frac{F l^3}{3EI}$$



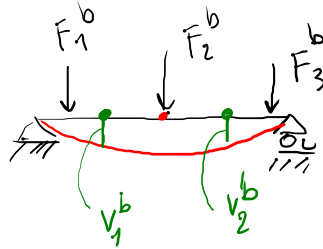
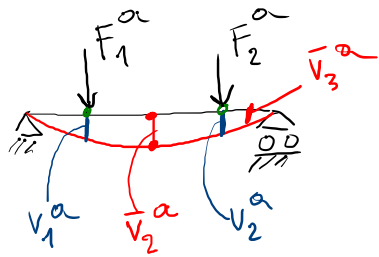
$$M(z) = -\frac{3EI}{l^3} \delta z$$



$$\frac{1}{2} \int_0^l \frac{M^2}{EI} dz = \frac{1}{2} \int_0^l \frac{1}{EI} \frac{9(EI)^2}{l^6} \delta^2 z^2 dz = \frac{9}{2} \frac{EI}{l^6} \delta^2 \frac{l^3}{3} = \left(\frac{9}{6}\right) \frac{EI}{l^3} \delta^2$$

$$mgh = \frac{3}{2} \frac{EI}{l^3} \delta^2 \Rightarrow \delta = \sqrt{\quad}$$

TEOREMA DI BETTI (O DI RECIPROCAITA') 1872

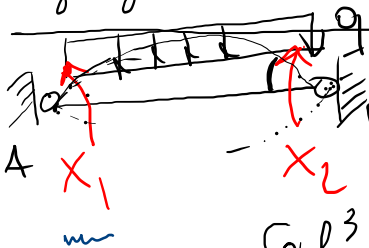


IPOTESI
TH BETTI =
TH DI
CLAUPEYRON

$$F_1^a v_1^b + F_2^a v_2^b = F_1^b v_1^a + F_2^b v_2^a + F_3^b v_3^a$$

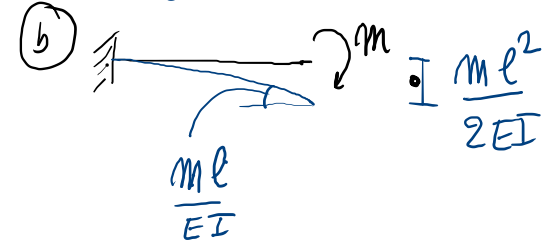
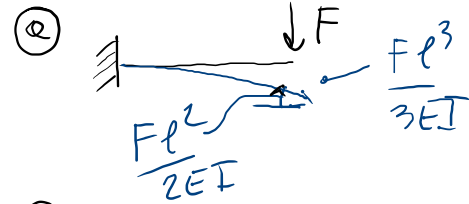
$$L_{ab} = L_{ba}$$

uguaglianza dei lavori virtuali.



$$\begin{cases} \varphi_A = 0 \\ \varphi_B = 0 \end{cases}$$

$$\begin{cases} \frac{ql^3}{24EI} - \frac{X_1 l}{3EI} - \frac{X_2 l}{6EI} = 0 \\ -\frac{ql^3}{24EI} + \frac{X_2 l}{3EI} + \frac{X_1 l}{6EI} = 0 \end{cases}$$



$$L_{ab} = F \frac{ml^2}{2EI}$$

$$L_{ba} = m \frac{Fl^2}{2EI}$$

$$\begin{cases} -\frac{ql^3}{24EI} + \frac{X_1 l}{3EI} + \frac{X_2 l}{6EI} = 0 \\ -\frac{ql^3}{24EI} + \frac{X_2 l}{3EI} + \frac{X_1 l}{6EI} = 0 \end{cases}$$

PER TH. DI
BETTI.

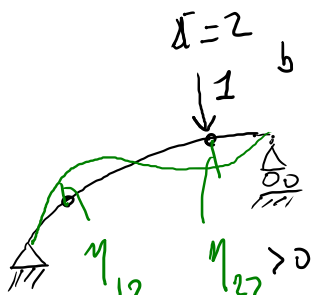
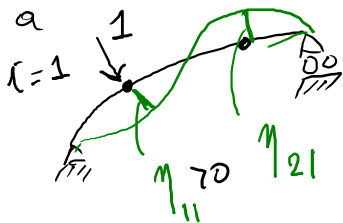
$$\begin{bmatrix} \frac{l}{3EI} & \frac{l}{6EI} \\ \frac{l}{6EI} & \frac{l}{3EI} \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} \frac{ql^3}{24EI} \\ \frac{ql^3}{24EI} \end{bmatrix}$$

BETTI $\eta_{12} = \eta_{21}$; $\eta_{11} > 0$; $\eta_{22} > 0$

COEFF DI INFLUENZA

$$\eta_{ii} > 0$$

COEFF DI INFLUENZA



$$1^a \cdot \eta_{12} = 1^b \cdot \eta_{21}$$

$$\Rightarrow \eta_{12} = \eta_{21}$$

TH. DI MAXWELL

η_{ij} = SPOST. NELLA DIREZ. i DOVUTO AD UNA FORZA UNITARIA NELLA DIREZ. j .

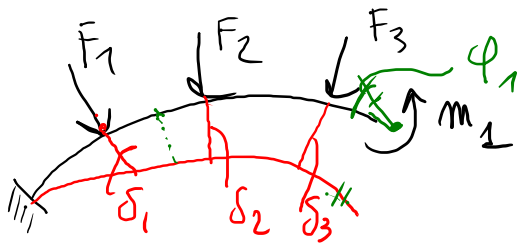
$$\eta_{12} = \text{DIR 1 FORZA LUNGO 2}$$

$$\eta_{21} = \text{DIR 2 FORZA LUNGO 1}$$

$$\eta_{11} = \text{DIR 1 FORZA LUNGO DIR 1}$$

TH. DI CASTIGLIANO

→ ATR



$$\Phi = \frac{1}{2} \int \frac{M^2}{EI} + \frac{N^2}{EA} = \Phi(F_1, F_2, \dots, m_1)$$

$$M, N = f(F_1, F_2, \dots, m_1)$$

STESSE IPOTESI TH. CLAPEYRON
CARICHI CONCENTRATI

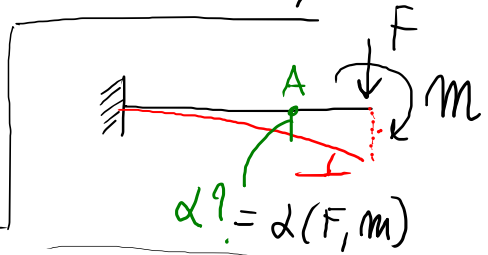
NO ATERMICHE
ATT. VINCOLI
ELASTICI

$$\frac{\partial \Phi(F_1, F_2, \dots)}{\partial F_i} = \delta_i$$

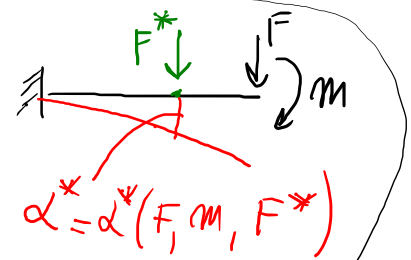
SPOSTAMENTO
CORRELATO
ALLA FORZA
 F_i

$$\frac{\partial \Phi}{\partial m_i} = \varphi_i$$

ROTAZ. CORRELATA
AL MOMENTO m_i



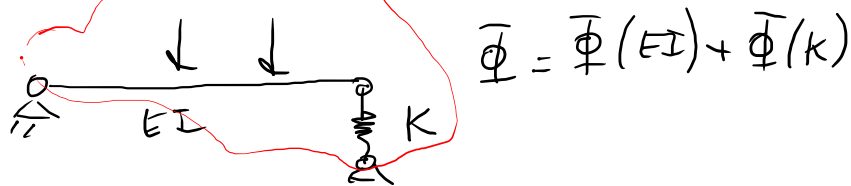
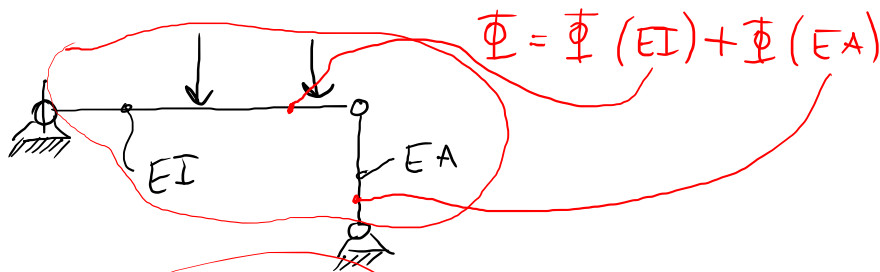
$$\alpha = \alpha(F, m)$$



$$\alpha^* = \alpha(F, m, F^*)$$

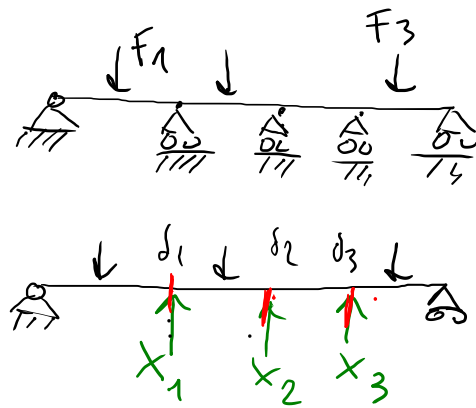
$$\alpha^* = \frac{\partial \Phi}{\partial F^*}$$

$$\alpha = \lim_{F^* \rightarrow 0} \alpha^* = \lim_{F^* \rightarrow 0} \frac{\partial \Phi}{\partial F^*}$$



TUTTA L'EN. ELASTICA DEL SIST.
VA CONSIDERATA ~~CON~~ NEL
TH. DI CASTIGLIANO

FRA TUTTI I POSSIBILI VALORI ATTRIBUIBILI
ALLE INCOGNITE X_i , L'INSIEME CHE
SODDISFA LA CONGRUENZA È QUELLO
CHE RENDE MINIMA L'ENERGIA ELASTICA.



VINCOLI FISSI
STR 3
VOLTE IPERSI.

S. PRINCIPALE
 $\Phi = \Phi(F_1, \dots, X_1, X_2, X_3)$

$$\left\{ \begin{array}{l} \delta_1 = 0 \\ \delta_2 = 0 \\ \delta_3 = 0 \end{array} \right. \begin{array}{l} \text{EQ DI} \\ \text{CONGR.} \\ (X_1, X_2, X_3) \end{array}$$

1
VINCOLI
FISSI

$$\left. \begin{array}{l} \frac{\partial \Phi}{\partial X_1} = 0 \\ \frac{\partial \Phi}{\partial X_2} = 0 \\ \frac{\partial \Phi}{\partial X_3} = 0 \end{array} \right\}$$

$$\Phi(\dots, X_1, X_2, X_3)$$

TH. DI MENABREA