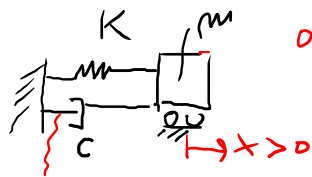


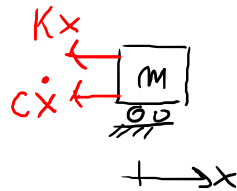
OSCILLATORE CON SMORZAMENTO (o CON DISSIPAZIONE)

23/11/22



OSCILLAZIONI LIBERE

$$m\ddot{x} = F$$



c: coeff di smorzamento viscoso

$$[c\dot{x}] = [\text{FORZA}]$$

$$[c] = \left[\frac{FT}{L} \right] \sim \frac{Ns}{m}$$

SMORZATORE (DASH POT)

EQ. DELLA DINAMICA

$$m\ddot{x} = -Kx - c\dot{x} \quad ; \quad \boxed{m\ddot{x} + c\dot{x} + Kx = 0}$$

$$\ddot{x} + \frac{2c}{2m\omega} \dot{x} + \omega^2 x = 0 \rightarrow \boxed{\ddot{x} + 2\nu\omega \dot{x} + \omega^2 x = 0} \quad ; \quad \nu = \frac{c}{2m\omega}$$

$$\omega = \sqrt{\frac{K}{m}}$$

$$\nu = \frac{c}{2m\omega} = \frac{c}{2\sqrt{Km}} = \frac{c}{c_{cr}}$$

ν : RAPPORTO DI SMORZAMENTO ; $[\nu] = [-]$

$c_{cr} = 2\sqrt{Km}$
 SMORZAMENTO CRITICO

$\nu \sim 0,03 \div 0,07$ nelle strutture civili.

$$\ddot{x} + 2\nu\omega\dot{x} + \omega^2x = 0 \quad ; \quad x(t) = e^{\lambda t} \quad ; \quad \dot{x} = \lambda e^{\lambda t} \quad ; \quad \ddot{x} = \lambda^2 e^{\lambda t}$$

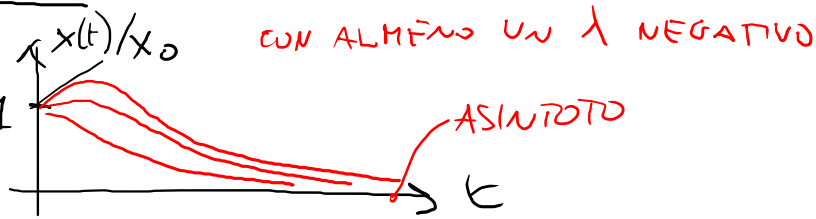
$$(\lambda^2 + 2\nu\omega\lambda + \omega^2)e^{\lambda t} = 0$$

λ_1, λ_2

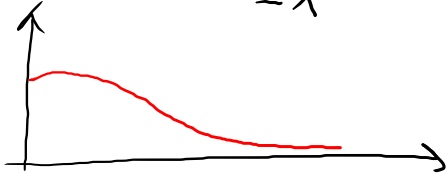
$$\lambda_{1,2} = -\nu\omega \pm \sqrt{\nu^2\omega^2 - \omega^2} = \omega \left(-\nu \pm \sqrt{\nu^2 - 1} \right)$$

$\nu > 1$ SMORZ. SUPERCRITICO
 $\nu = 1$ " CRITICO
 $\nu < 1$ " SOTTOCRITICO

$\nu > 1$: λ_1, λ_2 : REALI ; $x(t) = A_1 e^{\lambda_1 t} + A_2 e^{\lambda_2 t}$ *



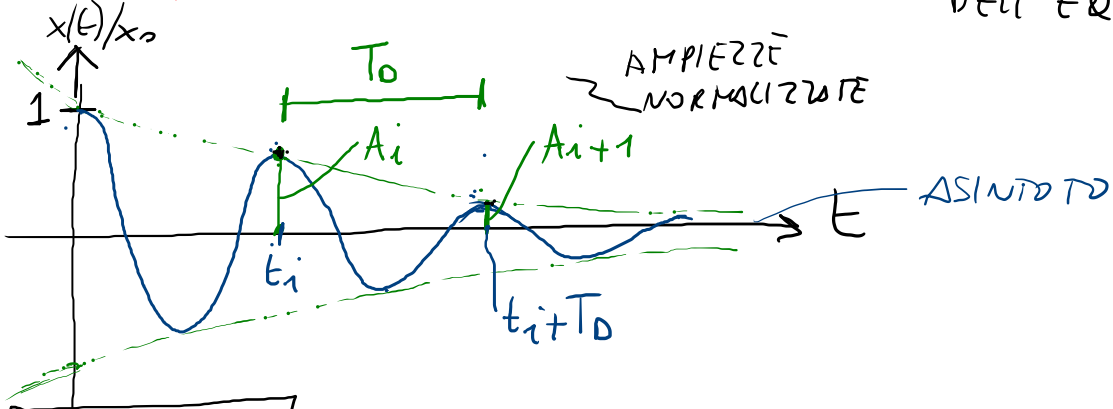
$\nu = 1$: $\lambda_1 = \lambda_2 = -\nu\omega = -\omega = \lambda$; LA SOLUZ. (*) NON VA PIU' BENE : $x(t) = A_1 e^{-\lambda t} + A_2 \lambda e^{-\lambda t}$



$$\boxed{\nu < 1}: x(t) = A_1 e^{-\nu \omega t + i \omega \sqrt{1-\nu^2} t} + A_2 e^{-\nu \omega t - i \omega \sqrt{1-\nu^2} t}$$

$$x(t) = \underbrace{e^{-\nu \omega t}}_{\text{MODULANTE}} \left(\underbrace{B_1 \sin \omega_D t + B_2 \cos \omega_D t}_{\text{OSCILLANTE}} \right)$$

MODO ALTERNATIVO
DI SCRIVERE
L'INT. GENERALE
DELL'EQ.



$$E_{mecc} = \frac{1}{2} K A^2$$

$$\Delta E_{mecc} = \frac{1}{2} K (A_{i+1}^2 - A_i^2) < 0$$

DECREMENTO
DI EN. MECC.
DEL SISTEMA.

$$\omega(-\nu \pm \sqrt{\nu^2 - 1})$$

$$\omega(-\nu \pm i \sqrt{1 - \nu^2})$$

$$\omega_D = \omega \sqrt{1 - \nu^2} \quad \text{PULSAZIONE RIDOTTA}$$

$$T_D = \frac{2\pi}{\omega_D} \quad \text{PERIODO RIDOTTO}$$

$$e^{i\omega_0 t} = \cos \omega_0 t + i \sin \omega_0 t$$

$$\omega_D < \omega ; T_D > T$$

$$\nu \rightarrow 0 \quad \omega_D \rightarrow \omega ; T_D \rightarrow T$$

$$\nu \rightarrow 1 ; \omega_D \rightarrow 0 ; T_D \rightarrow \infty$$

$$A_i = e^{-v\omega t_i}$$

$$A_{i+1} = e^{-v\omega(t_i + T_0)} = e^{-v\omega t_i} \cdot e^{-v\omega T_0} = A_i e^{-v\omega T_0}$$

$$\left| \frac{A_i}{A_{i+1}} = e^{v\omega T_0} \right| > 1$$

$$\frac{A_i}{A_{i+1}} = e^\delta ; \delta = v\omega T_0 : \text{DECREMENTO LOGARITMICO} ; \ln \frac{A_i}{A_{i+1}} = \delta$$

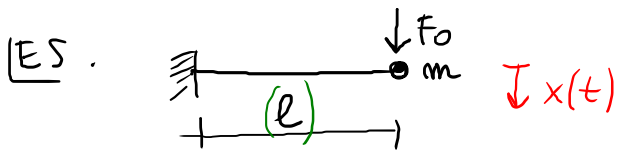
$$\text{STUDIO } v\omega T_0 = v \omega \frac{2\pi}{\omega \sqrt{1-v^2}} = \frac{2\pi v}{\sqrt{1-v^2}} ; \text{ SE } v \ll 1 \simeq 2\pi v$$

$$\text{ALLORA } \frac{A_i}{A_{i+1}} \simeq e^{2\pi v} ; \text{ MAE } e^{2\pi v} \simeq 1 + 2\pi v \quad (v \ll 1) \Rightarrow \frac{A_i}{A_{i+1}} \simeq 1 + 2\pi v$$

ESPRESS' APPROSS.

ESEMPIO DI
IDENTIFICAZIONE
STRUTTURALE

POSSO COLLEGARE v ATTRAVERSO IL
RAPPORTO TRA DUE AMPIEZZE CONSECUTIVE
DELLA FUNZIONE OSCILLANTE

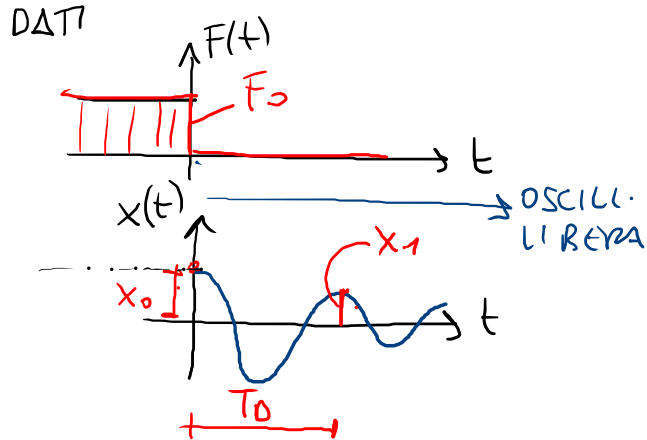


INCOGNITE
 m ? OK
 c ?
 K ? OK

PROPOSTA DI SOLUZ.
 $\nu = \frac{c}{2\sqrt{Km}}$

NOTO
 $\frac{x_0}{x_1} = 1 + 2\pi\nu \rightarrow \nu \approx 0.035$

NOTO
 $\omega = \frac{2\pi}{T_0} \frac{1}{\sqrt{1-\nu^2}} \rightarrow \omega \approx 4.49 \frac{\text{rad}}{\text{s}}$



$x_0 = 5 \text{ mm}$
 $x_1 = 4 \text{ mm}$
 $T_0 = 1.40 \text{ s}$
 $F_0 = 90 \text{ KN}$

$K = \frac{3EF}{l^3}$

$\omega^2 = \frac{K}{m}$

LA SOLUZ. STATICA ($t \leq 0$) E' :

$Kx_0 = F_0 + mg$

$Kx_0 = F_0 + \frac{K}{\omega^2}g \Rightarrow K$

$m = \frac{K}{\omega^2} \Rightarrow m$

NOTO
 $c = \nu \cdot 2 \sqrt{Km} \Rightarrow c$

