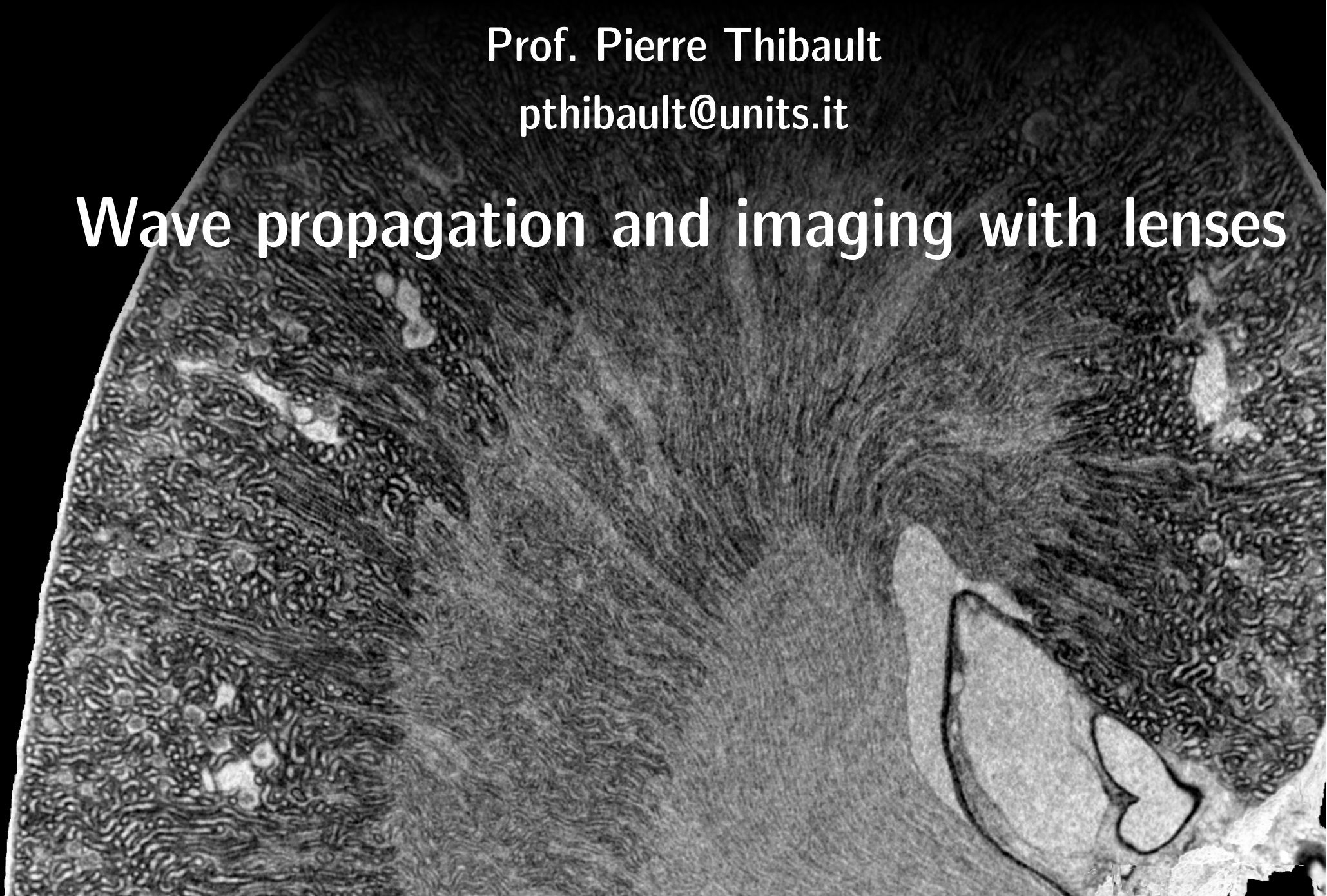


Image Processing for Physicists

Prof. Pierre Thibault

pthibault@units.it

Wave propagation and imaging with lenses



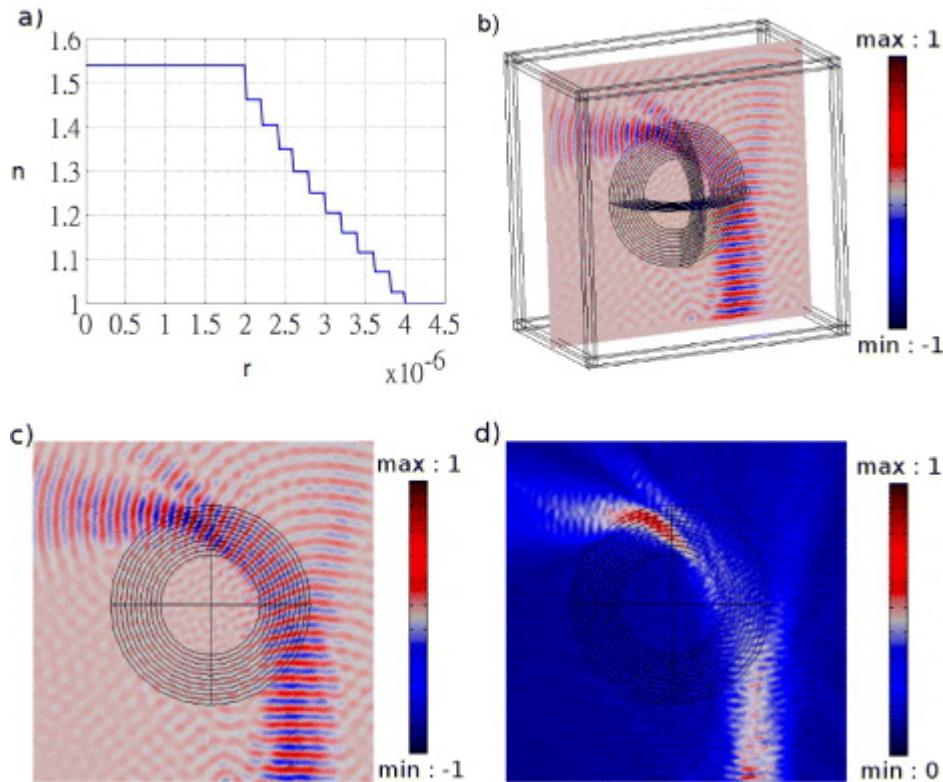
Overview

- Propagation modelization
- Wave propagation:
 - Near-field regime
 - Far-field regime

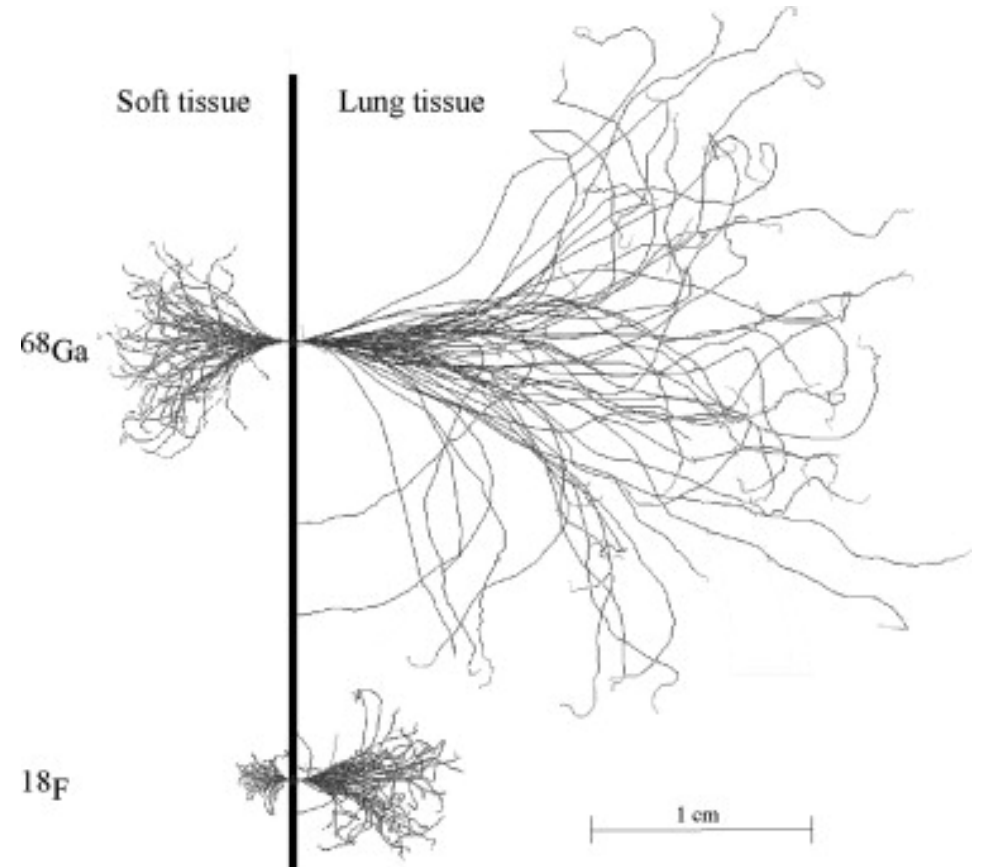
Propagation modeling

- Motivations:

1. Validation



Finite element simulation of an electromagnetic field in a dielectric



Monte Carlo simulation of positrons trajectories resulting from ^{68}Ga and ^{18}F decay.

sources: T.M. Chang *et al.* New J. Phys. (2012)
A. Sanchez-Crespo, Appl. Rad. Isotopes (2012)

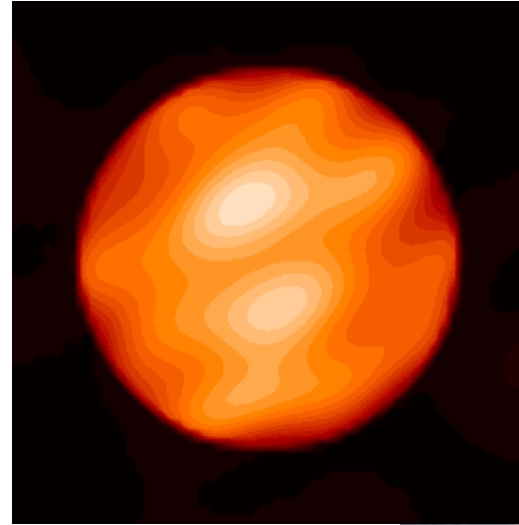
Propagation modeling

- Motivations:

2. Inversion



Image reconstruction from sound wave propagation (ultrasonography)



The surface of Betelgeuse reconstructed from interferometric data (IOTA)



sources: wikipedia

Haubois *et al.* *Astronom. & Astrophys.* (2009)

Propagation modeling

- Particles
 - Model particle tracks (rays) through different media
 - Model may include: refraction, force fields, particle decay and interactions
 - Not included: diffraction
- Wave
 - Model the interaction of a field with a medium
 - Can be very complicated → approximations are needed

Propagation modeling

Starting point: Helmholtz equation

- for EM field: neglect polarization (scalar wave approximation) \leftarrow Maxwell's equations
- for electron wave, assume high energy electrons

Maxwell approximation as a scalar field:

$$\nabla^2 \psi + \frac{n^2}{c^2} \frac{\partial^2}{\partial t^2} \psi = 0$$

$\psi \rightarrow$ electric field

ψ : complex-valued scalar field

n : index of refraction

c : speed of light

For n constant: plane wave solutions

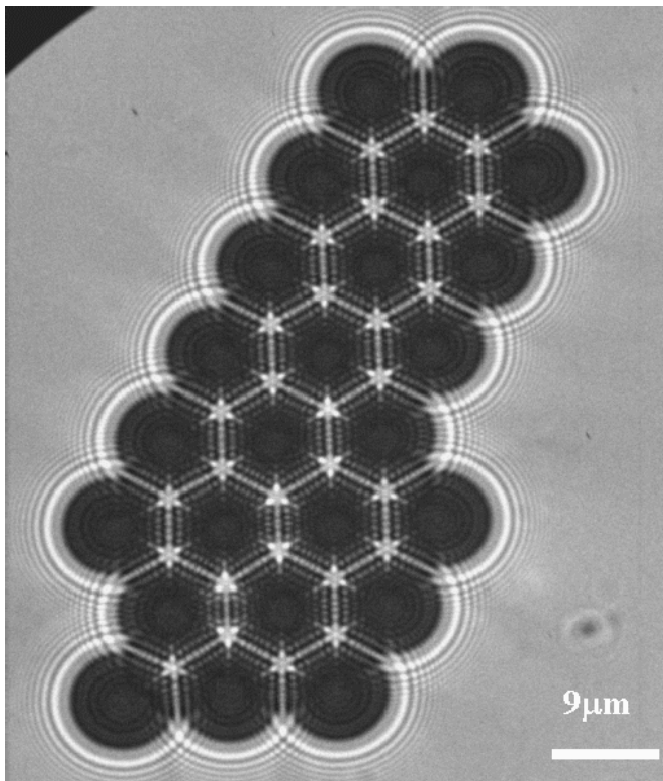
$$\psi(\vec{r}) = \psi_0 e^{i(\vec{k} \cdot \vec{r} - \omega t)}$$

(dispersion relation: $k^2 = \frac{n^2 \omega^2}{c^2}$)

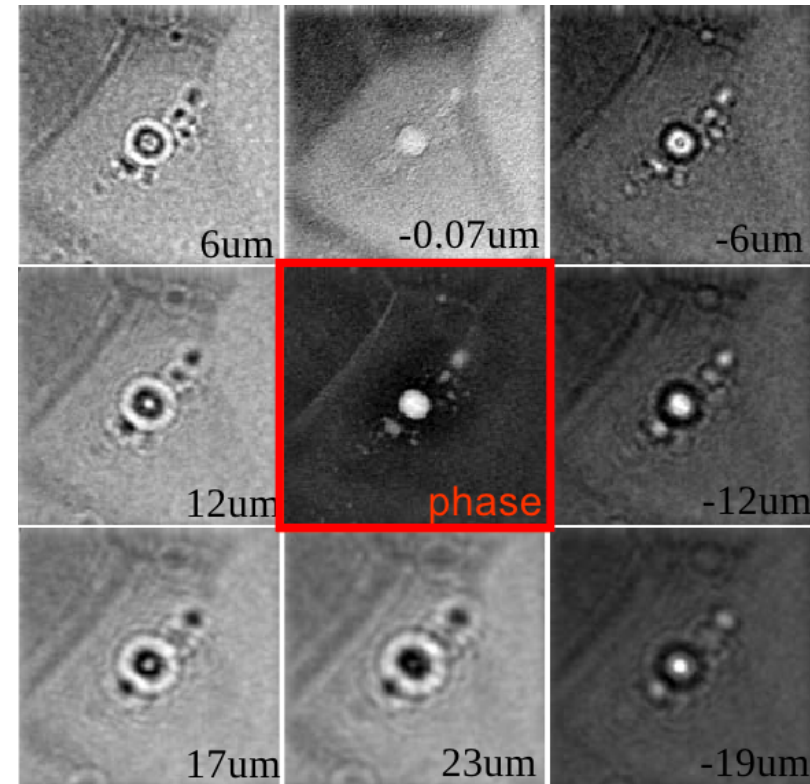
Propagation modeling

- Useful to:
 - better understand optical systems
 - understand diffraction, holography, phase contrast, interferometry, ...

X-ray hologram



TEM through-focus series



sources: Mayo *et al.* Opt. Express (2003)
<http://www.christophtkoch.com/Vorlesung/>

The physics of propagation

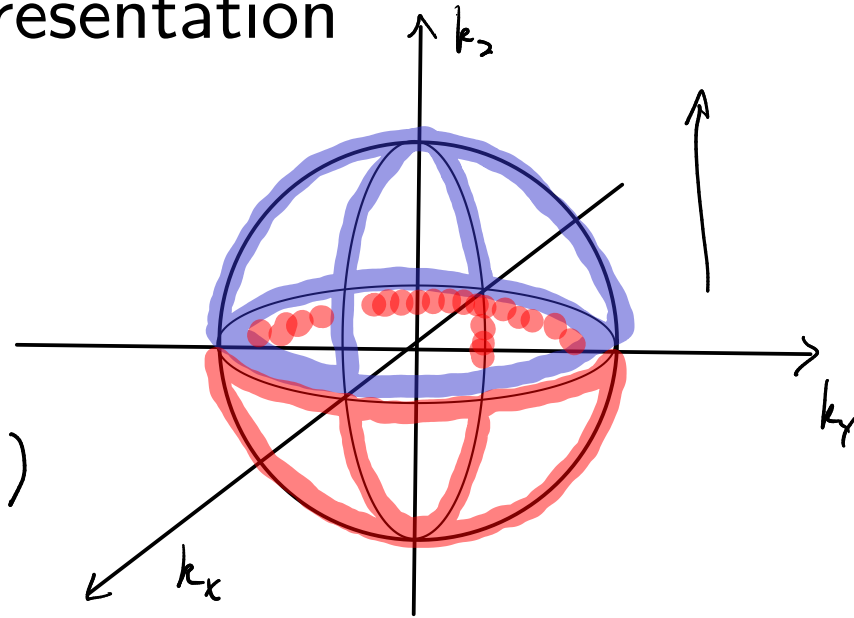
Angular spectrum representation

constant

$$k_z = \begin{matrix} + \\ - \end{matrix} \sqrt{k^2 - k_x^2 - k_y^2}$$

$$\psi(\vec{r}) = \sum_{k_x, k_y} A_{k_x, k_y}^+ e^{i(k_x x + k_y y + \sqrt{k^2 - k_x^2 - k_y^2} z)}$$

$$+ \sum_{k_x, k_y} A_{k_x, k_y}^- e^{i(k_x x + k_y y - \sqrt{k^2 - k_x^2 - k_y^2} z)}$$



Consider only propagation towards positive k_z

$$\vec{r}_\perp = (x, y)$$

$$\psi(\vec{r}_\perp; z) = \sum_{\vec{k}_\perp} A_{\vec{k}_\perp} e^{i\vec{k}_\perp \cdot \vec{r}_\perp} e^{i\sqrt{k^2 - k_\perp^2} z}$$

2D Fourier transform!

Fourier synthesis equation
for any propagating
wavefield

Forward propagation

Case $z=0$: $\Psi(\vec{r}_\perp; z=0) = \sum_{\vec{k}_\perp} A_{\vec{k}_\perp} \exp(i\vec{k}_\perp \cdot \vec{r}_\perp)$

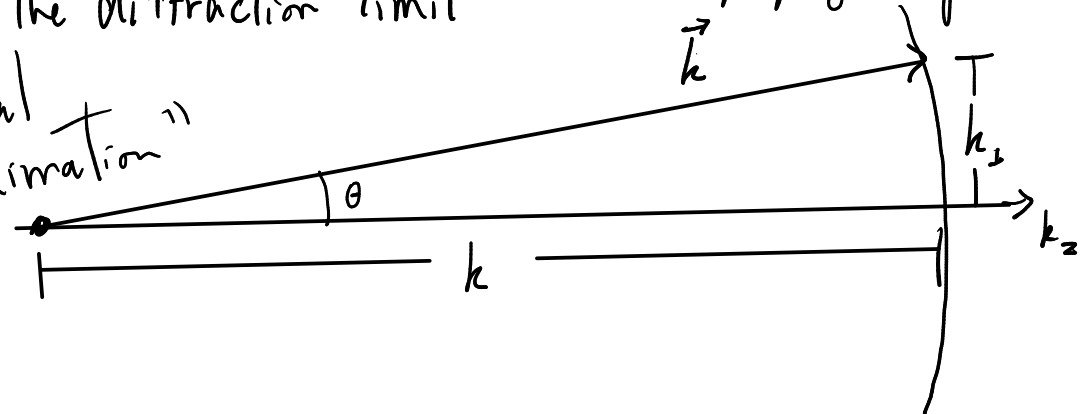
inverse Fourier transform for Ψ

$\Rightarrow A_{\vec{k}_\perp} = \mathcal{F}\{\Psi(\vec{r}_\perp; z=0)\}$ ← Formula to compute the amplitude of each plane wave component in the propagating wave field

One last approximation: it is often the case that $|k_\perp| \ll k$ far from the "diffraction limit"

$$\begin{aligned} \Rightarrow \sqrt{k^2 - k_\perp^2} &= k \sqrt{1 - \frac{k_\perp^2}{k^2}} \\ &\approx k \left(1 - \frac{1}{2} \frac{k_\perp^2}{k^2}\right) \\ &= k - \frac{k_\perp^2}{2k} \end{aligned}$$

"paraxial approximation"



$$\exp(i\sqrt{k^2 - k_\perp^2} z) = \underbrace{\exp(ikz)}_{\text{irrelevant for us}} \underbrace{\exp\left(\frac{-iz k_\perp^2}{2k}\right)}_{\text{"Fresnel propagator"}}$$

Since $k = \frac{2\pi}{\lambda}$, we are assuming that the relevant spatial frequencies in $\Psi(\vec{r}_\perp; z=0)$ are such that $|\vec{u}| \ll \frac{1}{\lambda}$

Forward propagation

Recipe:
$$\Psi(\vec{r}_\perp; z) = \mathcal{F}^{-1} \left\{ \mathcal{F} \left\{ \Psi(\vec{r}_\perp; z=0) \right\} \exp\left(\frac{-iz k_\perp^2}{2k}\right) \right\}$$

Discretization for implementation on a computer:

Trick #1: F.T.
$$e^{i\vec{k}_\perp \cdot \vec{r}_\perp} \rightarrow e^{2\pi i \vec{u} \cdot \vec{r}} \quad \vec{k}_\perp = 2\pi \vec{u}$$

↓
DFT

$$e^{2\pi i (m_x n_x / N + m_y n_y / N)} \quad \left(m_x \frac{n_x}{N} = u_x x \right)$$

Trick #2: Discretization

$$x = m_x \Delta x$$

 ↙ sampling pitch (space between pixels)

$$u_x = n_x \Delta u$$

$$\frac{m_x n_x}{N} = m_x n_x \Delta x \Delta u$$

Put all this together:

$$\Delta u = \frac{1}{N \Delta x}$$

$$\Delta x \Delta u = \frac{1}{N}$$

$$\exp\left(\frac{-iz k_\perp^2}{2k}\right) = \exp\left(-iz \frac{4\pi^2 u^2}{2\left(\frac{2\pi}{\lambda}\right)}\right) = \exp(-iz \pi \lambda u^2) = \exp(-iz \pi \lambda n_x^2 \Delta u^2)$$

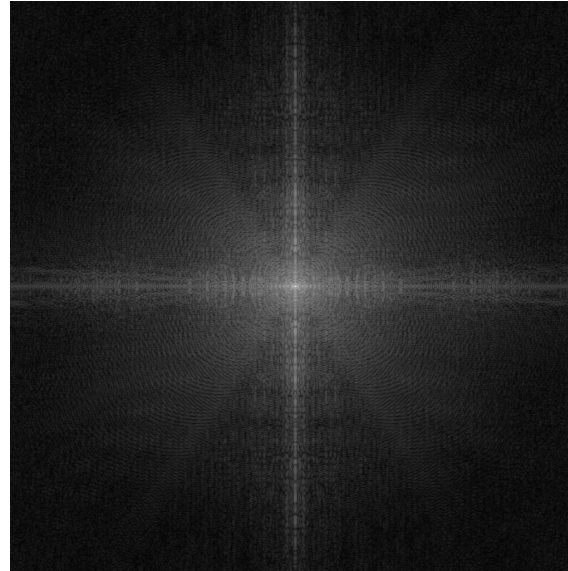
$$= \exp\left(-i\pi \left(\frac{z}{\Delta x}\right) \left(\frac{\lambda}{\Delta x}\right) \left(\frac{n_x}{N}\right)^2\right)$$

Forward propagation

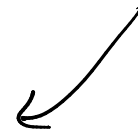
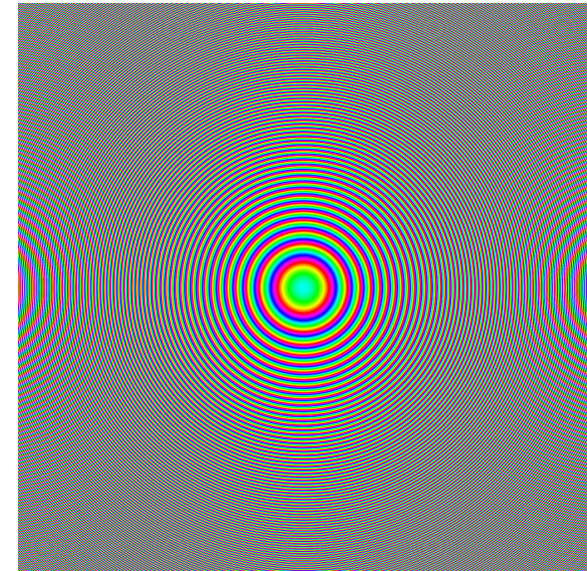
A numerical recipe

$\frac{n_x}{N}$: numpy.fft.
fft freq

$$\psi(\vec{r}_\perp; z=0)$$



$$\times \exp\left(\frac{-izk_\perp^2}{2k}\right)$$



Near field, far field

$$\psi(\vec{r}_\perp; z) = \mathcal{F}^{-1} \left\{ \mathcal{F} \left\{ \psi(\vec{r}_\perp; z=0) \right\} \exp \left(-\frac{izk_\perp^2}{2k} \right) \right\}$$

convolution!

$$= \psi(\vec{r}_\perp; z=0) * P_z(\vec{r}_\perp)$$

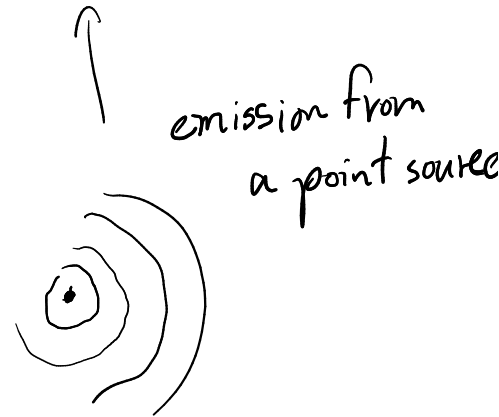
$$\mathcal{F}^{-1} \left\{ \exp(-i\pi \lambda z u^2) \right\}$$

$$\equiv \frac{-2\pi i}{\lambda z} \exp\left(i\pi \frac{r^2}{\lambda z}\right)$$

$$\psi(\vec{r}; z) = \frac{-2\pi i}{\lambda z} \int d^2 r' \psi(\vec{r}'; z=0) \exp\left(\frac{i\pi (\vec{r} - \vec{r}')^2}{\lambda z}\right)$$



"Fresnel - Huygens integral"

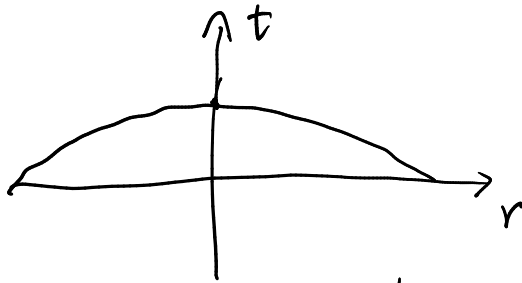


emission from a point source

Back focal plane of a lens

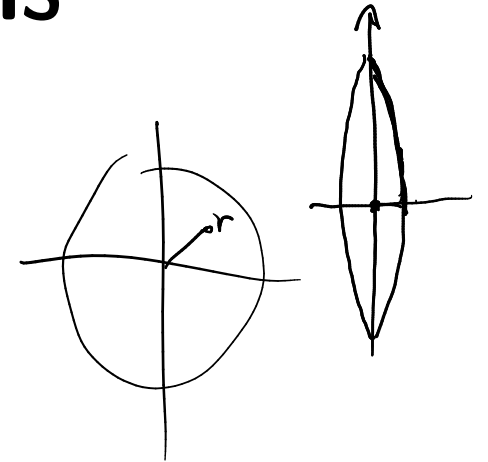
$\alpha > 0$: convergent

* model for a thin lens thickness profile:



$$t(r) = t_0 - \alpha r^2$$

↑ curvature of the lens profile



* phase of wavefield passed the lens

$n-1$: phase difference with respect to air

$$(\phi = k(n-1)t)$$

$$\phi(\vec{r}_\perp) = \frac{2\pi}{\lambda} (n-1) t(\vec{r}_\perp)$$

$$= \frac{2\pi}{\lambda} (n-1) t_0 - \frac{2\pi}{\lambda} (n-1) \alpha r_\perp^2$$

* at exit of lens:

$$\psi(\vec{r}_\perp) = \psi_0(\vec{r}_\perp) \cdot \exp(-ik(n-1)\alpha r_\perp^2)$$

↑ doesn't matter

* propagate further:

$$\psi(\vec{r}_\perp; z) = \frac{-2\pi i}{\lambda z} \int d^2r' \psi_0(\vec{r}') \exp\left(-ik(n-1)\alpha \vec{r}'^2\right) \exp\left(\frac{i\pi(\vec{r}-\vec{r}')^2}{\lambda z}\right)$$

↑ $\frac{2\pi}{\lambda}$

★

Back focal plane of a lens

definition
 $(n-1)\alpha := \frac{1}{2f}$

$$* = \exp \left[\frac{2\pi i}{\lambda} \left(\overbrace{-\frac{1}{2f} r^2} + \frac{(r^2 - 2\vec{r} \cdot \vec{r}' + r'^2)}{2z} \right) \right]$$

focal distance

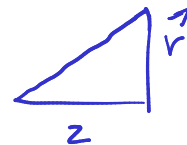
$$= \exp\left(\frac{i\pi r^2}{\lambda z}\right) \exp\left(\frac{i\pi}{\lambda} \left(\frac{1}{z} - \frac{1}{f}\right) r'^2\right) \exp\left(\frac{2\pi i \vec{r} \cdot \vec{r}'}{\lambda z}\right)$$

$$\Psi(\vec{r}_\perp; z) = \frac{-2\pi i}{\lambda z} \exp\left(\frac{i\pi r^2}{\lambda z}\right) \int d^2 r' \psi_0(\vec{r}') \underbrace{\exp\left(\frac{i\pi}{\lambda} \left(\frac{1}{z} - \frac{1}{f}\right) r'^2\right)} \exp\left(2\pi i \vec{r}' \cdot \left(\frac{\vec{r}}{\lambda z}\right)\right)$$

* Interesting: $z = f \quad \frac{1}{z} - \frac{1}{f} = 0$

$f=0$: no lens
 $z \rightarrow \infty$: F.T.
 far-field propagation

$$\begin{aligned} \hookrightarrow \Psi(\vec{r}_\perp; z=f) &= \dots \int d^2 r' \psi_0(\vec{r}') \exp\left(2\pi i \vec{r}' \cdot \left(\frac{\vec{r}}{\lambda z}\right)\right) \\ &= \dots \tilde{\mathcal{F}}\{\psi\}\left(\vec{u} = \frac{\vec{r}}{\lambda z}\right) \end{aligned}$$

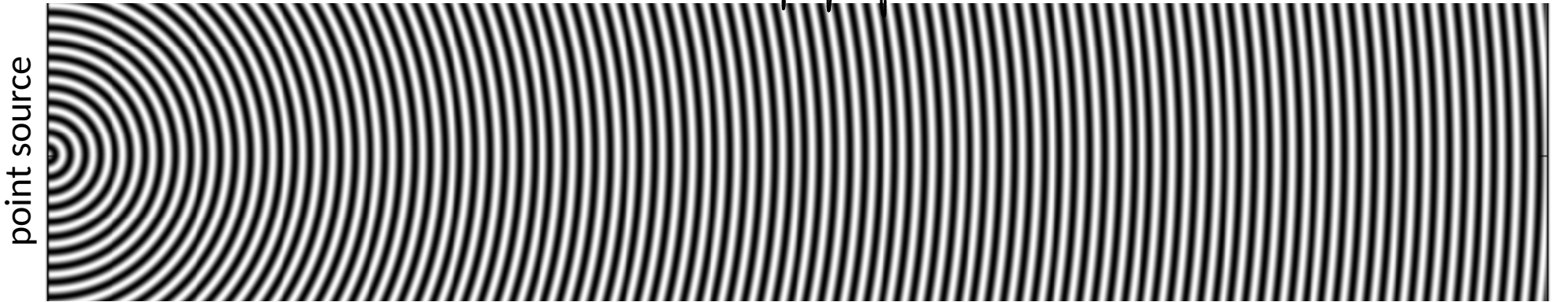


Wave propagation A lens acts as a Fourier transform operator!

Plane waves, point sources

$$\Psi(r_{\perp}^2; z \rightarrow \infty) = \frac{2\pi i}{\lambda z} \exp\left(\frac{i\pi r^2}{\lambda z}\right) \int \left\{ \Psi_0(\vec{r}) \right\} \left(\vec{u} = \frac{\vec{r}}{\lambda z} \right)$$

↑
Far-field propagation



circular waves
evanescent waves
contact region

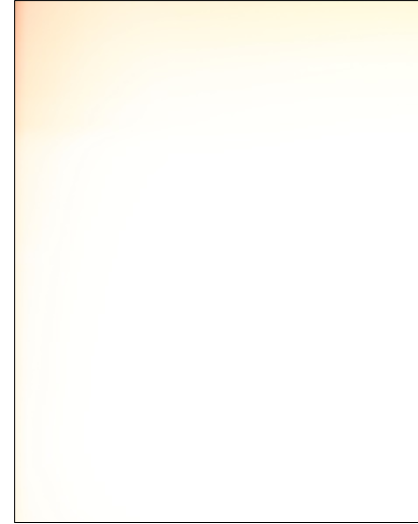
parabolic waves
near field
Fresnel region

plane waves
far field
Fraunhofer region

Why optical elements?



with objective lens

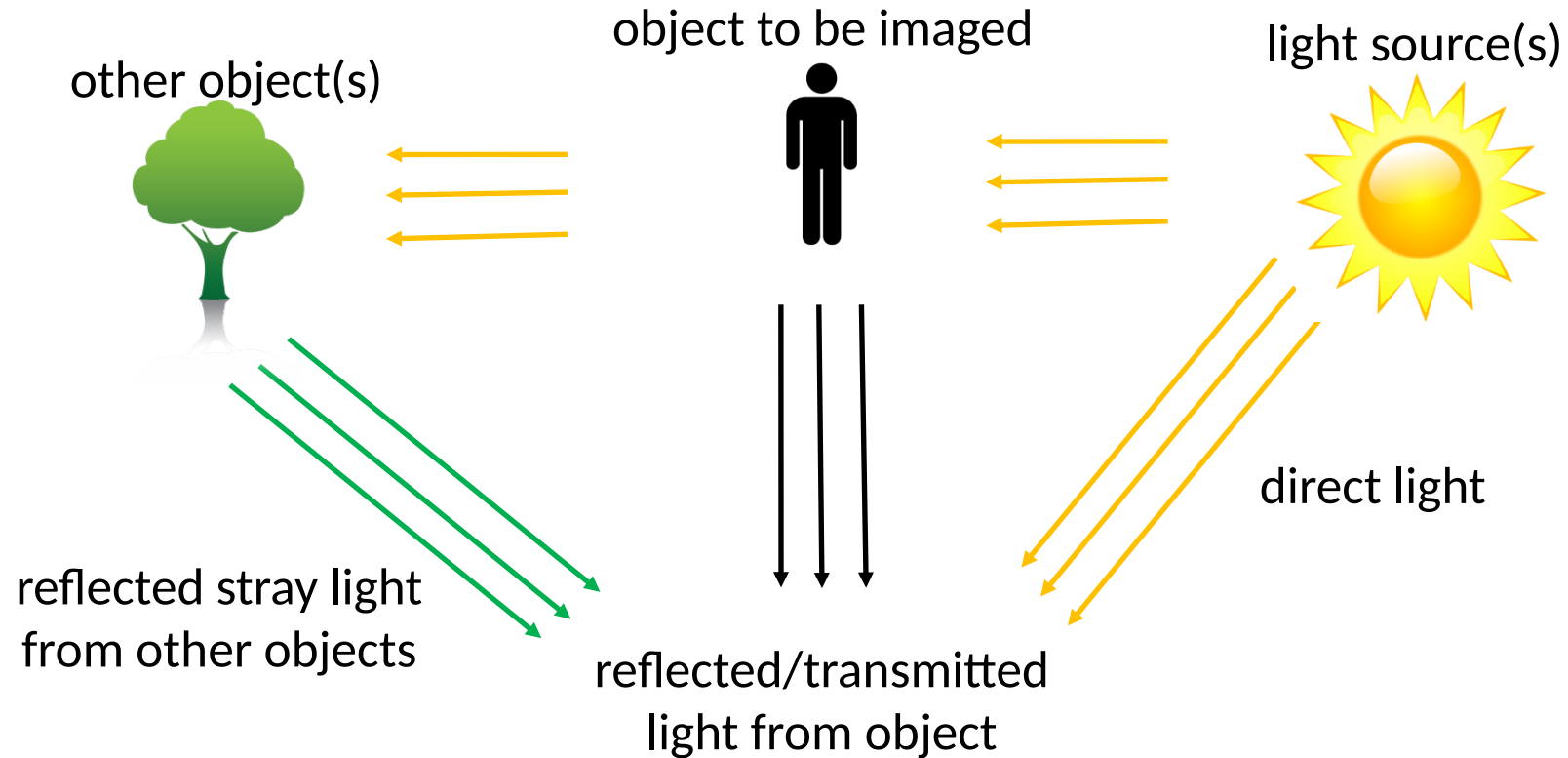


without objective lens



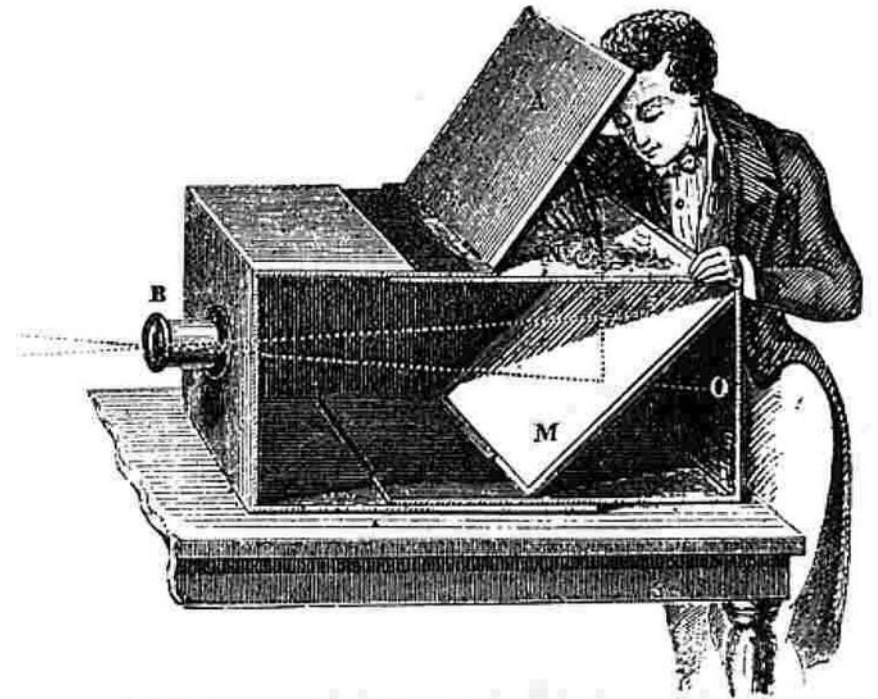
Why optical elements?

- Information from many sources overlaps in detector plane
- Need models to understand image forming systems



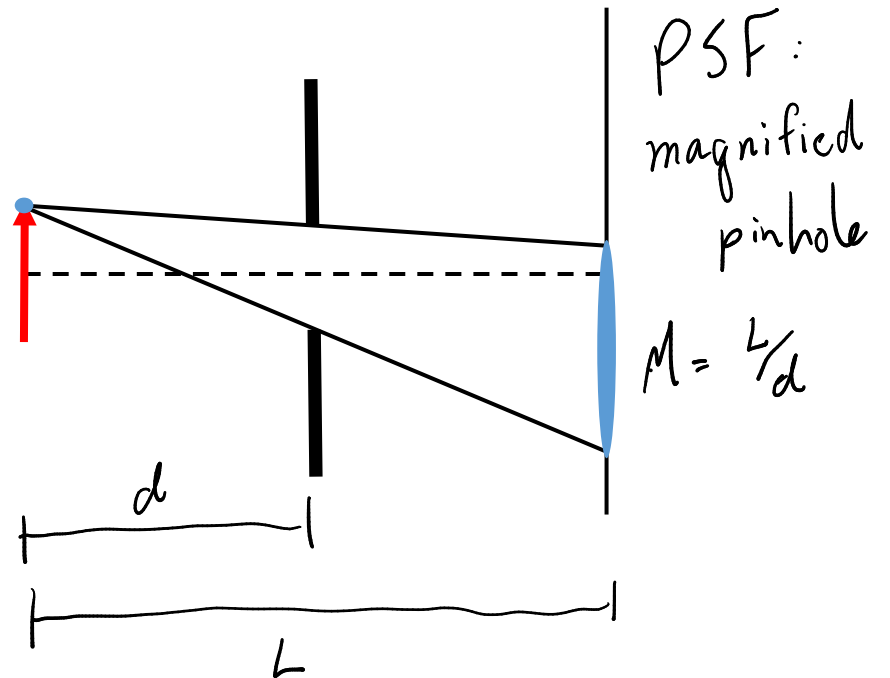
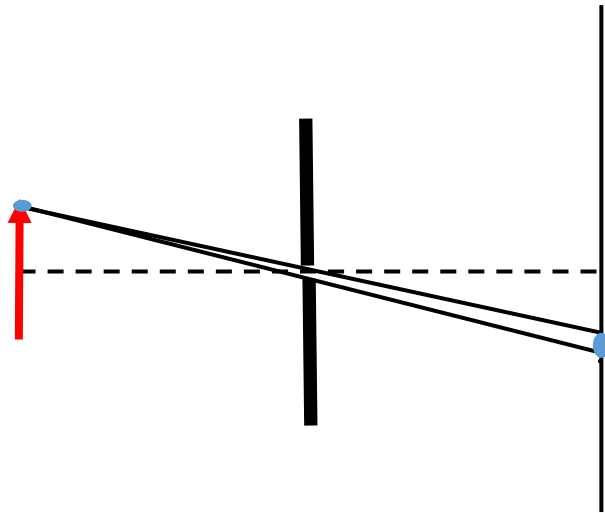
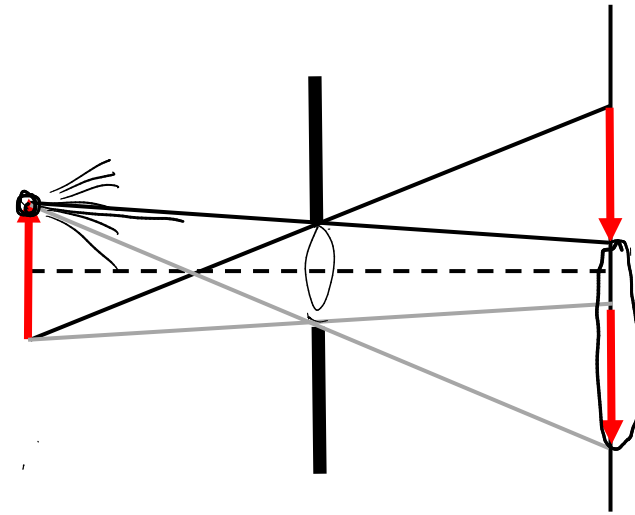
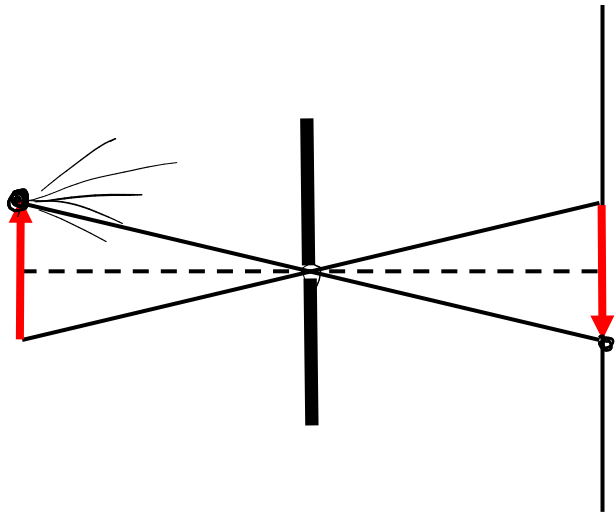
Pinhole camera model

camera obscura



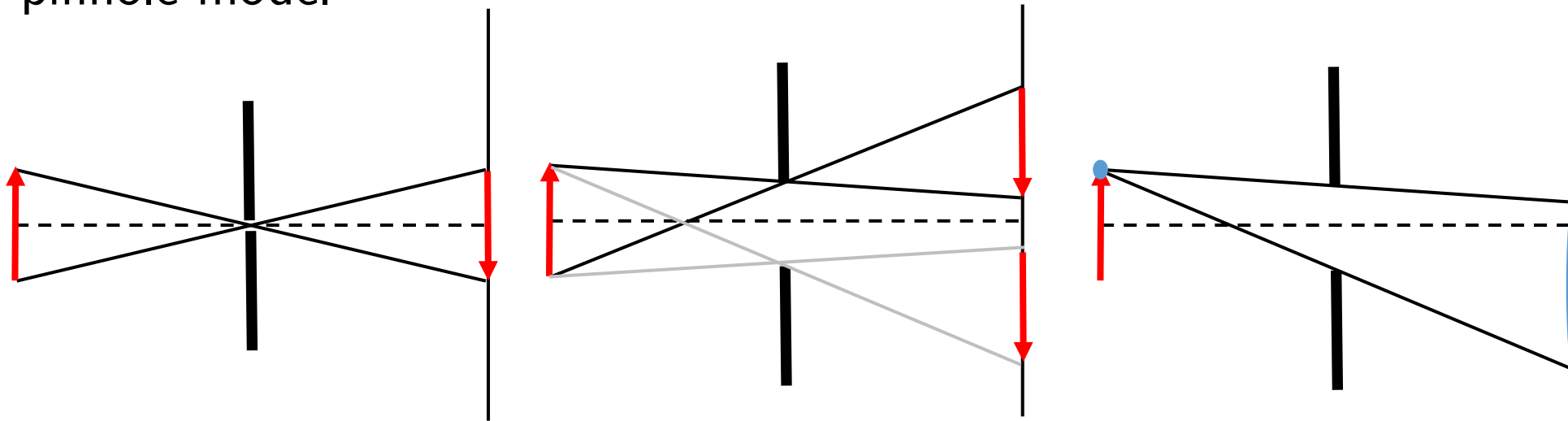
Pinhole camera model

PSF determined by aperture width

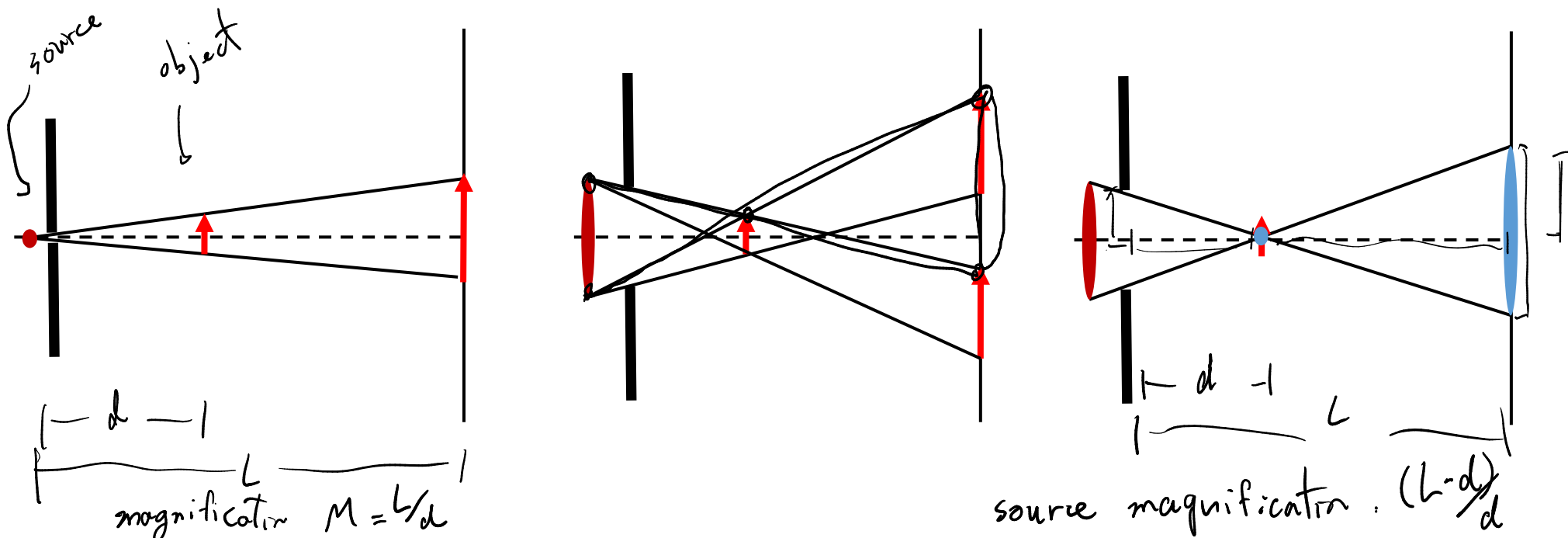


Projection model

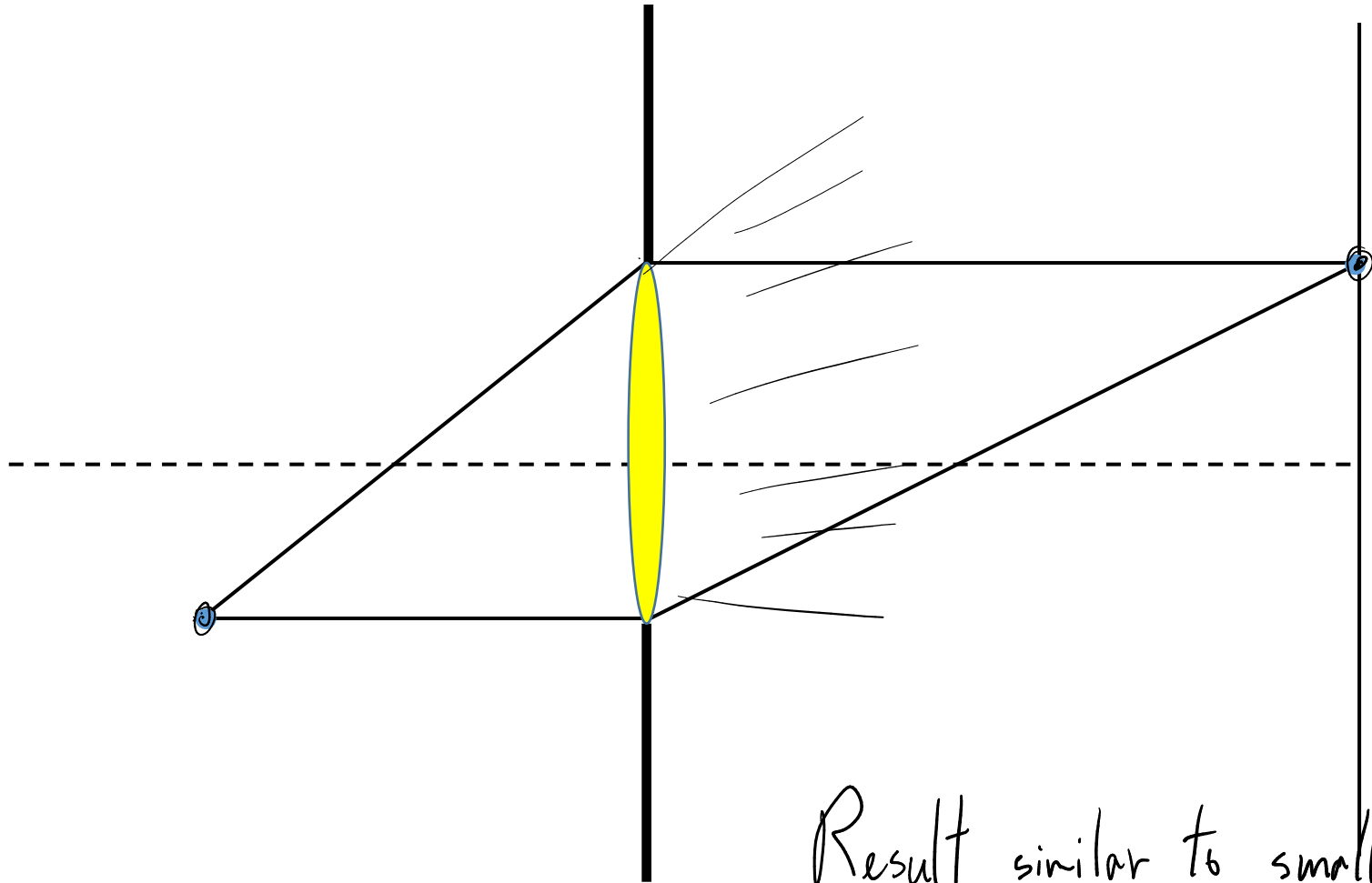
pinhole model



projection model



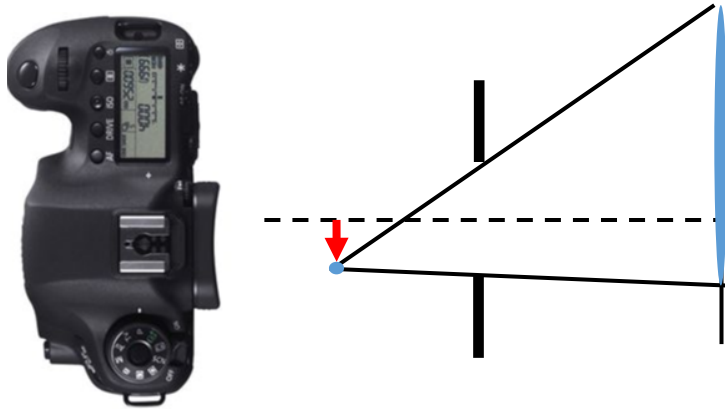
Lens camera model



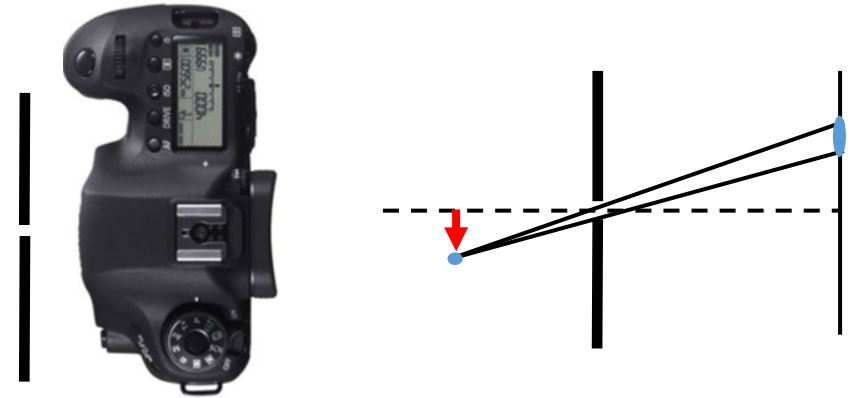
Result similar to small pinhole
but without compromise on intensity

Lens camera model

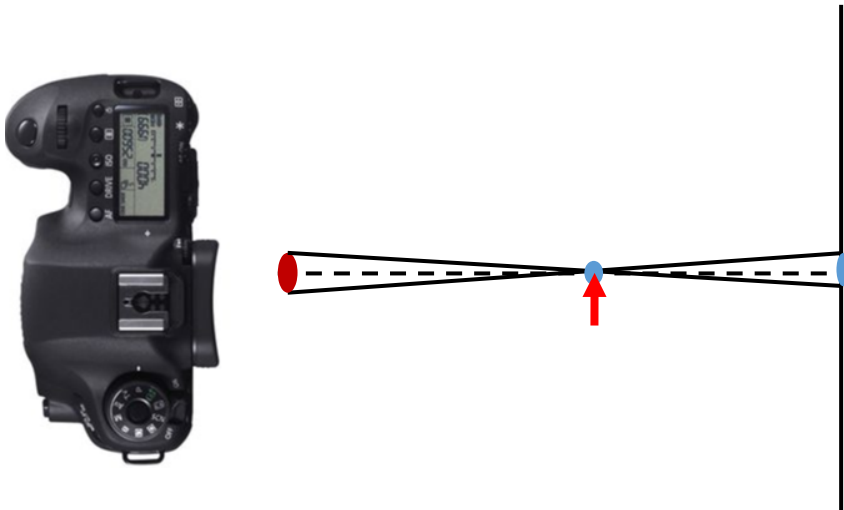
lensless model



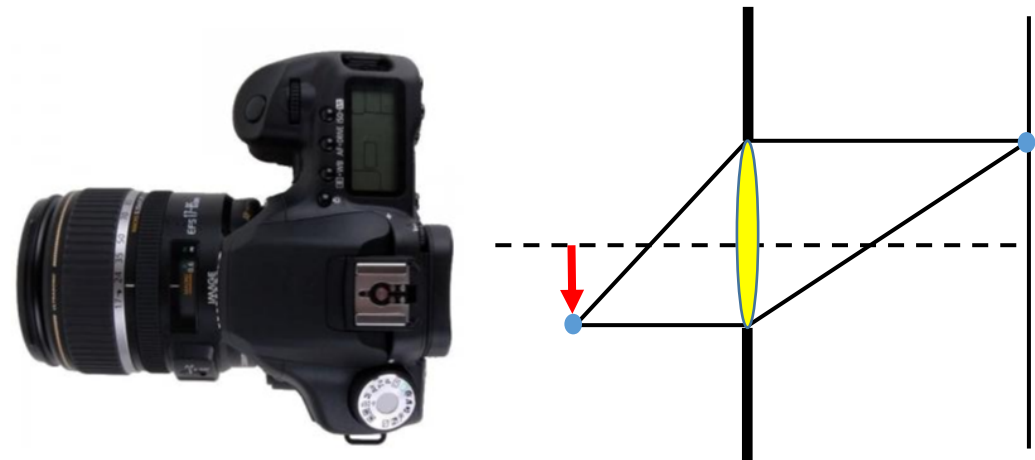
pinhole camera model



projection model

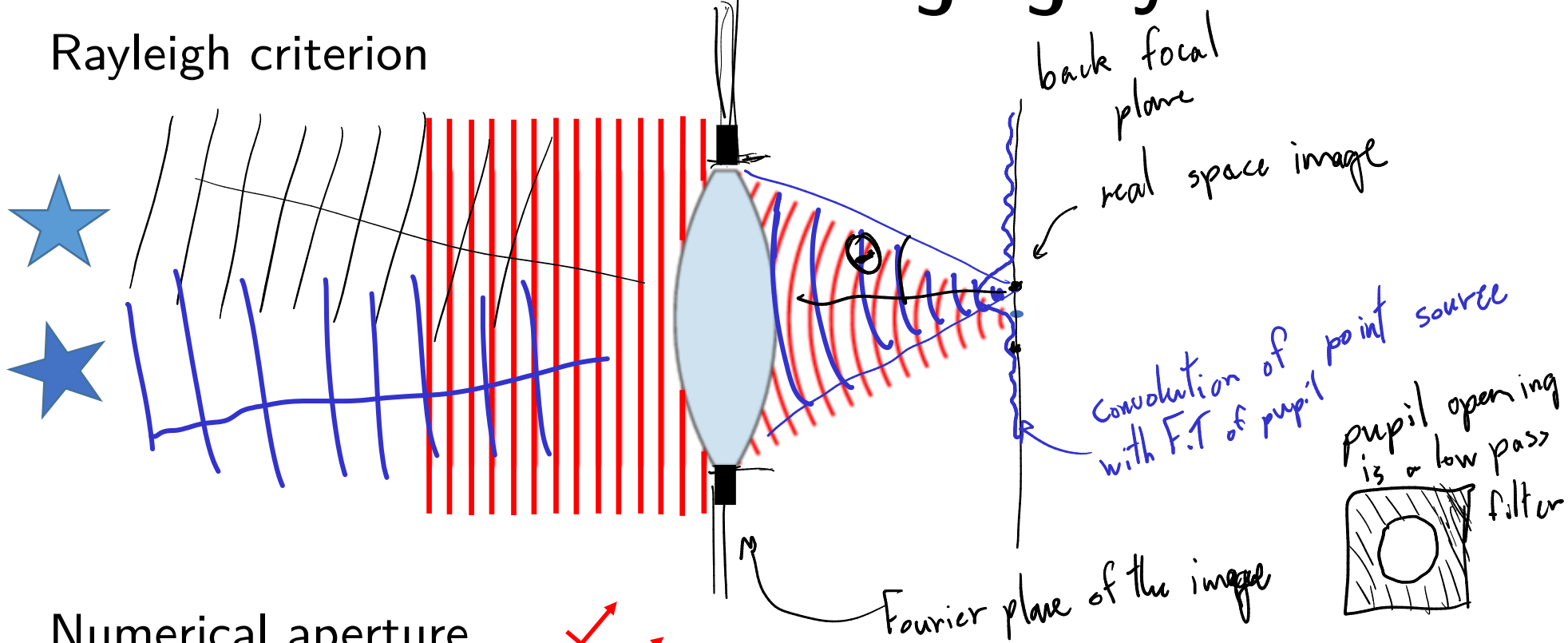


lens camera model

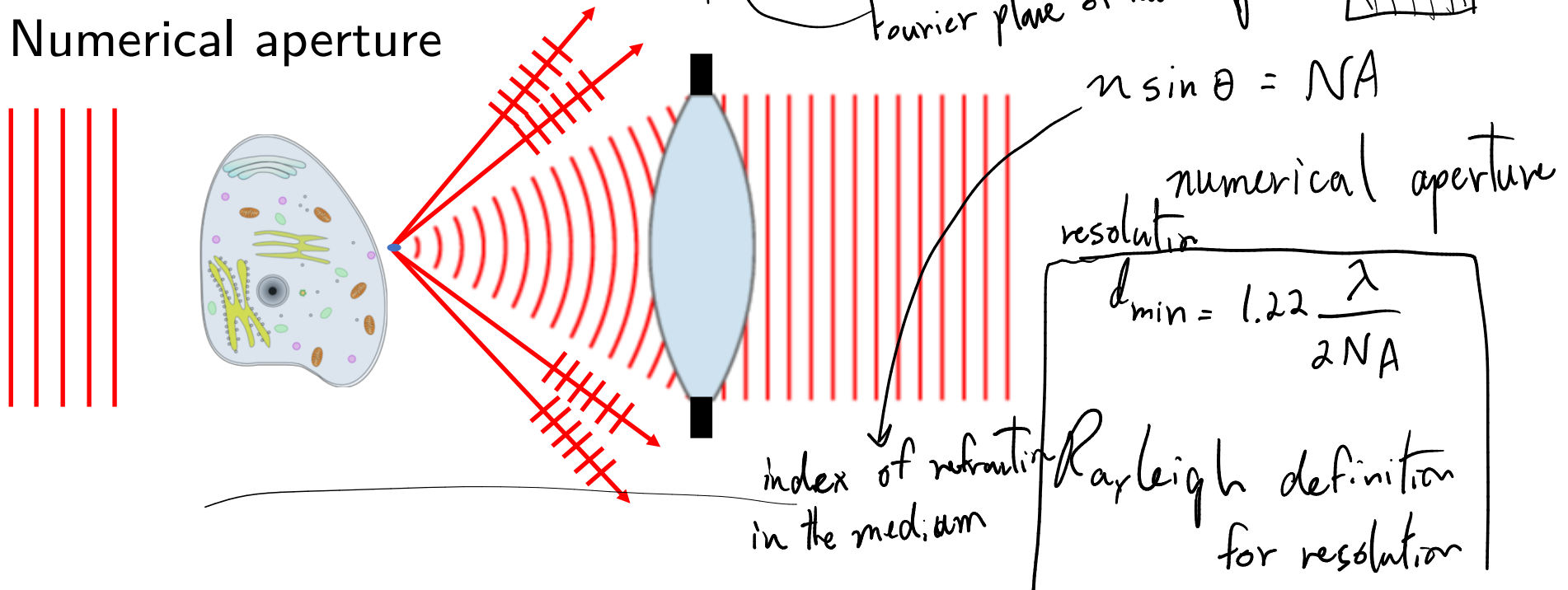


Diffraction-limited imaging systems

- Rayleigh criterion



- Numerical aperture

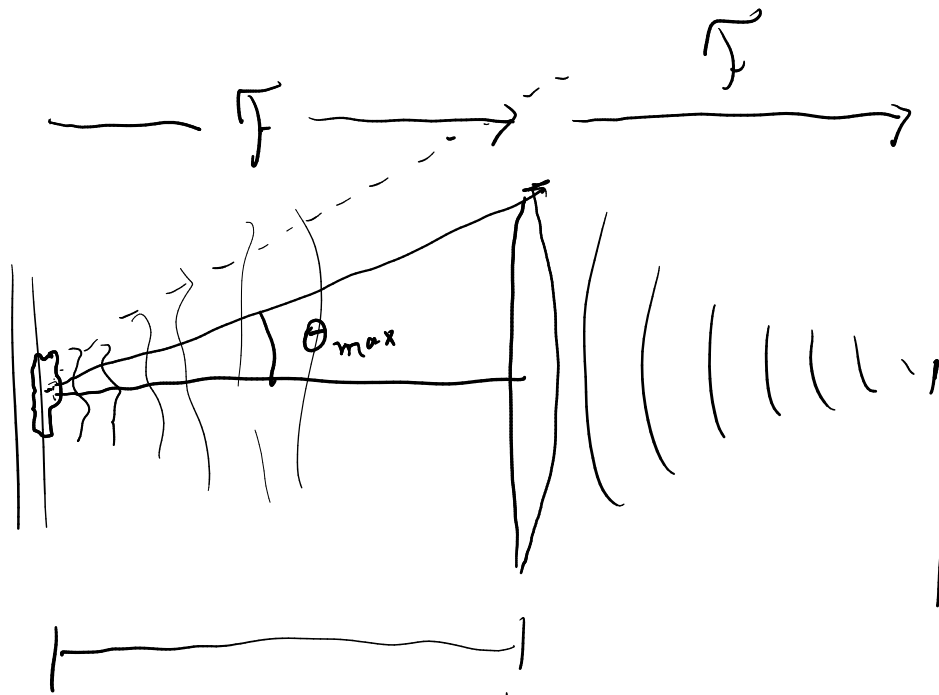


$$n \sin \theta = NA$$

resolution

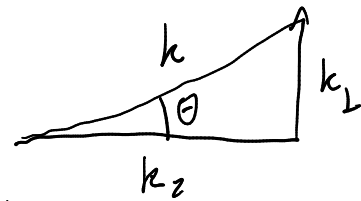
$$d_{\min} = 1.22 \frac{\lambda}{2NA}$$

Rayleigh definition for resolution



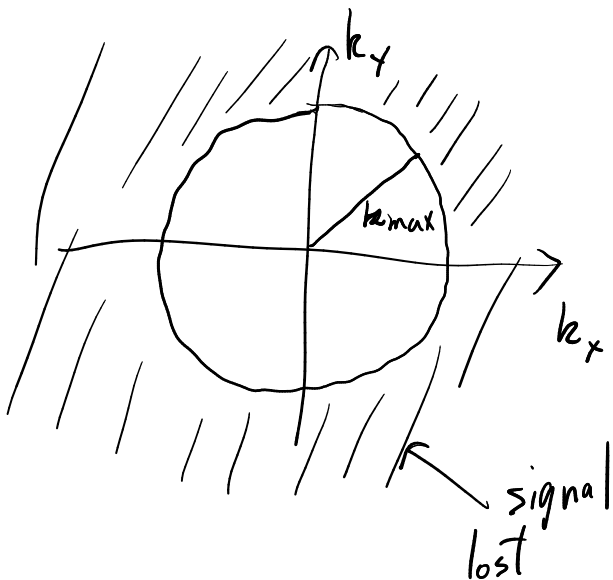
small object \Rightarrow Fraunhofer regime already in the lens plane

Far field:



$$\sin \theta_{\max} = \frac{k_{\max}}{k}$$

maximum spatial frequency captured by a lens with opening given by θ_{\max}



F.T. of disc radius k_{\max} :

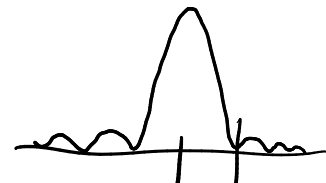
J_1 = First Bessel function

$$\frac{J_1(r k_{\max})}{r k_{\max}}$$

Rayleigh: resolution = distance of first 0 from origin $J_1(3.83) = 0$

$$r_{\min} k_{\max} = 3.83$$

$$PSF = \left| \frac{J_1(r k_{\max})}{r k_{\max}} \right|^2 \text{ PSF!}$$



Scanning systems

Transmission

- **Scanning Transmission Electron Microscopy**
- **Scanning Transmission X-ray Microscopy**
- ...

Indirect (reflection, scattering, fluorescence, ...)

- **Laser Scanning Confocal Microscopy**
- **Scanning Electron Microscopy**
- **X-ray Fluorescence Microscopy**
- **PhotoEmission Electron Microscopy**
- ...

Physical probe

- **Atomic Force Microscopy**
- **Scanning Tunneling Microscopy**
- ...

$$r_{\min} = \frac{3.83}{k \sin \theta_{\max}}$$

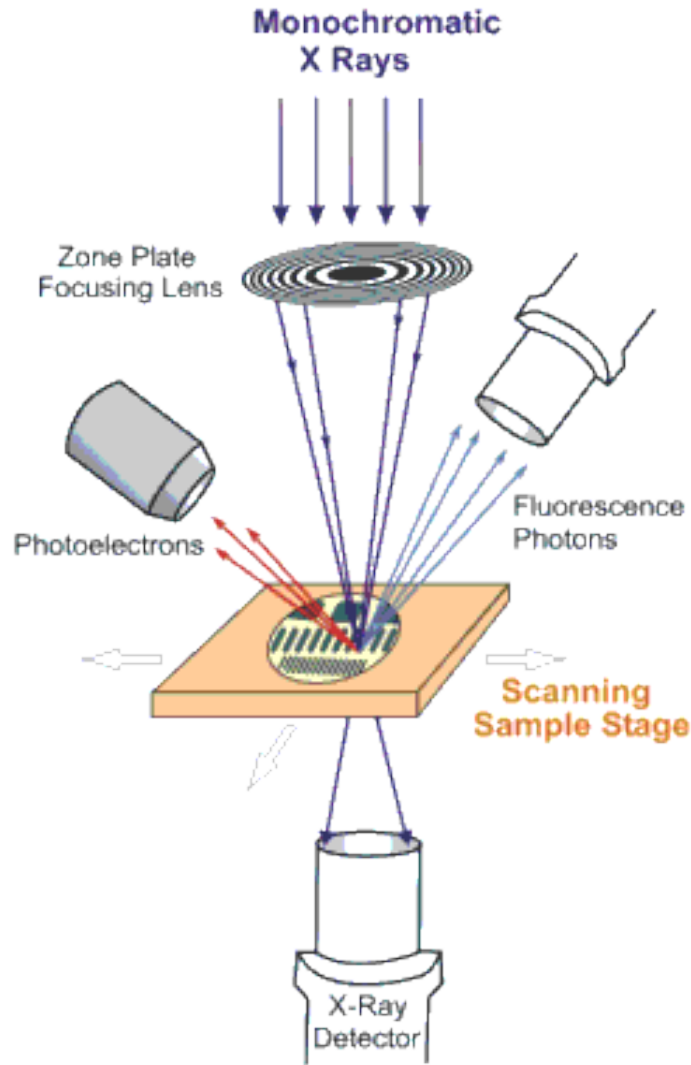
$$\frac{3.83}{\pi} = 1.22 \quad = \frac{1.22 \lambda}{2 \sin \theta_{\max}}$$

$$NA = \sin \theta_{\max}$$

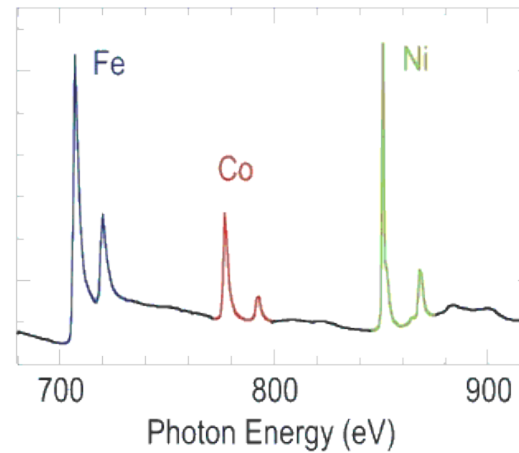
$$\Rightarrow d \leq r_{\min} = 1.22 \frac{\lambda}{2 NA}$$

Scanning transmission X-ray microscopy

Scanning Transmission X-ray Microscopy
STXM

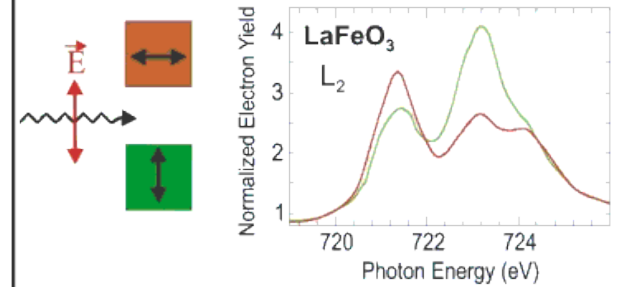


Tune x-ray **energy**
for elemental specificity

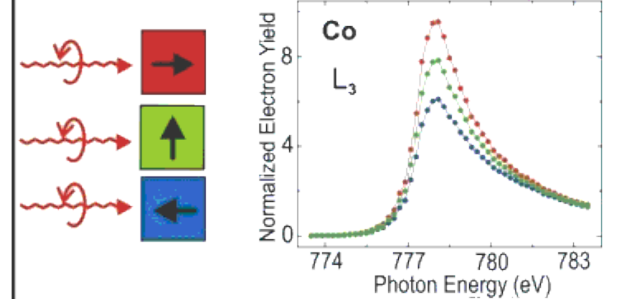


Tune x-ray **polarization**
for magnetic specificity

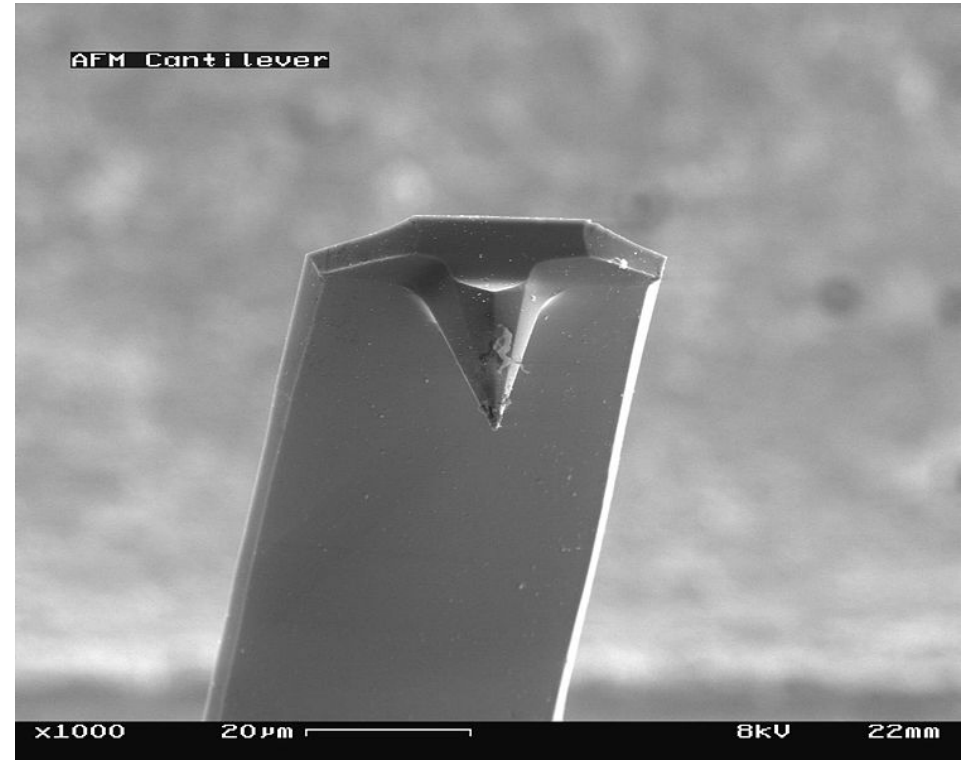
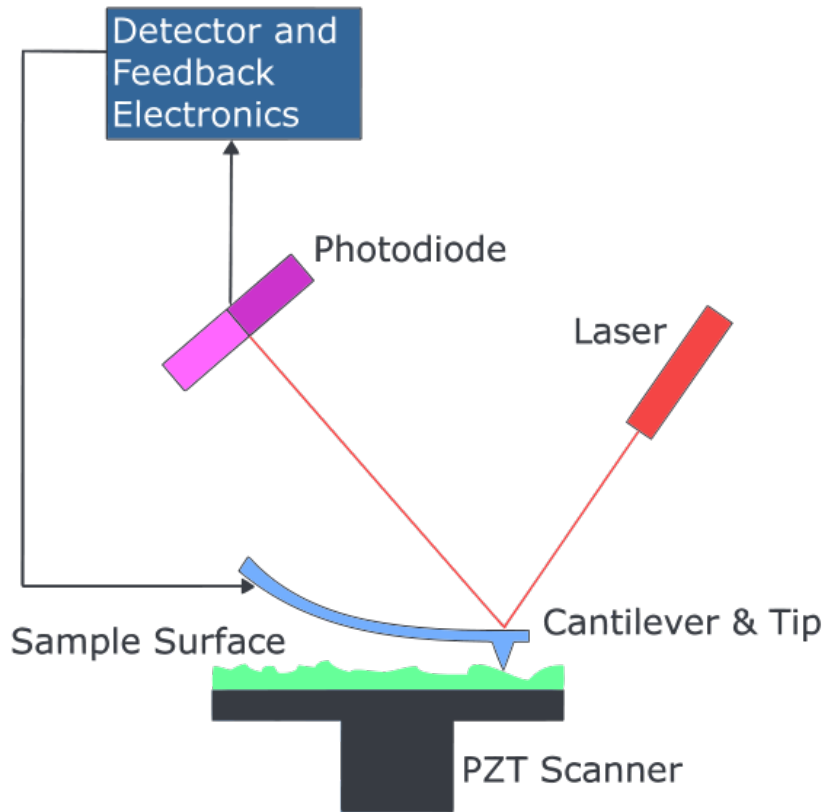
Linear Dichroism - Antiferromagnets



Circular Dichroism - Ferromagnets



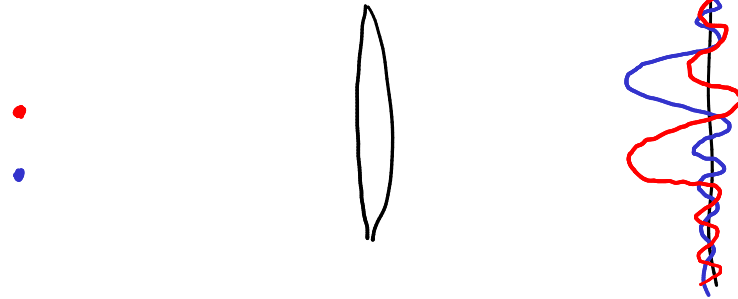
Atomic force microscopy



Resolution in scanning systems

Resolution mainly limited by probe size, interaction region

Note: coherent vs incoherent imaging



coherent vs incoherent

can interfere vs cannot interfere

scanning system = incoherent transmission

coherent: \downarrow
Image: $I = |PSF * \psi|^2$
 \uparrow
propagated wave field

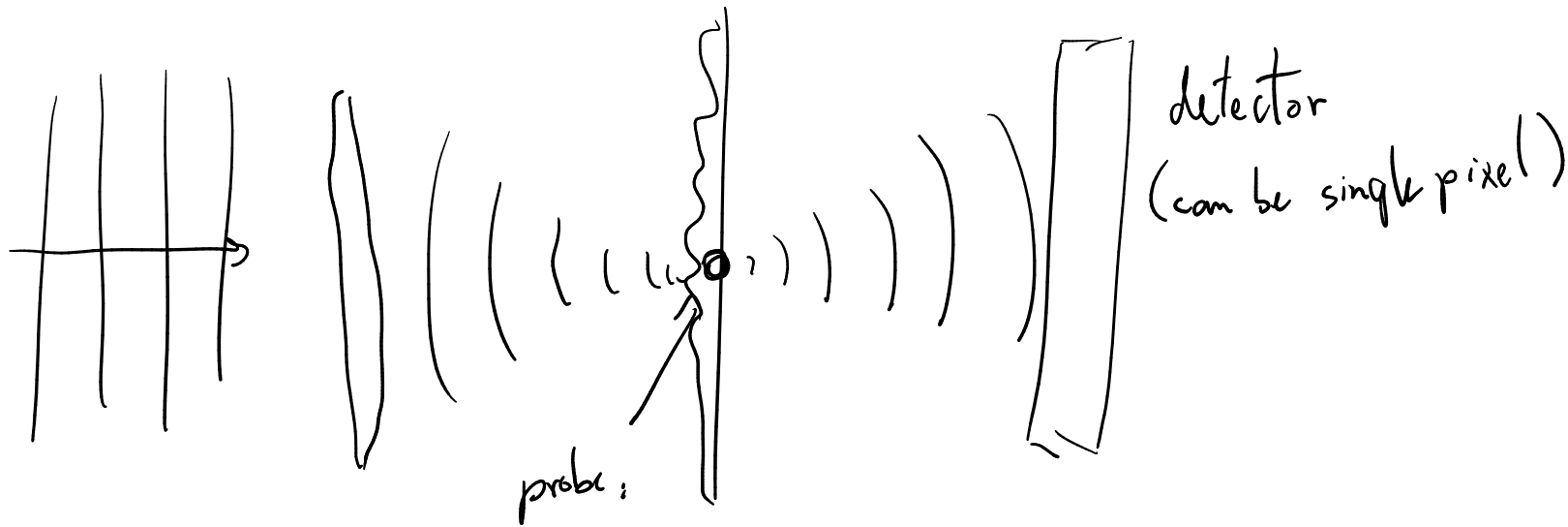
region
e.g. $\frac{J_1(x)}{x}$

incoherent:

Image: $I = |PSF|^c * |\psi|^2$

Scanning vs. full field systems

Transmission probe: the reciprocity theorem



PSF given by lens NA

\Rightarrow resolution in a scanning system : $1.22 \frac{\lambda}{2NA}$

focusing lens \nearrow

transmission system : objective lens