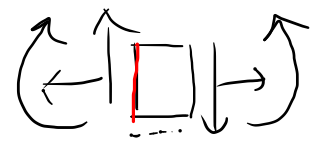
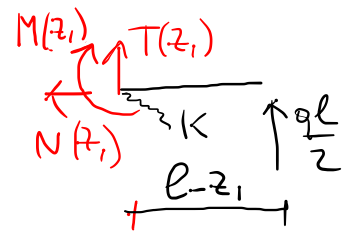
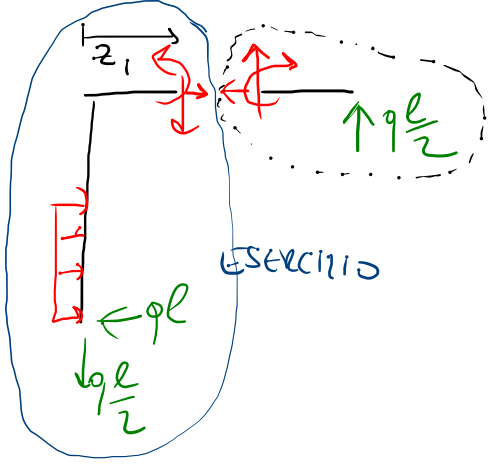
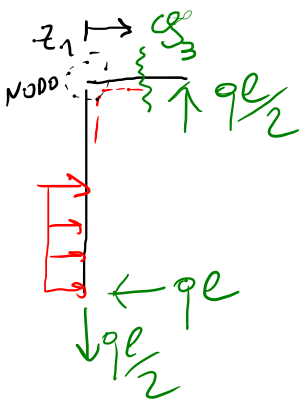


20/04/23



EQUILIBRIO

$$\rightarrow : -N(z_1) = 0$$

$$N(z_1) = 0$$

$$\uparrow : +T(z_1) + \frac{ql}{2} = 0$$

$$T(z_1) = -\frac{ql}{2}$$

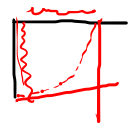
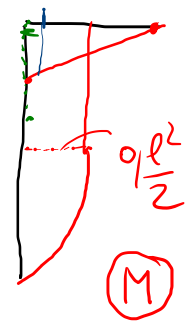
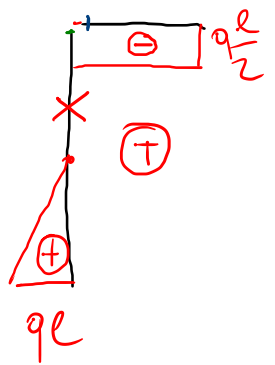
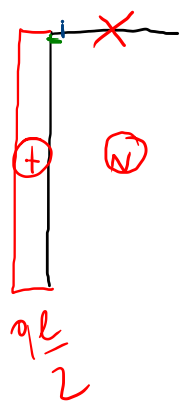
$$\leftarrow (M) : -M(z_1) + \frac{ql}{2}(l-z_1) = 0 ; M(z_1) = \frac{ql}{2}(l-z_1)$$

EQUILIBRIO DEL NODO

EQUIL. VERT: OK

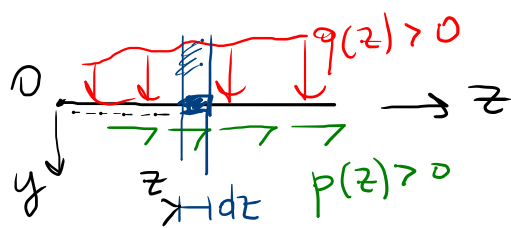
" ORIZZ: OK

EQUIL. ROTAZ: OK

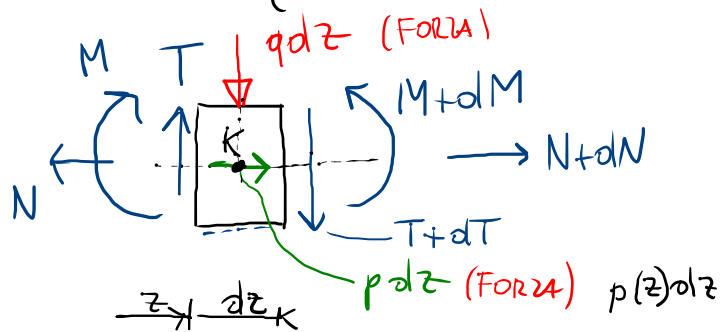


RIBALTAMENTO INTERNO PER DIAGR. (M)

EQ. DI EQUILIBRIO PUNTALE DELLE TRAVI RETTILINEE (EQ. INDEFINITE DI EQUILIBRIO)



$$[P, q] = \left[ \frac{F}{L} \right]$$



EQUILIBRIO DEL CUCIO INFINITESIMO

$$\rightarrow: -N + pdz + N + dN = 0 \Rightarrow dN = -pdz \Rightarrow$$

$$\uparrow: +T - qdz - (T + dT) = 0 \Rightarrow dT = -qdz \Rightarrow$$

$$\curvearrow: -M - T \frac{dz}{2} - (T + dT) \frac{dz}{2} + M + dM = 0 \Rightarrow -T \frac{dz}{2} - T \frac{dz}{2} - dT \frac{dz}{2} + dM = 0$$

$$-T dz - dT \frac{dz}{2} + dM = 0 \Rightarrow \frac{dM}{dz} = T$$

$\underbrace{\hspace{1.5cm}}_{\text{I ORDINE}}$ 
 $\underbrace{\hspace{1.5cm}}_{\text{II ORDINE}}$ 
 $\underbrace{\hspace{1.5cm}}_{\text{I ORDINE}}$

$$\frac{dN(z)}{dz} = -p(z)$$

$$\frac{dT(z)}{dz} = -q(z)$$

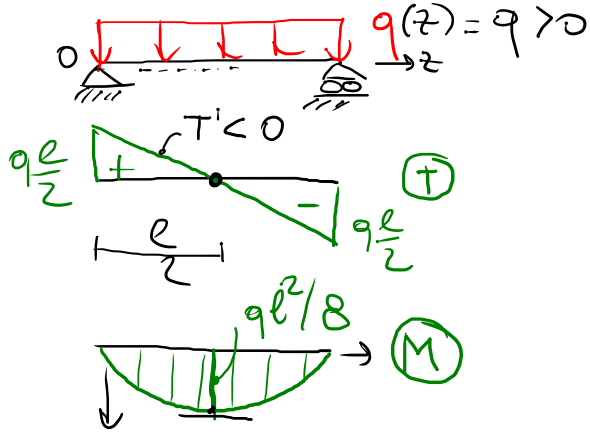
EQ. EQUIL.  
PUNTALE  
(O INDEFINITE)

SIGNIFICATO FISICO DELLE EQ. EQUIL - PUNTUALE

$$\frac{dN}{dz} = -P$$

$$\frac{dT}{dz} = -q$$

$$\frac{dM}{dz} = T$$



$$T(z) = \frac{ql}{2} - qz ; \frac{dT}{dz} = -q \quad \text{OK}$$

$$M(z) = \frac{ql}{2}z - \frac{qz^2}{2} ; \frac{dM}{dz} = \frac{ql}{2} - \frac{2qz}{2} \quad \text{OK}$$

$$= \frac{ql}{2} - qz = T(z)$$

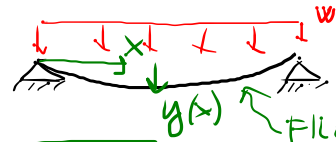
$\frac{dM}{dz} = 0 \Rightarrow$  MASSIMI / MINIMI } PUNTI STAZIONARI E TANGENTI

$$T = 0$$

$$\frac{d^2M}{dz^2} = \frac{dT}{dz} = -q$$

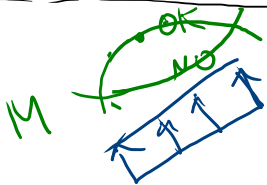
$$\frac{d^2M(z)}{dz^2} = -q(z)$$

ANALOGIA

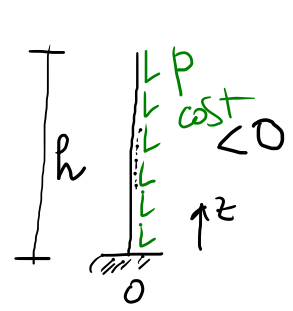


$$\frac{d^2y}{dx^2} = -w$$

FILLO TESO SENZA PESO



ESERCIZIO DI INTEGRAZ. DELL'EQ  $\frac{dN}{dz} = -p$

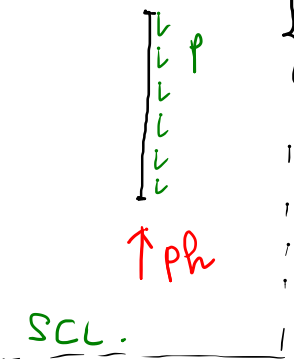


? CALCOLORE  $N(z)$  INTEGRANDO  $\frac{dN}{dz} = -p$

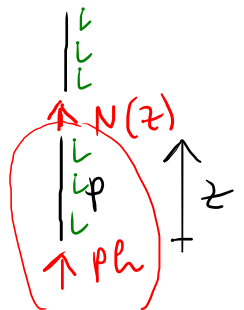
$(p < 0)$

$$\begin{cases} \frac{dN}{dz} = p \\ N(0) = -ph \end{cases} \Rightarrow N(z) = pz + C \Rightarrow \boxed{N(z) = pz - ph}$$

$\checkmark C = -ph$

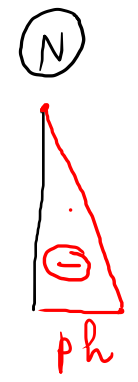


DET. DI  $N(z)$  CON IL METODO DELLA SEZIONE



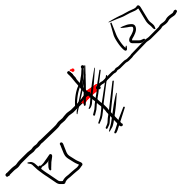
$$+\uparrow: +ph - pz + N(z) = 0$$

$$N(z) = pz - ph$$

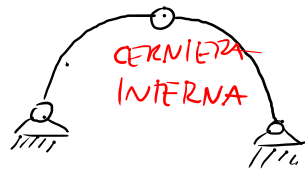


# VINCOLI INTERNI

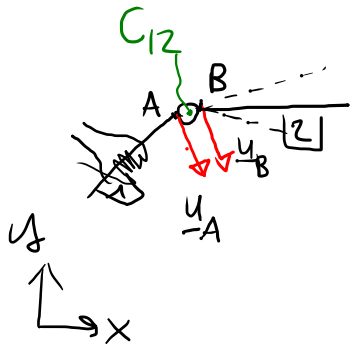
$\nu=3$ : INCASTRO INTERNO



VINCOLO CHE  
ANNULLA TUTTI  
I G.D.L. RELATIVI  
DEL CORPO [2] RISPETTO A [1]



$\nu=2$ : CERNIERA INTERNA



$$\frac{u_A}{-A} = \frac{u_B}{-B} \quad \text{EQ. DI VINCOLO}$$

$$\begin{cases} u_{Ax} = u_{Bx} \\ u_{Ay} = u_{By} \end{cases}$$

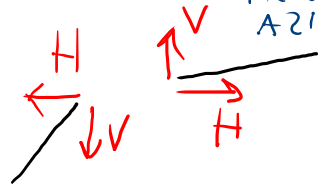
ROTAZIONI RELATIVE

~~LIBERE.~~

CINEMATICA

IL PUNTO CERNIERA È SEDE DI UN  
C.I.R. RELATIVO TRA I CORPI [1] e [2]:  $C_{12}$

OPPOSITE PER IL  
PRINCIPIO DI  
AZIONE-REAZ.



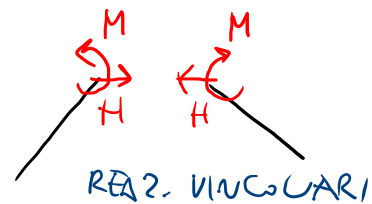
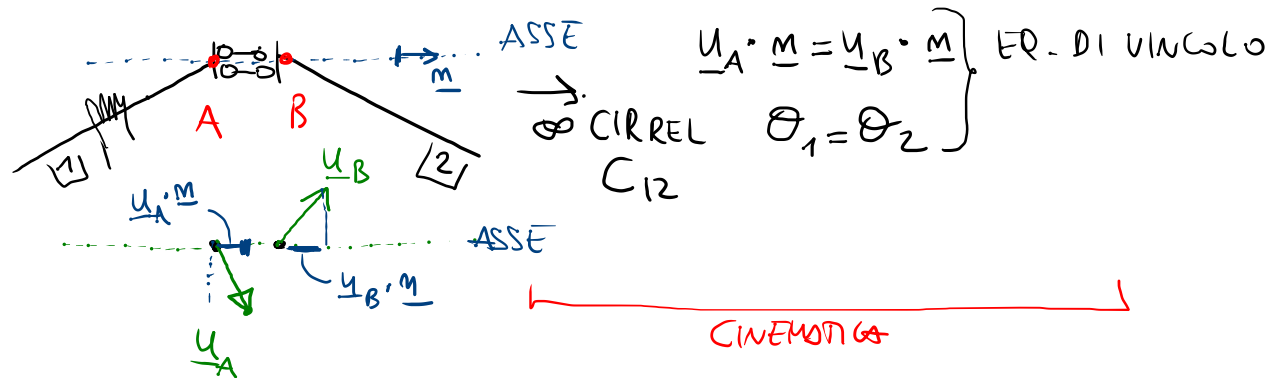
REAZ. VINCOLI

INTERNE: 2 INCOSNITE

STATICA

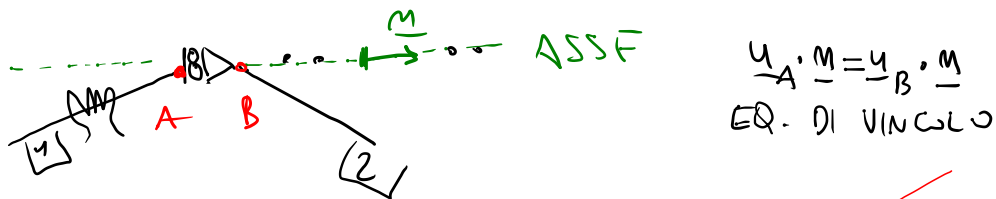
$V, H$

$\nu=2$ : DOPPIO PENDOLO INTERNO (PASTINO INTERNO)



STADICA

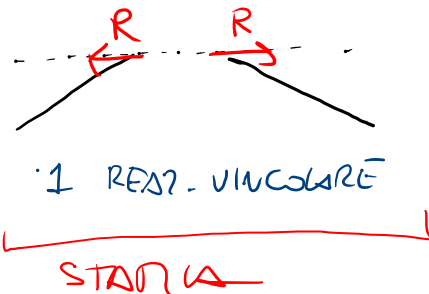
$\nu=1$ : CARRELLA (BIELLA, PENDOLO) INTERNO



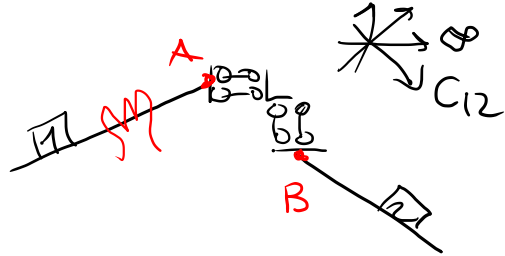
(NOTA: ROT. RESTRIE LIBERE:  $\theta_1 \neq \theta_2$ )

CINEMATICA

$C_{12}$ : UN PUNTO DELL'ASSE



$v=1$  : DOPPIO-DOPPIO PENDOLO INTERNO

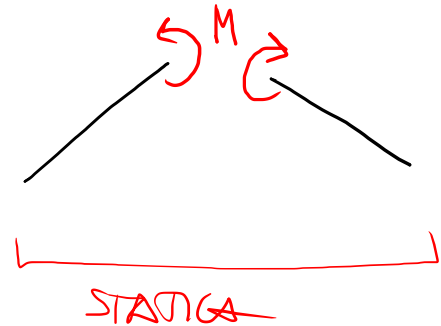


$\theta_1 = \theta_2$  EQ. DI VINCOLO

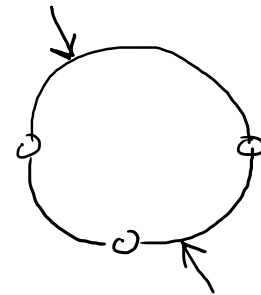
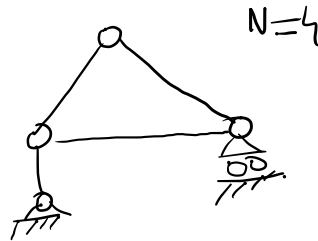
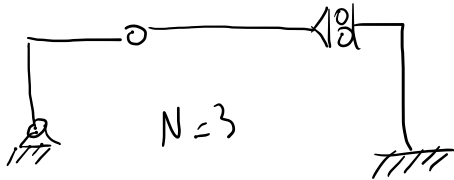
$C_{12}$  E RETTA IMPROPRIA

(NOTA: IL CORPO [2] PUÒ TRASLARE LIBERAMENTE RISPETTO A [1])

CINEMATICA



OSSERVAZ. CON I VINCOLI INTERNI POSSO COSTRUIRE STRUTTURE FORMATE DA N CORPI RIGIDI



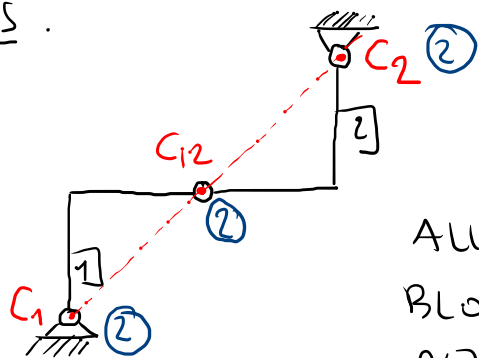
$N=3$ , SOLO VINCOLI INTERNI  
CARICHI EQUILIBRATI

Lo studio della cinematica di 2 C.R. mutuamente vincolati coinvolge 3 CENTRI IST. DI ROTAZIONE (3 C.I.R.):  $C_1, C_2, C_{12}$

PROPRIETA': CONDIZ. NECESSARIA affinché avvenga un moto relativo tra 2 C.R. è che i C.I.R.  $C_1$  e  $C_2$  siano allineati con  $C_{12}$ .

$$\underline{C_1 \leftrightarrow C_{12} \leftrightarrow C_2}$$

ES.



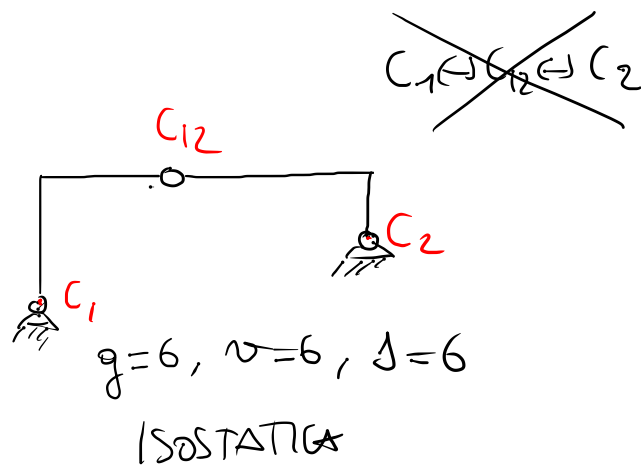
$$g = 2 \cdot 3 = 6$$

$$v = 6$$

L'ALLINEAM. DEI CENTRI NON PERMETTE ALLE 3 CERNIERE DI BLOCCARE TUTTI I GOL DEL SISTEMA

$$\Rightarrow \Delta = 5$$

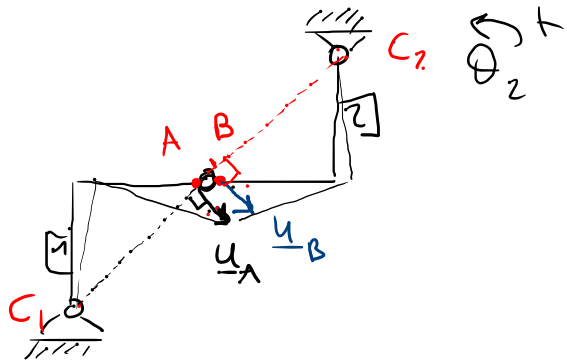
VINCOLI INEFFICACI



$$g = 6, v = 6, \Delta = 6$$

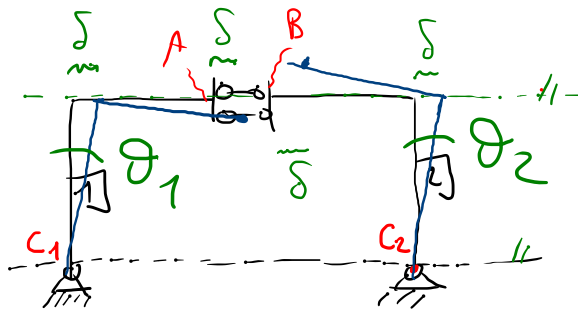
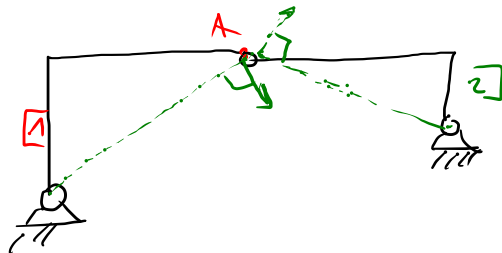
ISOSTATICA





$$\theta_1 \curvearrowright$$

L'ALLINEAM. DELLE 3  
CERNIERE GARANTISCE  
CHE I PUNTI A e B SI  
POSSONO SPOSTARE  
COMPATIBILMENTE CON  
I VINCOLI DEL SISTEMA



$$C_{12}$$

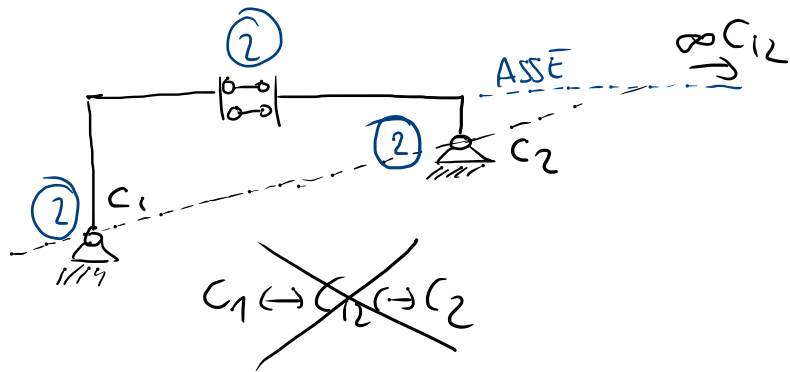
$$C_1 \Leftrightarrow C_{12} \Leftrightarrow C_2$$

$$\theta_1 = \theta_2$$

$$l_1 \quad l_2$$

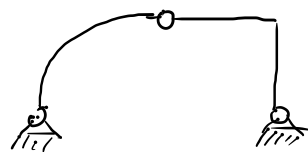
CINEMATISMO  
(STR. LIBILE)

$$g=6, v=6, \Delta=5$$



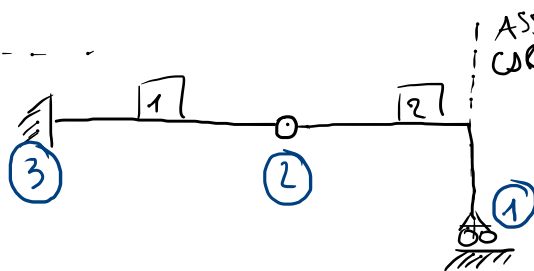
STR ISOSTATICA.

ESEMPI DI STR ISOSTATICHE

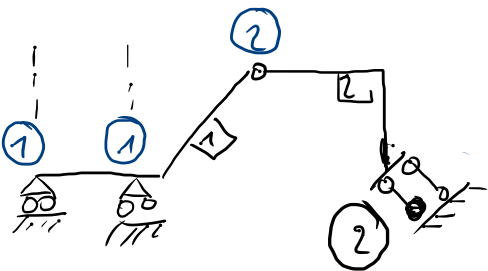


ARCO A 3 CERNIERE

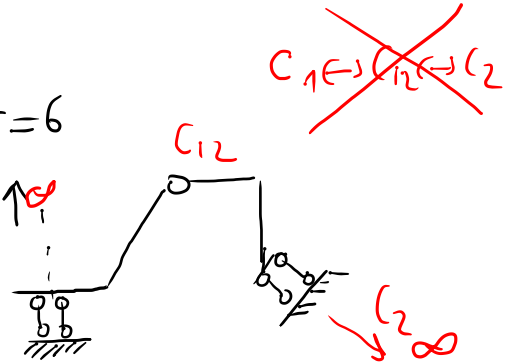
(CERNIERE NON ALLINEATE)



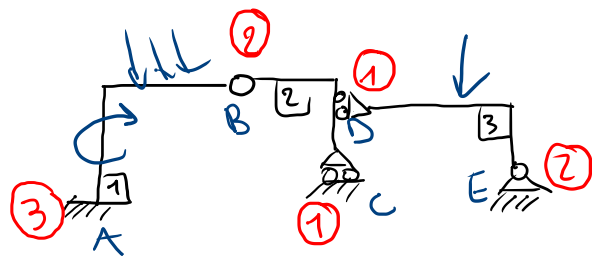
$g=6, v=6$   
 $\Delta=6$



$g=6, v=6$   
 $\Delta=6$

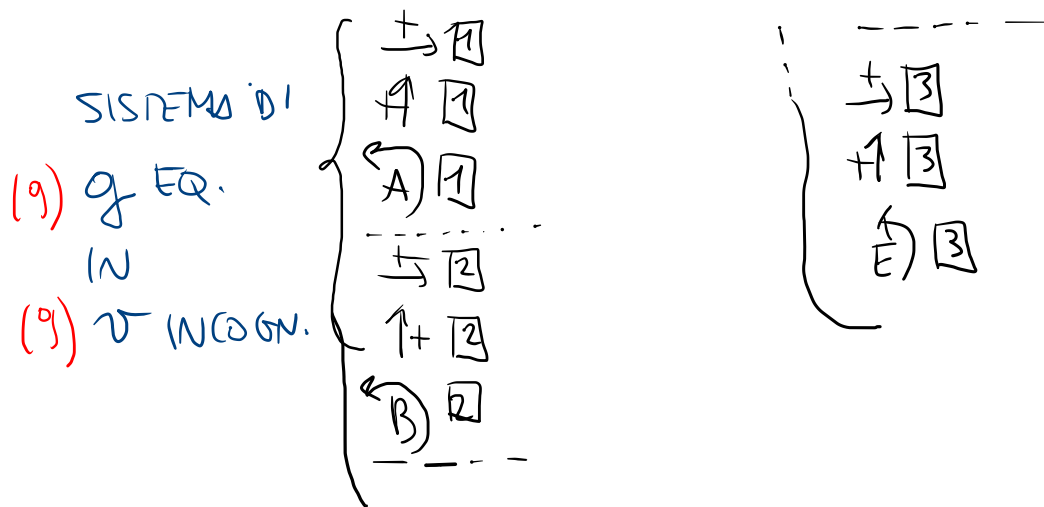
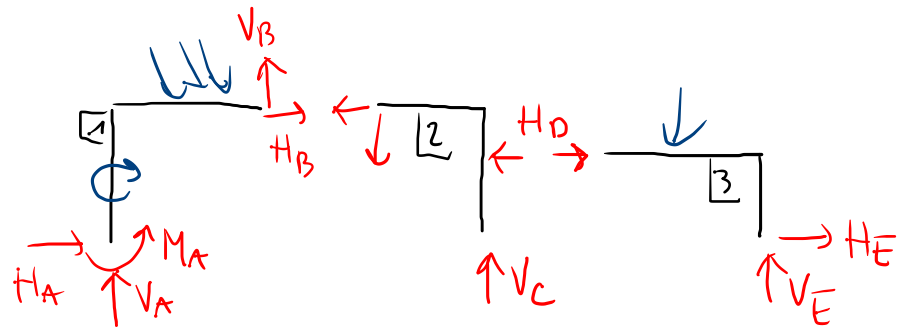


# METODO GENERALE DI ANALISI STATICA DELLE STR. ARTICOLATE

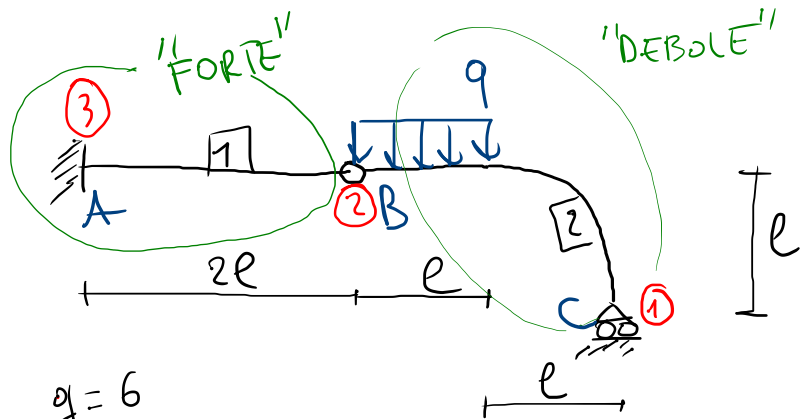


$g=9, v=9, \Delta=9$  (ISOST.)

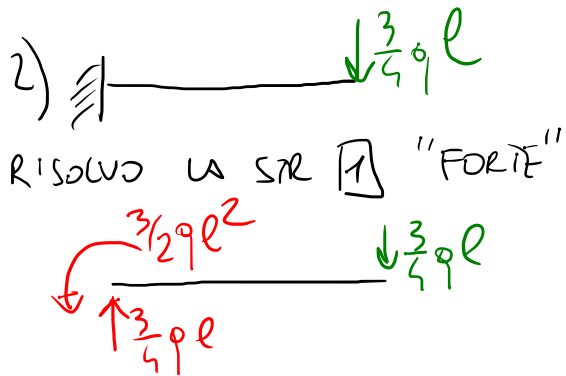
QUANTE INCOGNITE STATICHE  
CI SONO? 9!



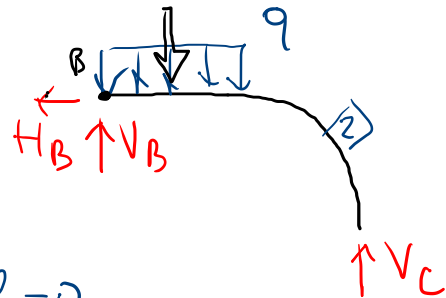
# ES: STUDIO DI UNA STR ISOSTATICA "A STRUTTURA GERARCHICA"



$g = 6$   
 $v = 6$   
 $d = 6$   
 ISOST.



1) RISOLVO PRIMA LA STR 2, INFATTI NOTO CHE LE INCOGNITE CHE INSISTONO SU 2 SONO SOLO 3.



$$\sum \rightarrow: -H_B = 0$$

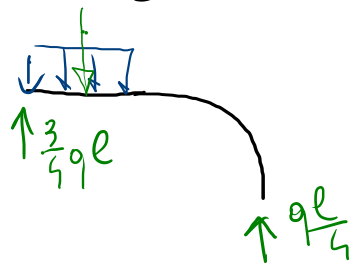
$$\sum \uparrow: V_B + V_C - ql = 0$$

$$\sum \leftarrow \text{B): } -ql \frac{l}{2} + V_C 2l = 0$$

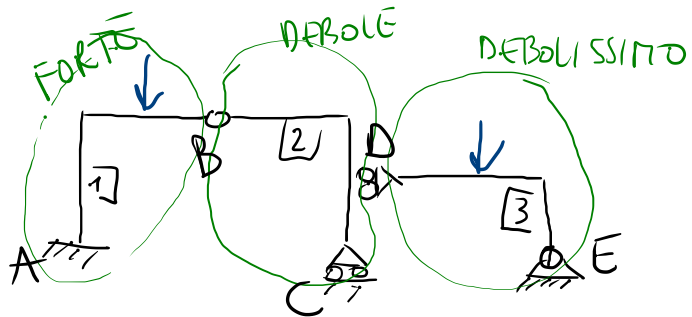
$$V_C = +ql \frac{1}{4}$$

$$V_B = \frac{3}{4} ql$$

$$H_B = 0$$

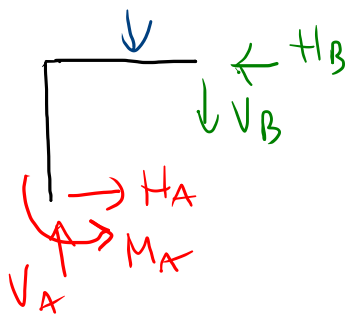


ES: STRUT. CON 2 ORDINI DI GERARCHIA



3) RISOLVO [1]

3 EQ. IN 3 INCOGNITE



1) RISOLVO [3] (3 EQ. IN 3 INCOGNITE)

e applico la net. opposta in D e



2)

RISOLVO [2] (3 EQ. IN 3 INCOGNITE)

e applico le net. opposte in B e [1]

