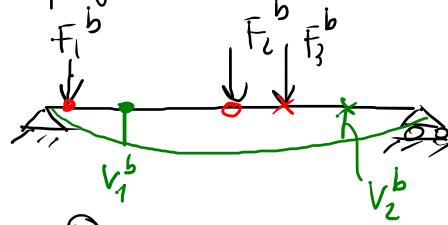
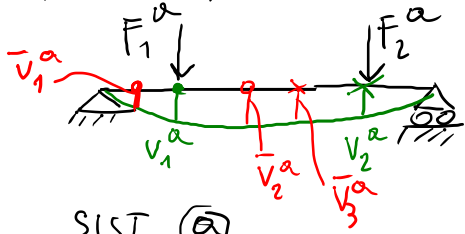


TEOREMA DI BETH (o DI RECIPROCA') 1872

MDS, 21/11/23

Ipotesi: quelle del th di Clepeyron.



$$F_1^a v_1^b + F_2^a v_2^b = F_1^b v_1^a + F_2^b v_2^a + F_3^b v_3^a$$

LAVORO MUTUO
DELE FORZE (a) x
GLI SPOST. CORRISP.
DEI SIST. (b)

... (b) x GLI SPOST.
... SIST. (a)

$$L_{ab} = L_{ba}$$

(a) $\varphi_a = \frac{F l^2}{2EI}$

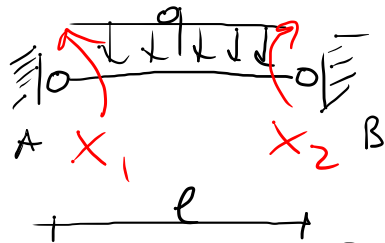
(b) $I \eta^b = \frac{M l^2}{2EI}$

$$F \eta^b = M \varphi^a$$

$$\frac{F M l^2}{2EI} = M \frac{F l^2}{2EI}$$

OK

LES: RIS. STR IPERST (METODO FORZE)



$$\varphi_A = 0 \quad \varphi_B = 0$$

$$\begin{cases} +\frac{ql^3}{24EI} - \frac{x_1 l}{3EI} - \frac{x_2 l}{6EI} = 0 \\ -\frac{ql^3}{24EI} + \frac{x_2 l}{3EI} + \frac{x_1 l}{6EI} = 0 \end{cases}$$

$$\begin{cases} \frac{x_1 l}{3EI} + \frac{x_2 l}{6EI} = \frac{ql^3}{24EI} \\ \frac{x_1 l}{6EI} + \frac{x_2 l}{3EI} = \frac{ql^3}{24EI} \end{cases}$$

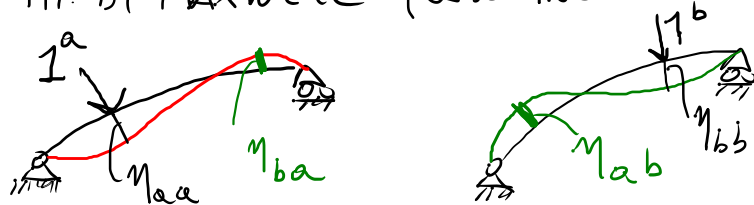
$\eta_{12} = \eta_{21}$ per il Teorema di Betti

η_{ij} : COEFF DI INFLUENZA.

$$[H] \begin{bmatrix} x_1 \\ x_2 \end{bmatrix} = \begin{bmatrix} N \\ 0 \\ + \\ 1 \end{bmatrix}$$

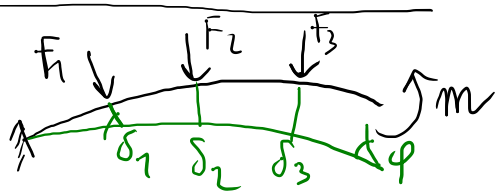
MATRICE DI CEDevolezza (η_{ij})

TH. DI MAXWELL (CASO PARTICOLARE DEL TH. DI BETTI)



$$-1^a \eta_{ab} = -1^b \eta_{ba} \implies \eta_{ab} = \eta_{ba}$$

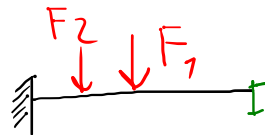
TM. DI CASTIGLIANO



$$N = N(F_1, F_2, F_3, m)$$

$$M = M(\quad)$$

DIPENDENZE
LINEARI



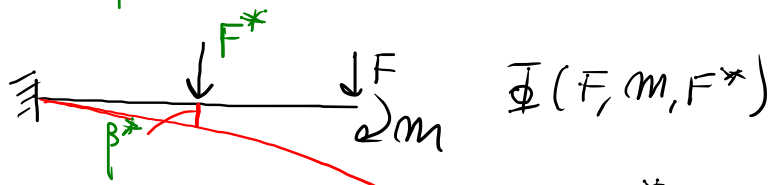
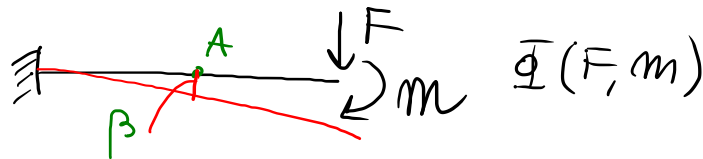
IPOTESI: QUELLE DI CAUPEYRON (NON SI POSSONO
CONSIDERARE
CARICHI CONCENTRATI (VALORI TERMICHE))

$$\bar{\Phi} = \frac{1}{2} \int_{s_1}^{s_2} \frac{N^2}{EA} + \frac{M^2}{EI} = \bar{\Phi}(F_1, F_2, \dots, m)$$

$$\frac{\partial \bar{\Phi}}{\partial F_i} = \delta_i \quad ; \quad \text{SPOST. CORRETTA
ALLA FORZA } F_i$$

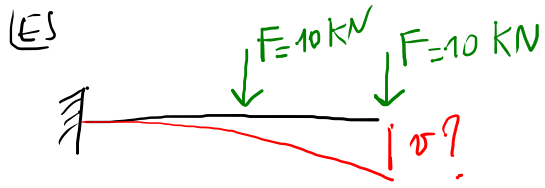
$$\frac{\partial \bar{\Phi}}{\partial m} = \varphi \quad ; \quad \text{ROTAZ. CORRETTA
A } m$$

CALCOLO DI SPST. DI PUNTI
SENZA FORZA CORRETTA



$$\beta^* = \frac{\partial \Phi(F, m, F^*)}{\partial F^*} \quad ; \quad \beta = \lim_{F^* \rightarrow 0} \beta^*$$

$$\beta^* = \beta^*(F, m, F^*)$$

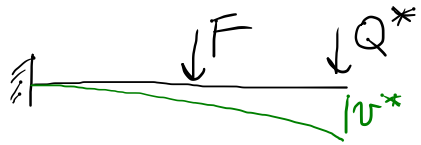


$$M = M(F) \quad ; \quad \Phi = \Phi(F)$$

$$\frac{\partial \Phi}{\partial F}$$

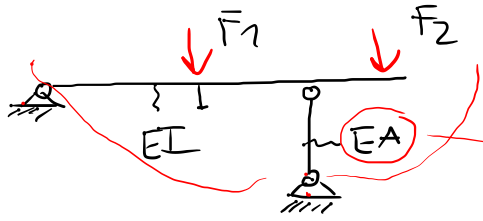
$$\frac{1}{2} k x^2 = \frac{1}{2} k \frac{F^2}{k^2}$$

$$\boxed{x = \frac{F}{k}} \quad \boxed{-\frac{1}{2} \frac{F^2}{k}}$$



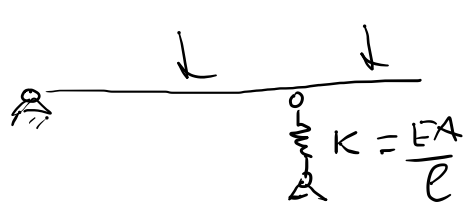
$$M(F, Q^*) \quad ; \quad \dots \quad ; \quad v^* = \frac{\partial \Phi}{\partial Q^*}$$

$$\lim_{Q^* \rightarrow F} v^* = v$$



$$\Phi = \Phi(EI) + \Phi(EA)$$

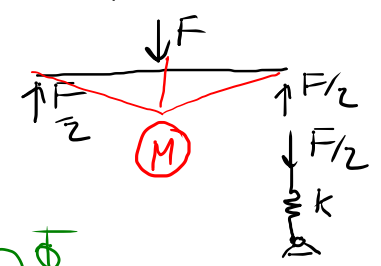
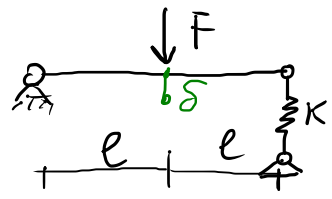
TUTTI GLI ELEMENTI ESISTENTI NELLA STRUTTURA DEVONO ENTRARE NELLA FORMULA DI Φ .



$$\Phi = \Phi(EI) + \Phi(K)$$

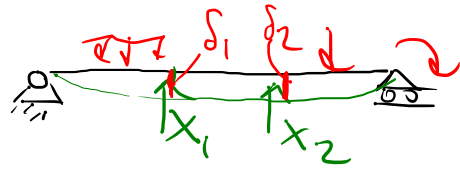
$$M(F)$$

$$\Phi = \frac{1}{2} \int \frac{M^2}{EI} dx + \frac{1}{2} \left(\frac{F}{2}\right)^2 \frac{1}{K}$$



$$\delta = \frac{\partial \Phi}{\partial F}$$

TH DI MEMBREA



$$\begin{cases} \delta_1 = 0 \\ \delta_2 = 0 \end{cases} \text{ EQ DI CONCORDANZA}$$

$$\Rightarrow \left. \begin{aligned} \frac{\partial \Phi}{\partial x_1} &= 0 \\ \frac{\partial \Phi}{\partial x_2} &= 0 \end{aligned} \right\}$$

STAZIONARITA' DI Φ

"LEAST ACTION"
(TH. DEL MINIMO LAVORO)

VINCOLI FISSI

STR IPERST. (2 V. IPERST.)

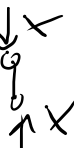
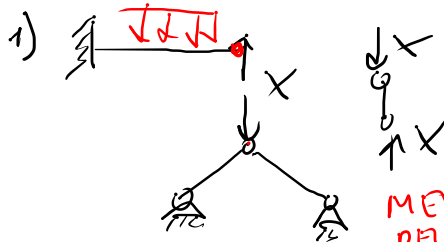
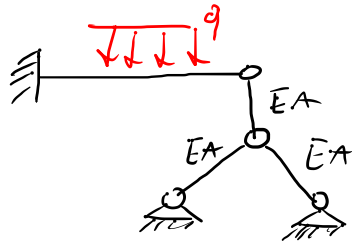
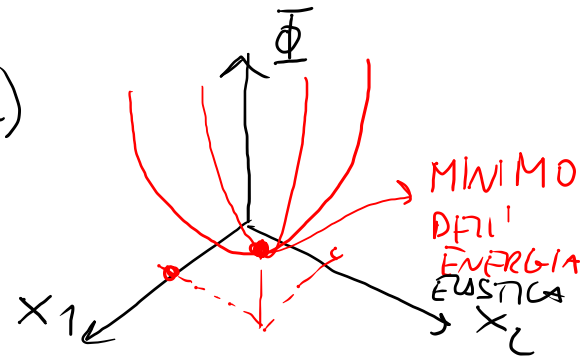
STR PRINCIPALE

$$\Phi(q, F, M; x_1, x_2)$$

$$\delta_i = \frac{\partial \Phi}{\partial x_i}$$

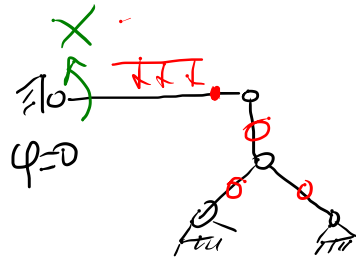
PER CASTIGLIANO

ENERGIA ELASTICA
=
LAVORO DI DEFORMAZIONE



METODO DELLE FORTE

2)



$$\Phi(EI, EA)$$

$$\varphi = \frac{\partial \Phi}{\partial X} = 0$$

T. DI MEMBREA