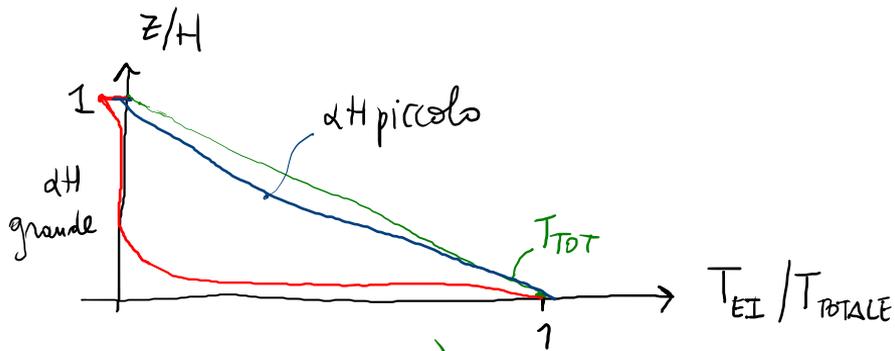
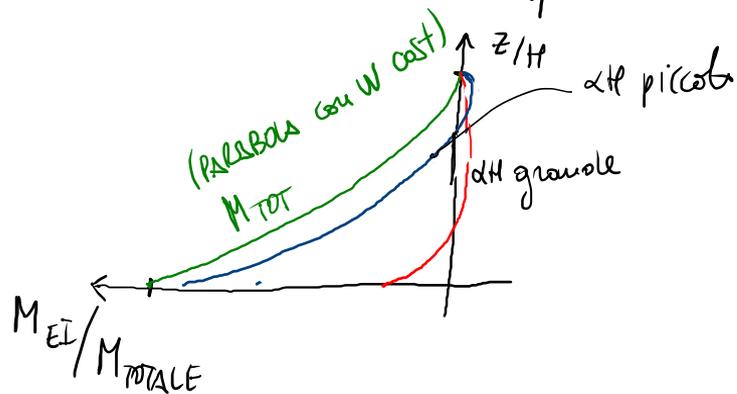


GRAFICI M, T (PROBL TEMIO + MENSOLA "EI")

9/05/24



dH "grande" (> 10): MENSOLA EI "soffice"
 "piccolo" (< 1): " " "Rigida"



MENSOLA "EI"

• osservo che: $M_{EI} + M_{GA} = -\frac{w(H-z)^2}{2}$; $T_{EI} + T_{GA} = w(H-z)$

• alcune soluz in forme chiuse:

$$M_{EI}(z) = -w \left[\frac{H}{\alpha} (\tanh \alpha H \cosh \alpha z - \sinh \alpha z) + \frac{1}{\alpha^2} \left(\frac{\cosh \alpha z}{\cosh \alpha H} - 1 \right) \right]$$

$$T_{EI}(z) = w \left[H (\cosh \alpha z - \tanh \alpha H \sinh \alpha z) - \frac{1}{\alpha} \left(\frac{\sinh \alpha z}{\cosh \alpha H} \right) \right]$$

$$y(z) = \frac{wH^4}{EI} \left[\frac{1}{(\alpha H)^4} \left[\frac{\alpha H \sinh \alpha H + 1}{\cosh \alpha H} (\cosh \alpha z - 1) - \alpha H \sinh \alpha z + (\alpha H)^2 \left[\frac{z}{H} - \frac{1}{2} \left(\frac{z}{H} \right)^2 \right] \right] \right]$$

HIGH-RISE BUILDINGS

POZZATI - vol 2-2 "TEORIA E TECNICA DELLE STRUTTURE", UTET

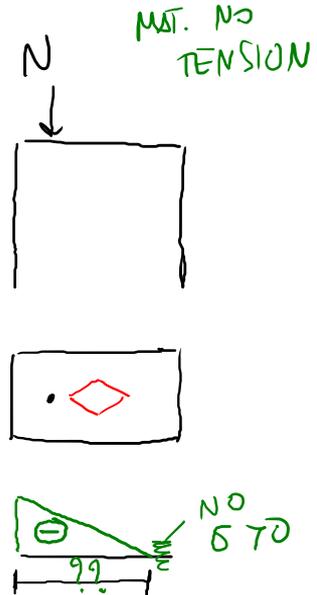
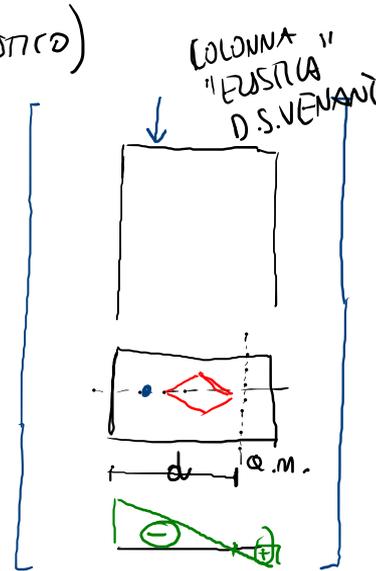
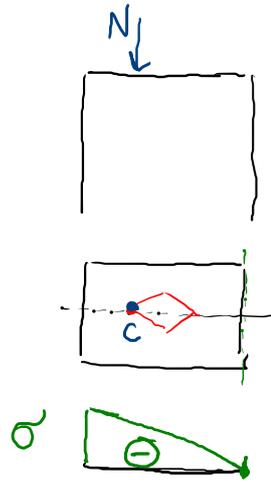
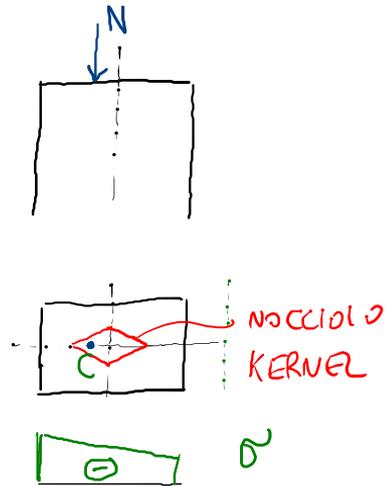
MECCANICA DELLE STRUTTURE MURARIE

$$\int_A \sigma dA = N$$

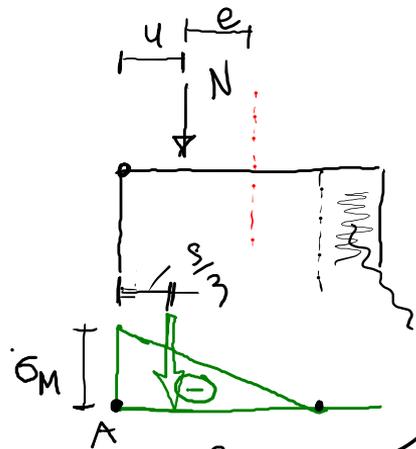
IPOTESI DI HEYMAN PER LA MODELLO? DELLE MURATURE

- 1) LA MURATURA NON HA RESIST. A TRAZIONE.
- 2) " " HA UNA INFINITA RESIST. A COMPRESSIONE.
- 3) LA CRISI PER SCORRIMENTO A TAGLIO DEI BLOCCHI NON PUO' AVVENIRE.

PILASTRO COMPRESSO IN MATERIALE "NO-TENSION" (ELASTICO)



TENSIONI DI COMPRESSIONE IN UN MOT. NO-TENSION IN UN PILASTRO CARICATO CON "GRANDE" ECCENTRICITA'.

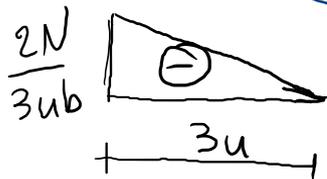


POSSIBILI FESSURAZIONI



SEZ. TRASV.

SEZ. RESISTENTE



σ_M ?
 s ?

$$\left\{ \begin{array}{l} \sigma_M s b \frac{1}{2} = N \quad (\text{EQUIVALENZA TRASV.}) \\ N u = \sigma_M s b \frac{1}{2} \frac{s}{3} \quad (\text{EQUIVALENZA MOM RISP. AD A}) \end{array} \right.$$

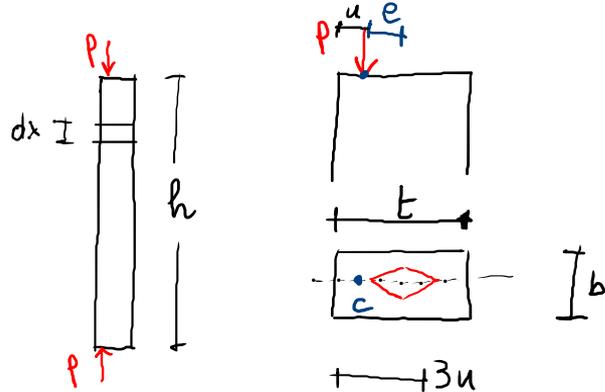
$$\rightarrow \boxed{u = \frac{s}{3}} \quad ; \quad \sigma_M 3u b \frac{1}{2} = N \Rightarrow \boxed{\sigma_M = \frac{2N}{3ub}}$$

NOTA: AMMETTO CHE $\max |\sigma_M| = f_K$

QUANTO VALE u_{\min} ?

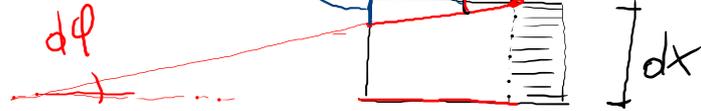
$$f_K = \frac{2N}{3u_{\min} b} \Rightarrow u_{\min} = \frac{2N}{3b f_K}$$

INSTABILITA' DI UN PIASTRO "NO-TENSION" CARICATO A GRANDE ECCENTRICITA'



$$\frac{2}{3} \frac{P}{bu} = \sigma_0$$

$$\epsilon_0 dx = \frac{\sigma_0}{E} dx$$



$$\frac{d\phi}{dx} ?$$

$$d\phi = \frac{\epsilon_0 dx}{3u} = \frac{\sigma_0}{E} dx \frac{1}{3u} = \frac{2}{9} \frac{P}{Ebu^2} dx$$

CURVATURA INDOTTA

$$\frac{d\phi}{dx} = \frac{2}{9} \frac{P}{Ebu^2} \Rightarrow (u(x))$$

SEGUONO
SLIDE E
DIAGRAMMI
DEL
PROBLEMA
DI YOKEL