

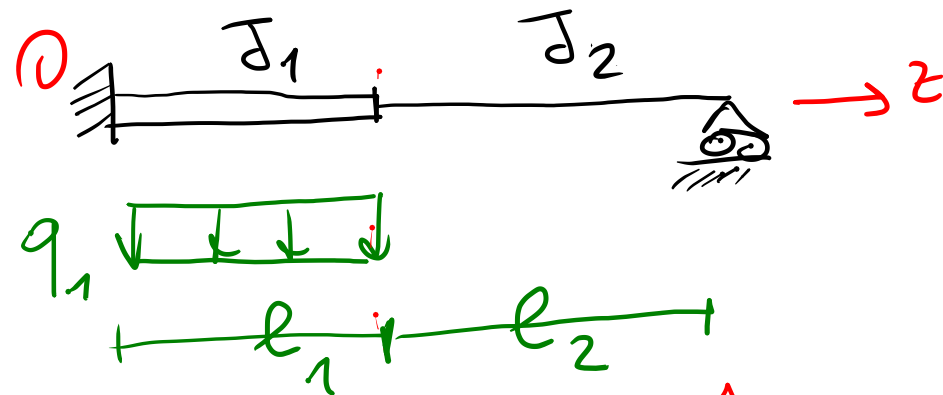
LINEA EL. IV ORDINE: CONDIZIONI DI RACCORDO PER PIU' CAMPI DI
INTEGRAZIONE

2/10/24

2 CAMPI DI INTEGRAZIONE

① $z \in [0, l_1]$

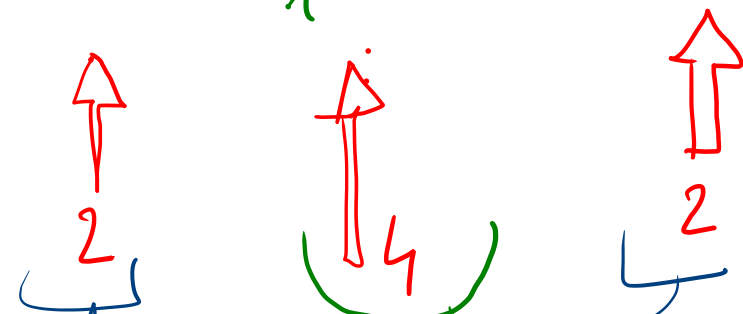
② $z \in]l_1, l_1 + l_2]$



① $EJ_1 v_1'''' = q_1 \leadsto C_1, C_2, C_3, C_4$

② $EJ_2 v_2'''' = 0 \leadsto C_5, C_6, C_7, C_8$

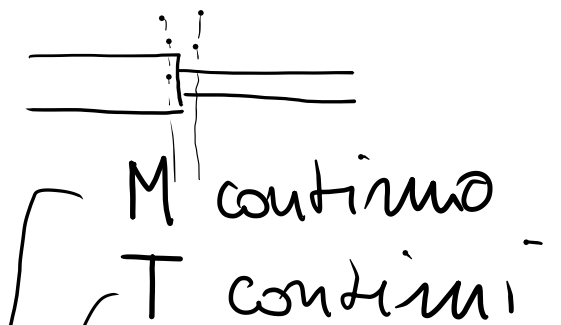
8 COSTANTI INCOGNITE



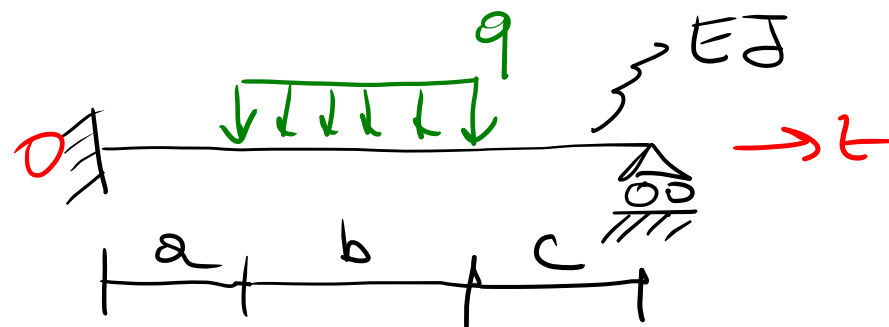
: CONDIZ. DA IMPORRE

$$\begin{cases} v_1(0) = 0 \\ v_1'(0) = 0 \\ v_2(l_1 + l_2) = 0 \\ v_2''(l_1 + l_2) = 0 \end{cases}$$

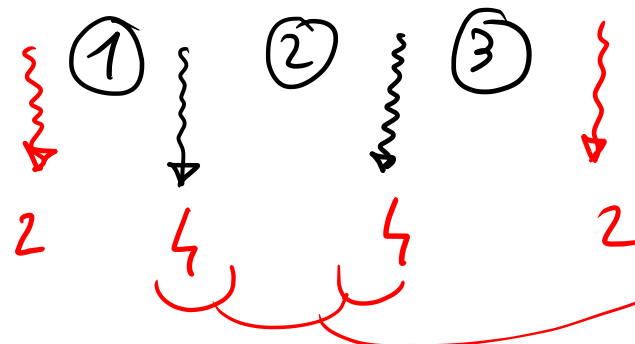
$$\begin{cases} v_1(l_1) = v_2(l_1) \\ v_1'(l_1) = v_2'(l_1) \\ EJ_1 v_1''(l_1) = -EJ_2 v_2''(l_1) \\ EJ_1 v_1'''(l_1) = -EJ_2 v_2'''(l_1) \end{cases}$$



ALTRI CASI: ①



CAMPI



$$z_1 \in [0, a]$$

$$EJ v_1^{IV}(z) = 0$$

$$z_2 \in [a, a+b]$$

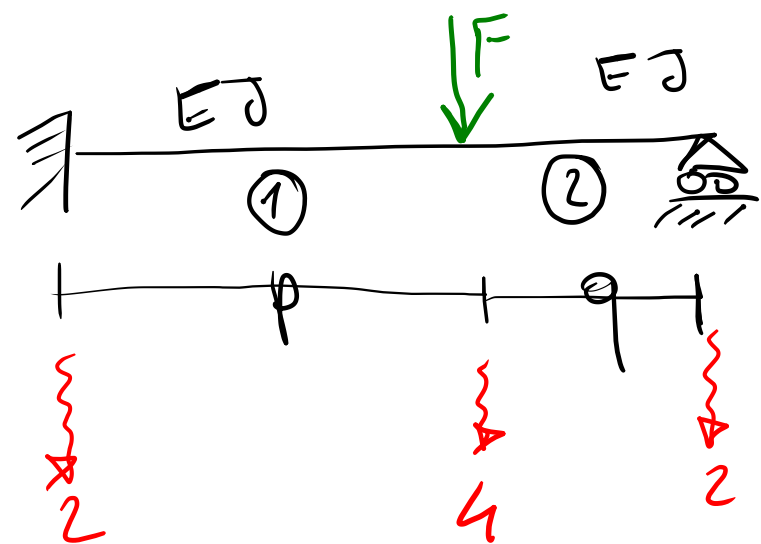
$$EJ v_2^{IV}(z) = q$$

$$z_3 \in [a+b, a+b+c]$$

$$EJ v_3^{IV}(z) = 0$$

CONTINUITÀ DI v, v', M, T

②



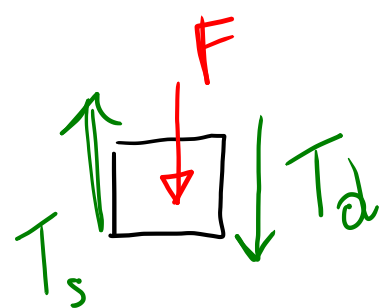
$$z_1 \in [0, p]$$

$$EJ v_1^{IV}(z) = 0$$

$$z_2 \in [p, p+q]$$

$$EJ v_2^{IV}(z) = 0$$

$$T = -EJ v'''$$



$$T_d + F - T_s = 0$$

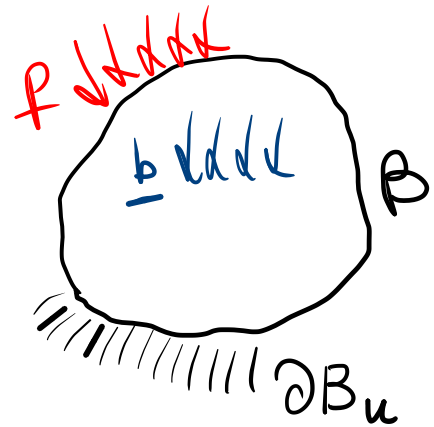
$$-EJ v_2'''(p) + F = -EJ v_1'''(p)$$

$$\begin{cases} v_1(p) = v_2(p) \\ v_1'(p) = v_2'(p) \\ v_2''(p) = v_2''(p) \\ v_1'''(p) - v_2'''(p) = -\frac{F}{EJ} \end{cases}$$

PRINCIPIO DI STAZIONARIETA' DELL' EN. POTENZIALE TOTALE

NELLA MECCANICA DEI SIST. DISCRETI QUESTO PRINCIPIO PERMETTE DI STUDIARE LE CONFIG. DI EQUILIBRIO

$$\underline{\underline{\varepsilon}} = \frac{1}{2} (\nabla \underline{u} + \nabla \underline{u}^T) ; \quad \underline{\underline{\sigma}} = \mathbb{C} \underline{\underline{\varepsilon}}$$



VINCOLI DI
NATURA CINEMATICA

$\underline{u}(\underline{x})$: CAMPO DI SPOST.
NELLA CONFIG. EQUILIBRATA
 $\underline{x} \in B$

$$\Pi(\underline{u}) = \underbrace{\frac{1}{2} \int_B \underline{\underline{\sigma}} \cdot \underline{\underline{\varepsilon}} dV}_{\Phi : \text{EN ELASTICA}} - \underbrace{\left\{ \int_B \underline{b} \cdot \underline{u} dV + \int_{\partial B} \underline{p} \cdot \underline{u} dA \right\}}_{\text{POTENZ. - CARICHI}}$$

E.P.T.

APPLICHO UNA "VARIAZIONE" $\delta \underline{u}$ (ANALOGO ALLO SPOST. VIRTUALE)

$$\Pi(\underline{u}) \rightarrow \Pi(\underline{u} + \delta \underline{u})$$

$$\Pi(\underline{u} + \delta \underline{u}) = \frac{1}{2} \int_B \mathcal{C}(\underline{\varepsilon} + \delta \underline{\varepsilon}) \cdot (\underline{\varepsilon} + \delta \underline{\varepsilon}) dV - \int_B \underline{b} \cdot (\underline{u} + \delta \underline{u}) dV - \int_{\partial B} p \cdot (\underline{u} + \delta \underline{u}) dA$$

$$= \frac{1}{2} \int_B \mathcal{C} \underline{\varepsilon} \cdot \underline{\varepsilon} + 2 \mathcal{C} \underline{\varepsilon} \cdot \delta \underline{\varepsilon} + \mathcal{C} \delta \underline{\varepsilon} \cdot \delta \underline{\varepsilon} dV - \int_B \underline{b} \cdot \underline{u} dV - \int_B \underline{b} \cdot \delta \underline{u} dV - \int_{\partial B} p \cdot \underline{u} dA - \int_{\partial B} p \cdot \delta \underline{u} dA$$

$$\cancel{\Pi(\underline{u})} + \delta \Pi =$$

$$\Rightarrow \delta \Pi = \underbrace{\int_B \mathcal{C} \underline{\varepsilon} \cdot \delta \underline{\varepsilon} - \int_B \underline{b} \cdot \delta \underline{u} dV - \int_{\partial B} p \cdot \delta \underline{u} dA}_{\delta \Pi^{(1)}} + \underbrace{\frac{1}{2} \int_B \mathcal{C} \delta \underline{\varepsilon} \cdot \delta \underline{\varepsilon} dV}_{\delta \Pi^{(2)}}$$

VISTO CHE $\underline{u}(x)$ DEFINISCE UNA
CONFIG. DI EQUILIBRIO, PER IL T.L.V.,

$\delta \Pi^{(1)}$: VARIAZIONE PRIMA

$\delta \Pi^{(2)}$
VARIAZIONE
SECONDA

$\delta \Pi^{(1)} = 0 \quad \forall \delta \underline{u} \Rightarrow$ LA FUNZIONE $\Pi(\underline{u})$ È
STAZIONARIA IN $\underline{u}$

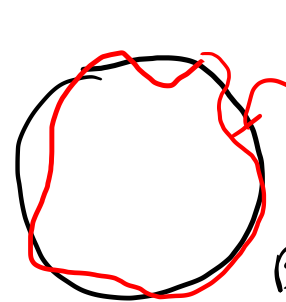
RICORDO. IL T.L.V.,
SIST. (A) STAT. AMMISS.

SOLUT. REALE
↑
 $\underline{\underline{\sigma}}$ in EQUIL. con $\underline{p}$ e $\underline{b}$

$$\begin{cases} \text{div } \underline{\underline{\sigma}} + \underline{b} = \underline{0} \\ \underline{\underline{\sigma}} \cdot \underline{n} = \underline{p} \end{cases}$$



SIST. (B) CINETIC. AMMISS.



$$\underline{\delta u} \rightarrow \underline{\delta \varepsilon} = \frac{1}{2} (\nabla \underline{\delta u} + \nabla \underline{\delta u}^T)$$

$$L_{ve} = L_{vi}$$

$$\int \underline{\underline{\sigma}} \cdot \underline{\delta \varepsilon} dV = \int \underline{p} \cdot \underline{\delta u} dA + \int \underline{b} \cdot \underline{\delta u} dV$$

HA UTILIZZATO

$$L_{ve} - L_{vi} = 0$$

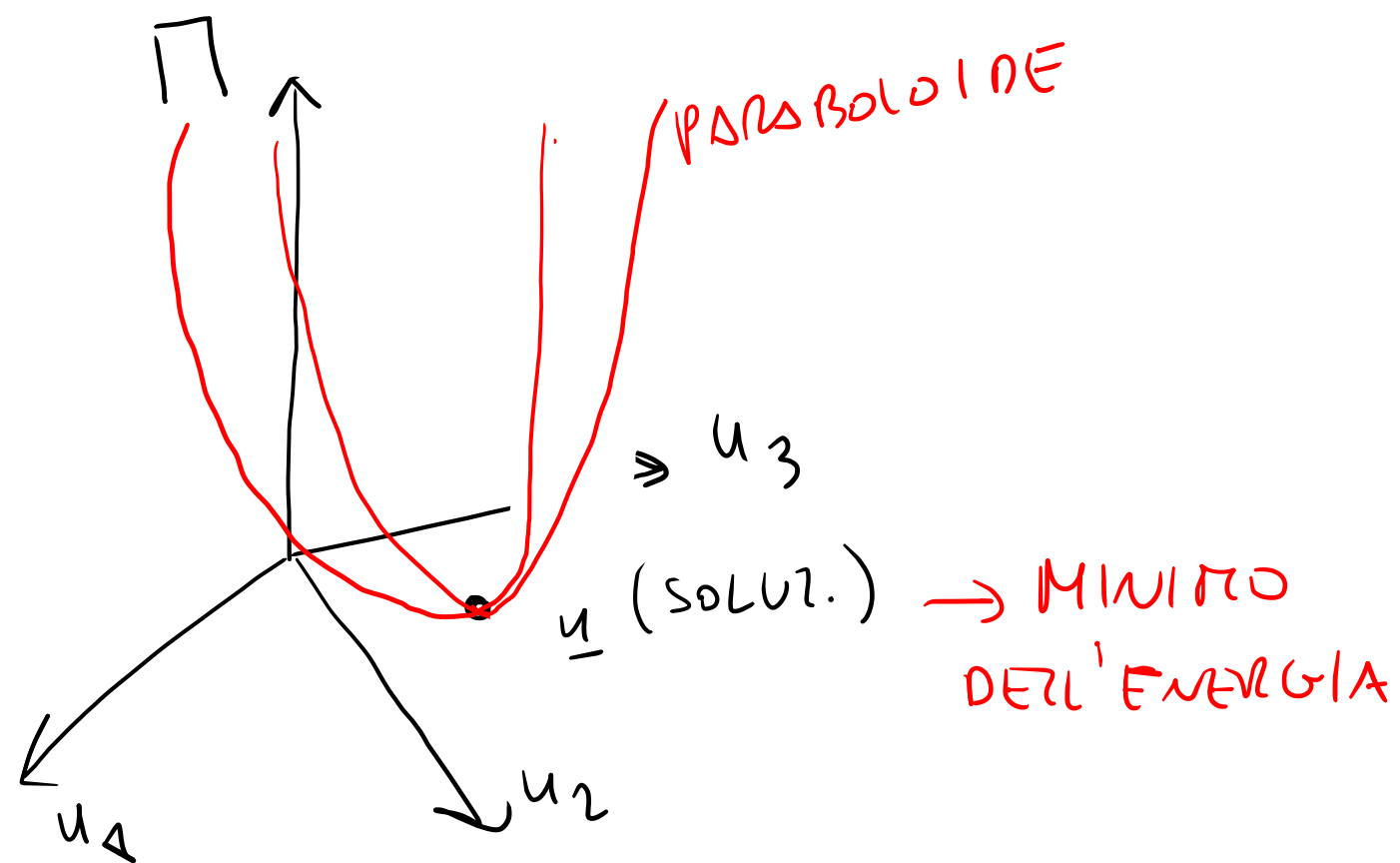
ALL' EQUILIBRIO:

$$\delta \Pi = \delta \Pi^{(2)} \Rightarrow \delta \Pi = \frac{1}{2} \int \mathbb{C} \delta \underline{\underline{\varepsilon}} \cdot \delta \underline{\underline{\varepsilon}} > 0$$

$\mathbb{C}$: TENSORE DEFINITO POSITIVO

$\Rightarrow$ LA CONFIG. DI EQUILIBRIO

$\underline{u}(\underline{x})$ È UN MINIMO DELL' E.P.T.



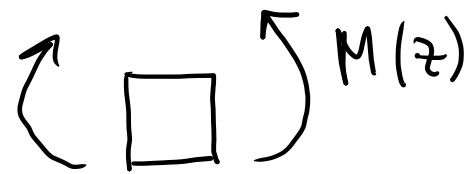
PRINCIPIO DI STAZ. DELL'E.P.T.
 TRA TUTTE LE CONFIGURAZIONI $\underline{u}(x)$
 CONGRUENTI, LA SOLUZ. EQUILIBRATA
 RENDE STAZIONARIA L'E.P.T.

$$\underline{u}: \text{CONGRUENTE} \Rightarrow \delta \Pi^{(1)} = 0 \Rightarrow \underline{u}(x) \text{ SOLUZ.}$$

RICORDIAMOCI CHE $\exists$ L'EN. POT. ^{TOTALE} COMPLEMENTARE

$$\Pi^c(\underline{\sigma}) = \underbrace{\frac{1}{2} \int_B \underline{\sigma} \cdot \underline{C}^{-1} \underline{\sigma} \, dV}_{\Phi^c: \text{EN. ELASTICA COMPL.}} - \int_B \underline{b} \cdot \underline{u} \, dV - \int_{\partial B} \underline{p} \cdot \underline{u} \, dA$$

E.P.T. $\Pi(u)$ DI STR. INFLESSE (EULERO - BERNOLLI)
 DA VINCI



$$d\varphi = \kappa dz$$

$$\text{CURVATURA} = -v''(z)$$

$$d\Phi = \frac{1}{2} M d\varphi : \frac{1}{2} M \kappa dz = -\frac{1}{2} M v''(z) dz \rightsquigarrow$$

$$\Phi = -\frac{1}{2} \int_{SM} M v''(z) dz$$

EN ELASTICA
 NEL CONCIO
 ELEMENTARE
 (MOM. FLETTENTE)

$$\Phi = \frac{1}{2} \int_{SM} EJ (v''(z))^2 dz$$

$$M = -EJ v''(z)$$

EN ELASTICA

POT. ELASTICO ESTERNO

$$\Pi(v) = \frac{1}{2} \int_{SM} EJ v''(z)^2 dz - \int_{SM} q v(z) dz$$

E.P.T. TRAVI SUELT
 INFLESSE