

24/3/25

RESULT THAT: $\Pi(\underline{u}) = \frac{1}{2} \int_{\Omega} \underline{\tilde{\varepsilon}} \cdot \underline{C} \underline{\tilde{\varepsilon}} dV - \int_{\partial\Omega} \underline{p} \cdot \underline{u} dS - \int_{\Omega} \underline{b} \cdot \underline{u} dV$

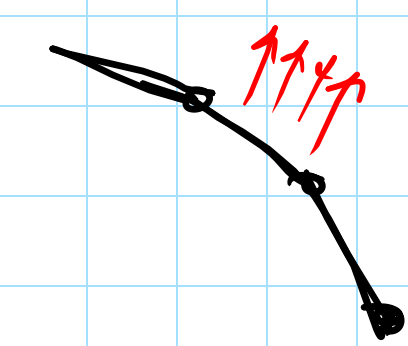
$\tilde{\Pi} = \sum_{e=1}^m \left(\frac{1}{2} \int_{\Omega_e} \underline{B}_e \underline{D}_e \cdot \underline{C} \underline{B}_e \underline{D}_e dV - \int_{\partial\Omega_e} \underline{p} \cdot \underline{N}_e \underline{D}_e dS - \int_{\Omega_e} \underline{b} \cdot \underline{N}_e \underline{D}_e dV \right)$

$\delta \tilde{\Pi} = \frac{\partial \tilde{\Pi}}{\partial \underline{D}} \delta \underline{D} = \sum_{e=1}^m \left[\frac{\partial \tilde{\Pi}_e}{\partial \underline{D}_e} \right] \delta \underline{D}_e = 0 \quad ; \quad \left[\frac{\partial \tilde{\Pi}_e}{\partial \underline{D}_e} = \underline{0} \right] \quad e=1, \dots, m$

$\frac{\partial \tilde{\Pi}_e}{\partial \underline{D}_e} = \int_{\Omega_e} \underline{B}_e^T \underline{C} \underline{B}_e dV \underline{D}_e - \int_{\partial\Omega_e} \underline{N}_e^T \underline{p} dS - \int_{\Omega_e} \underline{N}_e^T \underline{b} dV = \underline{0}$

STIFFNESS MATRIX $\underline{K}_e$ EQUIV. SURFACE FORCE VECTOR EQUIVALENT FREE-BODY FORCE VECTOR

$\underline{K}_e \underline{D}_e - \underline{P}_e - \underline{B}_e = \underline{0}$



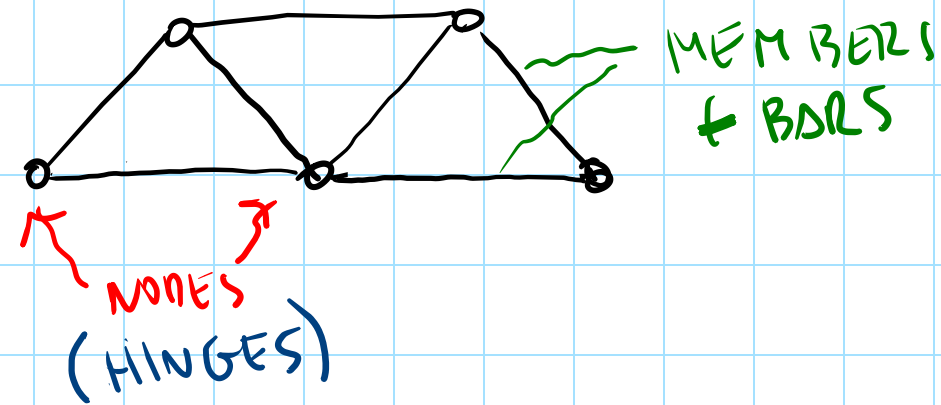
$Q = \frac{1}{2} \underline{A} \underline{D}_e \cdot \underline{D}_e$
 $\frac{\partial Q}{\partial \underline{D}_e} = \underline{A} \underline{D}_e$

DIMENSIONS CHECK

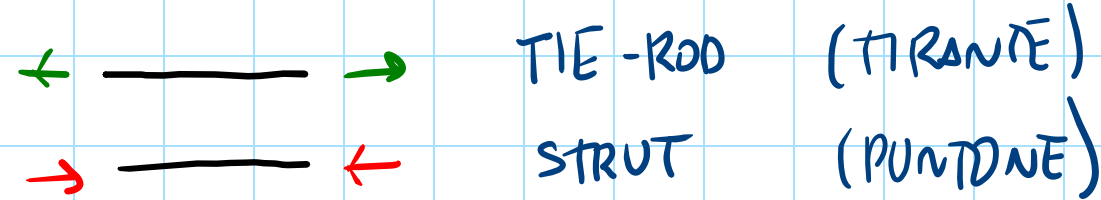
$\underline{K}_e : \underline{3m \times 3m} : (3m \times 6)(6 \times 6)(6 \times 3m)$
 $\underline{P}_e, \underline{B}_e : \underline{3m} : (3m \times 3) 3$

VERY IMPORTANT : $\underline{K}_e$: SYMMETRIC ($\underline{C}$ IS SYMM.)
 $\underline{K}_e$: POSITIVE DEFINITE ($\underline{C}$ IS POSIT. DEFINITE)
 $\underline{K}_e$ HAS GOT THE PROPERTIES OF $\underline{C}$

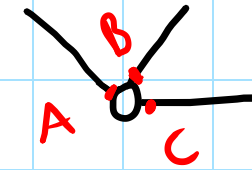
TRUSS STRUCTURES (PLANE)



BEHAVIOUR OF A BAR



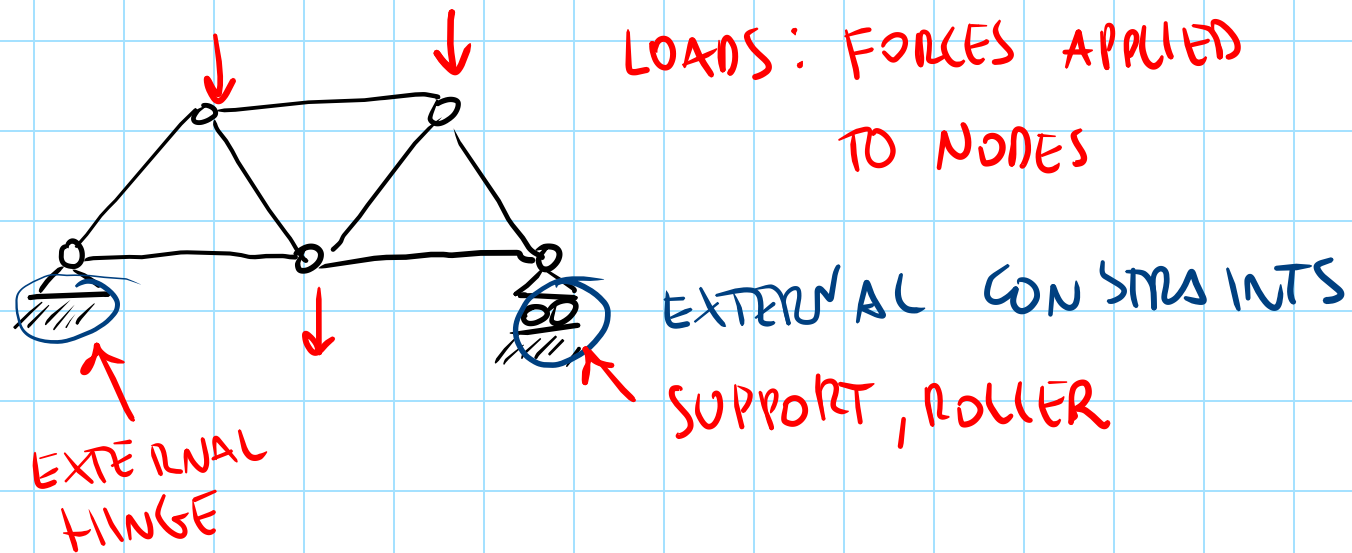
HINGE: CERNIERA



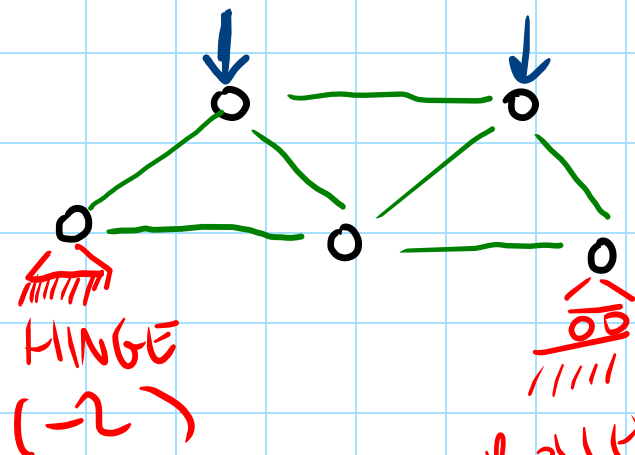
$$u_A = u_B = u_C$$

ROTATIONS AT THE HINGE ARE FREE

FOR EACH BAR



DEGREES OF FREEDOM OF A TRUSS STRUCTURE



$$5 \times 2 = 10 \text{ dofs}$$

$$7 \text{ bars} = -7 \text{ dofs}$$

$$\text{EXTERN} = -3 \text{ dofs}$$

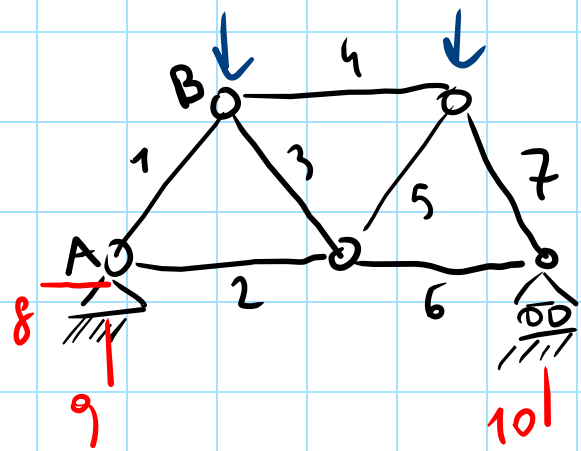
$$0 \text{ dofs} : \text{MINIMUM NO. OF CONSTRAINTS}$$

3 dofs remaining
(RIGID BODY IN THE PLANE)

STRUCTURE IS FIXED

ISOSTATIC STRUCTURE

HOW MANY UNKNOWNS FOR THE PROBLEM IN THE PREVIOUS PAGE?



2 TYPES: $\rightarrow$ NODAL DISPLACEMENTS (KINEMATICS) (a)

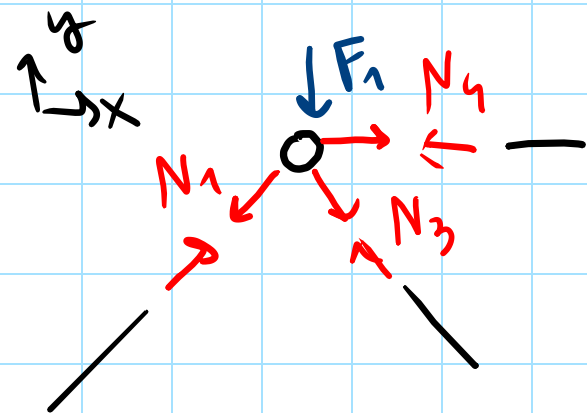
$\rightarrow$ FORCES IN BARS AND EXTERNAL REACTIONS (STATICS) (b)

FOCUS ON (b): HOW MANY? **(10)**

FOR EACH NODE WE CAN WRITE 2 SCALAR EQUATIONS $\rightarrow$ **(10)** EQS TOTAL

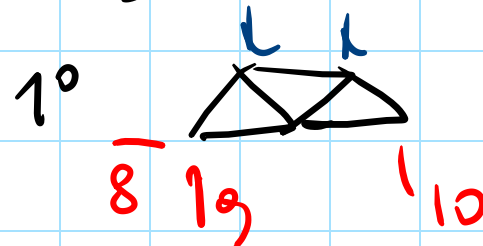
FOR AN ISOSTATIC STRUCTURE THE STATIC UNKNOWN^S CAN BE DETERMINED ONLY FROM THE MAXIMAL SYSTEM OF EQUILIBRIUM EQUATIONS

(EX: NODE B:

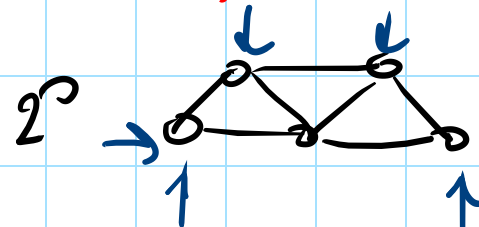


$$\begin{aligned} \sum F_x &= 0 \\ \sum F_y &= 0 \end{aligned}$$

USUALLY, FOR AN ISOST. STRUCT., WE CAN FIRST SOLVE EXTERNAL CONSTRAINTS ⁽³⁾, THEN, 2^o STEP, SOLVE INTERNAL UNKNOWN^S ⁽⁷⁾



3 GLOBAL EQUATIONS $\rightarrow$ 8, 9, 10



7 REMAINING EQS $\rightarrow$ 1, 2, ..., 7

TAKE OUT MESSAGE FROM ISOSTATIC STRUCTURES:

m_N : NO. OF NODES
 m_A : NO. OF BARS
 v_E : NO. OF EXTERNAL CONSTRAINTS

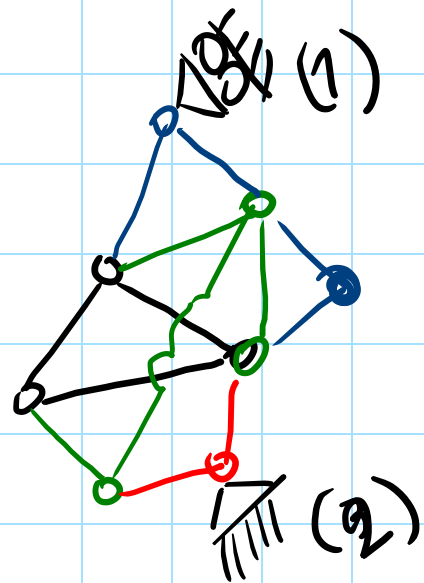
$\Rightarrow$ A NECESSARY
 CONDITION
 FOR A STRUCT.
 TO BE ISOSTATIC
 IS

MAXWELL RULE

$$2m_N = m_A + v_E$$

ISOSTATIC STRUCTURES ARE ALSO CALLED
 "DETERMINED" STRUCTURES

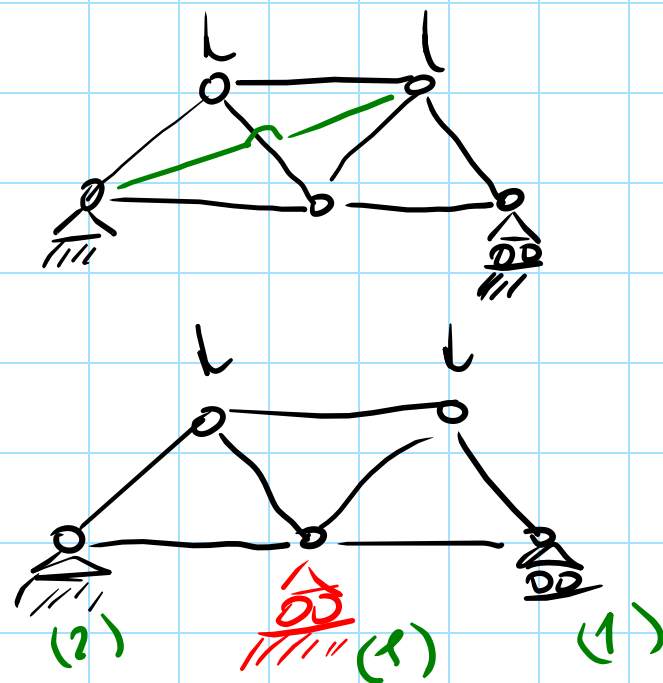
A TRICK TO BUILD A RIGID BODY COMPOSED OF NODES AND BARS



$m_N: 8$
 $m_A: 13$
 $v_E: 3$
 $16 = 13 + 3$
 OK

OVERCONSTRAINED STRUCTURES

/ ISOSTATIC STR
 — REDUNDANT STR.



ISOSTATIC STR + INTERNAL BAR

$$10 < 8 + 3$$

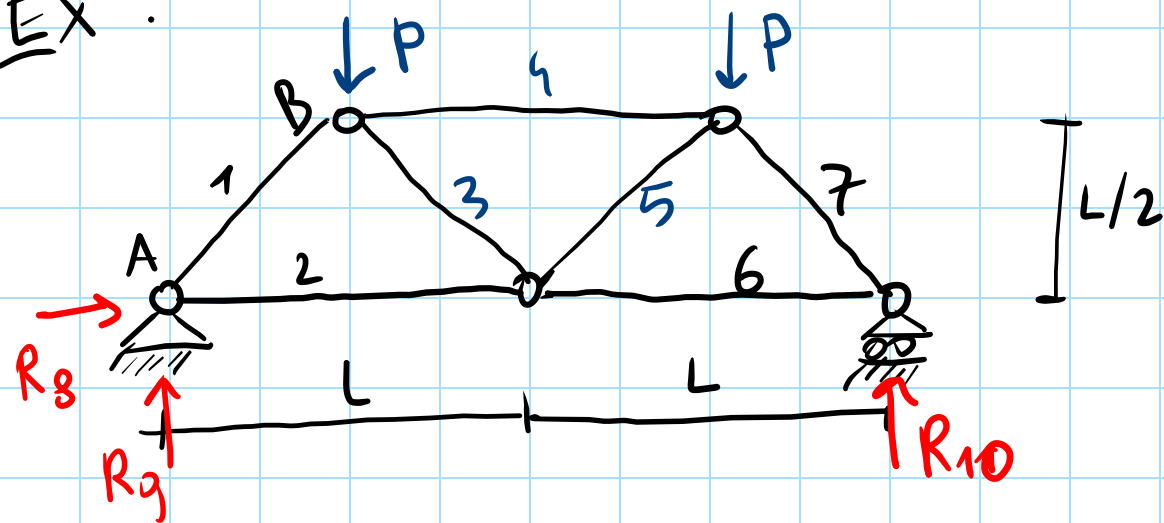
ISOSTATIC STR. + EXTERNAL CONSTRAINT

$$10 < 7 + 4$$

IN BOTH CASES I HAVE 11 UNKNOWN

10 EQUILIB. EQS
 + 1 ?? MUST INVOLVE
 ELASTICITY OF THE
 SYSTEM

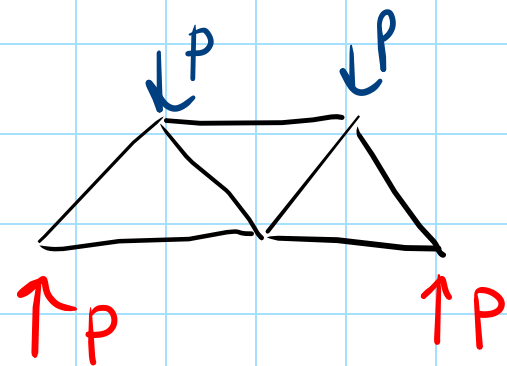
Ex .



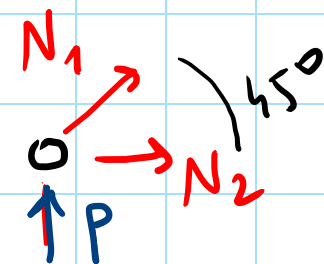
RESULTS:

$N_1 = -P\sqrt{2}$	:	STRUT
$N_2 = +P$	:	TIE-ROD
$N_6 = +P$	:	" "
$N_7 = -P\sqrt{2}$	:	STRUT

1°)



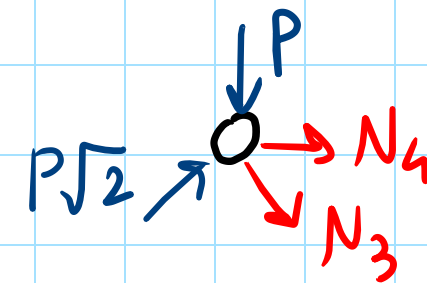
2°) Node A



$$\left. \begin{aligned} \sum F_x = 0 : N_2 + N_1 \frac{1}{\sqrt{2}} &= 0 \\ \sum F_y = 0 : P + N_1 \frac{1}{\sqrt{2}} &= 0 \end{aligned} \right\}$$

$$N_1 = -P\sqrt{2} \quad ; \quad N_2 = +P$$

3°) Node B



WE CAN SOLVE

