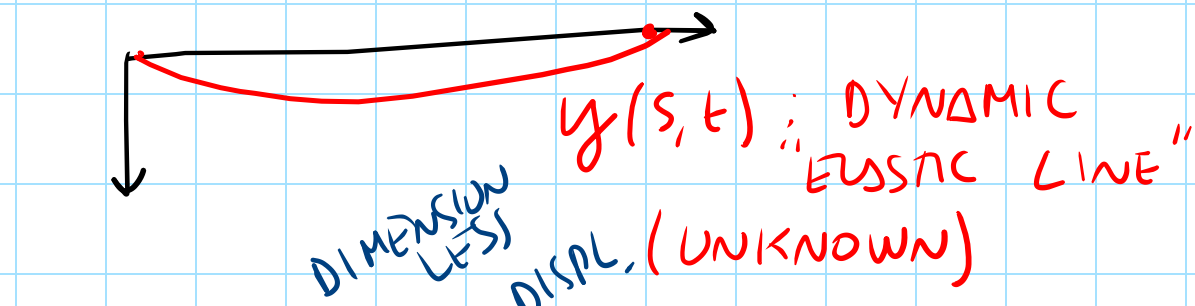
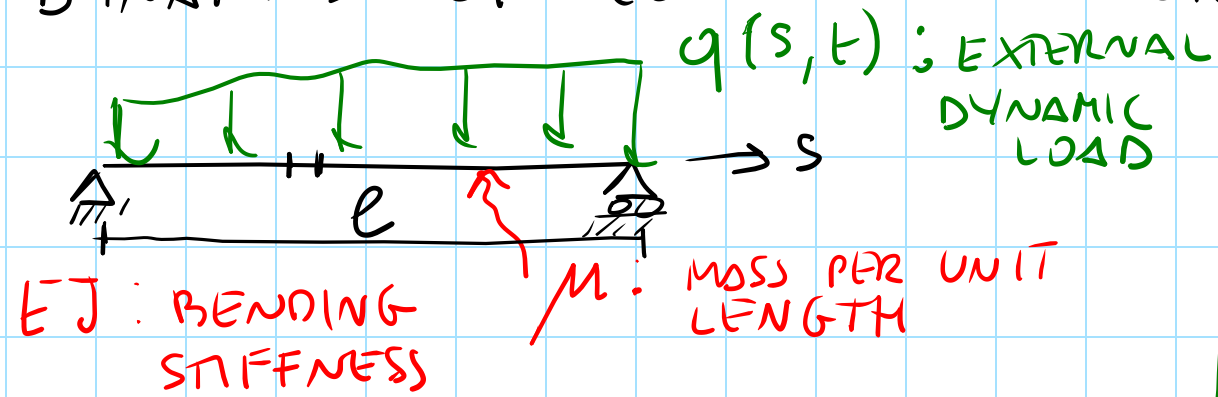


DYNAMICS OF CONTINUOUS SYSTEMS MODELLED AS 1 D.O.F.



$$y(s,t) = \underbrace{\psi(s)}_{\text{SHAPE FUNCTION (MUST FULFILL SOME CONDITIONS)}} x(t)$$

$$\dot{y} = \psi(s) \dot{x}(t) \quad \text{SEPARAT. OF VARIABLES}$$

$$\chi = -y'' = -\psi''(s)x(t) \quad \text{CURVATURE}$$

$$M(s,t) = -EJ y'' = -\psi''(s)x(t)EJ$$

A GENERALISED

HOW TO DETERMINE THE EQ. OF MOTION

$$\frac{d}{dt} [E_{kin} + E_{pot}] = \text{POWER OF EXT LOAD } q$$

$$E_{kin} = \frac{1}{2} \int_0^l m ds \dot{y}^2 = \frac{1}{2} \int_0^l m \psi^2(s) ds \dot{x}^2(t) = \frac{1}{2} m_{eq} \dot{x}^2$$

m_{eq} : EQUIV. MASS

$$E_{pot} = E_{ELASTIC} = \frac{1}{2} \int_0^l M \chi ds = \frac{1}{2} \int_0^l (-\psi'' x EJ) (-\psi'' x) ds$$

$$= \frac{1}{2} \int_0^l EJ \psi''^2 ds x^2 = \frac{1}{2} k_{eq} x^2$$

k_{eq} : EQUIV. STIFFNESS

POWER EXT LOAD q : $\int_0^l q ds \psi \dot{x} = \int_0^l q \psi ds \dot{x}$

(F_v)

F_{eq} : EQUIV. FORCE

$$\frac{d}{dt} \left[\frac{1}{2} m_{eq} \dot{x}(t)^2 + \frac{1}{2} K_{eq} x(t)^2 \right] = F_{eq} \dot{x}(t)$$

$$m_{eq} \ddot{x}(t) \cancel{\dot{x}(t)} + K_{eq} \cancel{\dot{x}(t)} x(t) = F_{eq} \cancel{\dot{x}(t)}$$

$$\Rightarrow \boxed{m_{eq} \ddot{x}(t) + K_{eq} x(t) = F_{eq}}$$

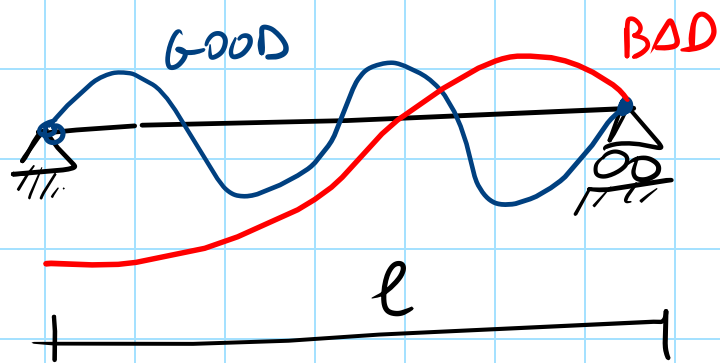
1 D.O.F. GOVERNING EQUAT.
(GENERALISED) (NO DISSIPATION)

$\psi(s)$: SHAPE FUNCTION TO BE CHOSEN
CAREFULLY (SEE BOUNDARY CONDITIONS)

FREE MOTION: $m_{eq} \ddot{x}(t) + K_{eq} x(t) = 0 \Rightarrow \omega^2 = \frac{K_{eq}}{m_{eq}} = \frac{\int_0^l EJ \psi''^2 ds}{\int_0^l \mu \psi^2 ds}$

ω : CIRCULAR FREQUENCY

REQUIREMENTS ON $\psi(s)$: THEY MUST SATISFY "GEOMETRIC"
BOUNDARY CONDITIONS (CONSTRAINT CONDITION)



$$EJ \psi'''' = q$$

$$\psi(0) = 0$$

$$\psi(l) = 0$$

GEOMETRIC

$$\psi''(0) = 0$$

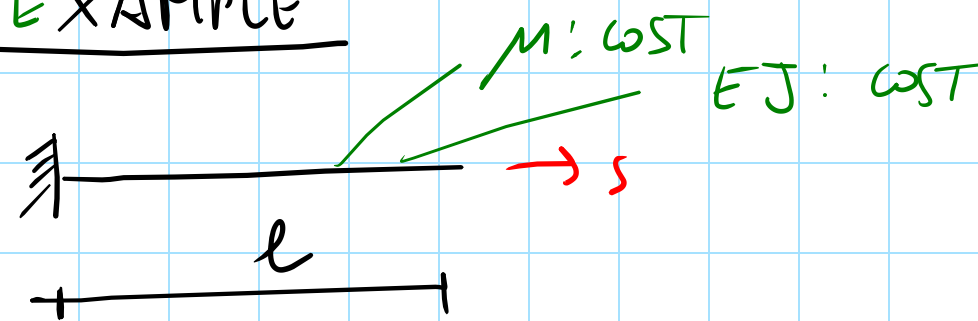
$$\psi''(l) = 0$$

ESSENTIAL

RAYLEIGH RATIO

(DEPENDS ON ψ)
 ψ "WORKS" SIMILAR TO
VIBRATION MODES

EXAMPLE



LET US STUDY FREE VIBRATION

EXACT SOLUTION : $\omega_{\text{EXACT}} = \frac{3.516}{l^2} \sqrt{\frac{EJ}{\mu}}$

$\psi_{\text{EXACT}} = \psi(\cos, \sin, \cosh, \sinh \text{ whose argument is } (\frac{s}{l}))$

OBS : LET US CHECK DIMENSION OF ω

$$[\omega] = \frac{1}{L^2} \sqrt{\frac{FL^2}{M}} = \frac{1}{L^2} \sqrt{\frac{\cancel{F} \cancel{L}^2 \cancel{L}^2}{\cancel{F} T^2}} = \frac{1}{T}$$

$$[\omega] = \left[\frac{1}{T} \right]$$

$$F = M \frac{L}{T^2} \Rightarrow M = \frac{FT^2}{L}$$

1) I APPROX

$$\psi_1 = \frac{3s^2}{2l^2} - \frac{s^3}{2l^3}$$

$$\psi_1(0) = 0 ; \psi_1'(0) = 0 \quad \text{OK VERIFIED}$$

$$m_{eq}^{(1)} = 0.236 \mu l$$

$$K_{eq} = 3 \frac{EJ}{l^3}$$

$$\Rightarrow \omega^{(1)} = \frac{3.568}{l^2} \sqrt{\frac{EJ}{\mu}}$$

ERROR : 1.5%

2) II APPROX

$$\psi_2(s) = 1 - \cos \frac{\pi s}{2l}$$

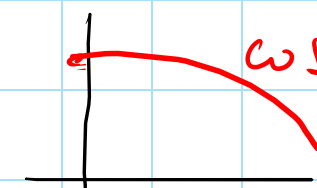
$$\psi_2(0) = 0 ; \psi_2' = \sin \frac{\pi s}{2l} \cdot \frac{\pi}{2l} \Rightarrow \psi_2'(0) = 0$$

$$m_{eq}^{(2)} = 0.227 \mu l$$

$$K_{eq}^{(2)} = 3.044 \frac{EJ}{l^3}$$

$$\Rightarrow \omega^{(2)} = \frac{3.664}{l^2} \sqrt{\frac{EJ}{\mu}}$$

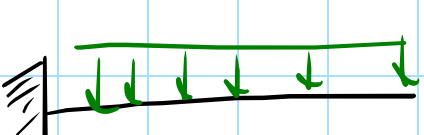
ERROR 4%

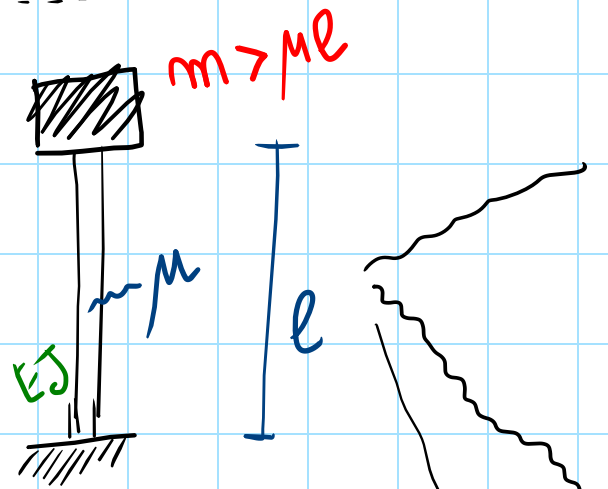


OBJ: THE TWO SHAPE FUNCT. SELECTED ^{ALSO} SATISFY $\psi''_k(l) = 0$ ($k=1,2$) (BENDING MOMENT

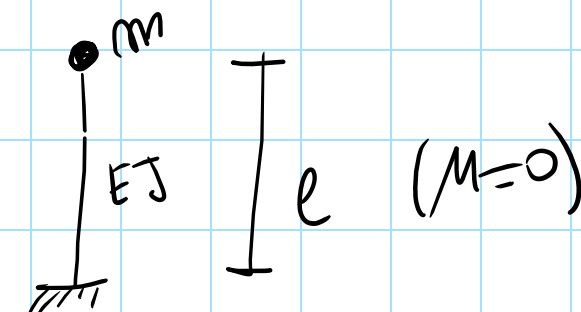
NULL AT THE THE TIP OF THE CANTILEVER). THIS CONDITION IS NOT STRICTLY REQUIRED.

$\Rightarrow$ ONE POSSIBLE INITIAL GUESS FOR $\psi(s)$ COULD BE THE SOLUTION OF THE "STATIC" ELASTIC LINE.

 $\Rightarrow$ SOLVE STATIC ELASTIC LINE " $v(s)$ " $\Rightarrow \psi_1(s) = v(s)$

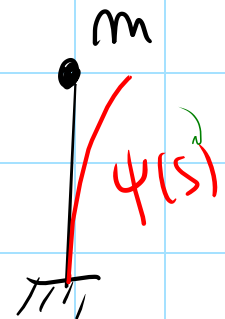


DIFFERENT
APPROX.
WAYS

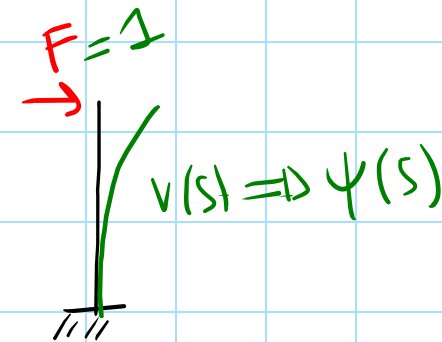


$$K = \frac{3EI}{l^3}$$

GENERALISED
1 D.O.F.



$\psi(s)?$



F.E.M. (NUM. METHOD)

