

Air Duct Calculation

Marco Manzan

University of Trieste
Department of Engineering and Architecture

May 2024

Basic Concepts

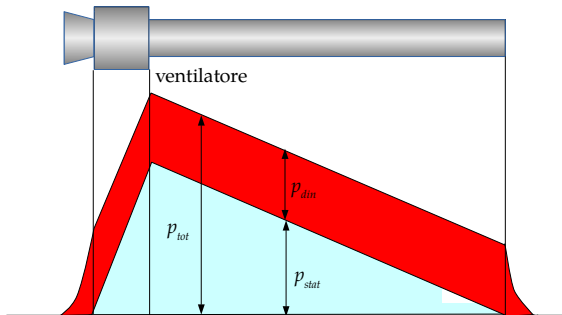
- With constant cross-section in segments (section changes are localized).
- Composed of different branches, with splits and mergers that cause variations in flow rate.
- The air velocity in the ducts must be chosen based on the system's use and the location of the ducts to limit noise.
- Velocity is also important because it determines the pressure distribution within the ducts.
- In junctions and branches, all arms have the same static pressure value.

Dynamic and Total Pressure

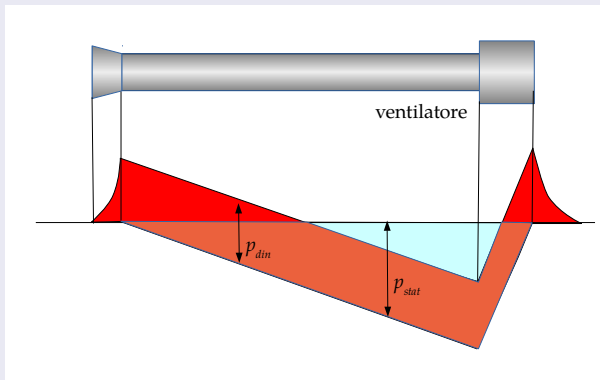
$$P_{dyn} = \frac{1}{2} \rho v^2 > 0 \text{ [Pa]}$$

$$P_{tot} = P_{dyn} + P_{stat}$$

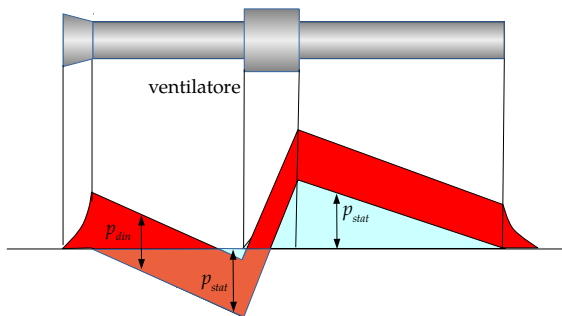
Pressure Trend in a Duct



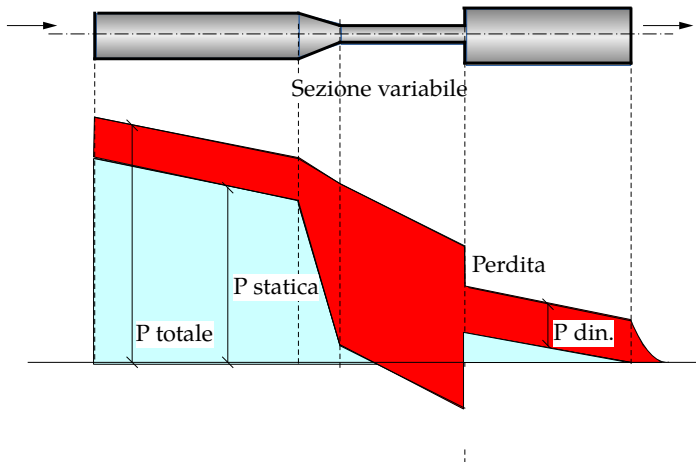
Suction



Intermediate Fan



Variable Cross-Section



Componente	Impianti		
	residential (m/s)	commercial (m/s)	industrial (m/s)
external inlet	2,5-4,0	2,5-4,5	2,5-6,0
Filteers	1,3-1,5	1,5-1,8	1,8-2,5
cold coil	1,5-2,0	2,0-2,5	2,5-3,8
hot coil	2,3-2,5	2,5-4,0	3,5-5,0
ventilator inlet	3,5-4,5	4,0-5,0	5,0-7,0
ventilator outlet	5,8-8,5	6,5-11,0	8,0-14,0
principal air duct	3,5-6,0	5,0-8,0	6,0-11,0
derivated air duct	3,0-5,0	3,0-6,5	4,5-9,0

Continuous pressure losses

$$\Delta P_{dist} = \frac{f_a}{D_h} \rho \frac{v^2}{2} L = \frac{f}{D} P_{dyn} L$$

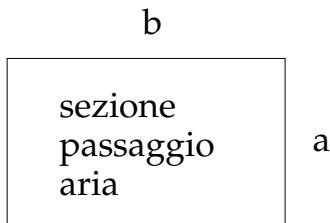
f_a friction factor

ρ fluid density

L duct length

D_h duct diameter if circular

Rectangular section



Equivalent Diameter

$$D_{eq} = 1,3 \frac{(ab)^{0,625}}{(a+b)^{0,25}}$$

$$1 \leq \frac{b}{a} \leq 4$$

Standard duct sizes

lunghezza del lato [mm]	100	150	200	250	300	400	500	600	800	1000	1200	
200	0,02	0,03	0,04									A ₁
	133	171	200									d ₁
	149	186	218									d ₂
	0,6	0,7	0,8									A ₁
250	0,025	0,038	0,05	0,063								A ₂
	143	188	222	250								d ₁
	165	206	241	273								d ₂
	0,7	0,8	0,9	1								A ₁
300	0,03	0,045	0,06	0,075	0,09							A ₂
	150	200	240	273	300							d ₁
	180	224	262	296	327							d ₂
	0,3	0,9	1	1,1	1,2							A ₁
400	0,04	0,06	0,08	0,1	0,12	0,16						A ₂
	160	218	267	308	343	400						d ₁
	205	255	299	337	373	436						d ₂
	1	1,1	1,2	1,3	1,4	1,6						A ₁
500		0,075	0,1	0,13	0,15	0,2	0,25					A ₂
		231	286	333	375	444	500					d ₁
		283	331	374	413	483	545					d ₂
		1,3	1,4	1,5	1,6	1,8	2					A ₁
600		0,09	0,12	0,15	0,18	0,24	0,3	0,36				A ₂
		240	300	353	400	480	545	600				d ₁
		307	359	406	448	524	592	654				d ₂
		1,5	1,6	1,7	1,8	2	2,2	2,4				A ₁
800			0,16	0,2	0,24	0,32	0,4	0,48	0,64			A ₂
			320	381	436	533	615	686	800			d ₁
			410	463	511	598	675	745	872			d ₂
			2	2,1	2,2	2,4	2,6	2,8	3,2			A ₁

lunghezza del lato [mm]	100	150	200	250	300	400	500	600	800	1000	1200	
1000				0,25	0,3	0,4	0,5	0,6	0,8	1		A ₂
				400	462	571	667	750	889	1000		d ₁
				512	566	662	747	825	965	1090		d ₂
1200				2,5	2,6	2,8	3	3,2	3,6	4		A ₁
					0,36	0,48	0,6	0,72	0,96	1,2	1,44	A ₂
					480	600	706	800	960	1091	1200	d ₁
1400					614	719	812	896	1049	1184	1308	d ₂
					3	3,2	3,4	3,6	4	4,4	4,8	A ₁
						0,56	0,7	0,84	1,12	1,4	1,68	A ₂
1600						622	737	840	1018	1167	1292	d ₁
						771	871	962	1125	1270	1403	d ₂
						3,6	3,8	4	4,4	4,8	5,2	A ₁
1800						0,64	0,8	0,96	1,28	1,6	1,92	A ₂
						640	762	873	1067	1231	1371	d ₁
						819	925	1022	1195	1350	1491	d ₂
2000						4	4,2	4,4	4,8	5,2	5,6	A ₁
							0,9	1,08	1,44	1,8	2,16	A ₂
							783	900	1108	1286	1440	d ₁
2200							976	1078	1261	1424	1573	d ₂
							4,6	4,8	5,2	5,6	6	A ₁
							1	1,2	1,6	2	2,4	A ₂
2400							800	923	1143	1333	1500	d ₁
							1024	1131	1323	1494	1650	d ₂
							5	5,2	5,6	6	6,4	A ₁

Friction factor computation

Colebrook

$$\frac{1}{\sqrt{f_a}} = -2 \log \left(\frac{\varepsilon}{3,7 \cdot D} + \frac{2,51}{Re \cdot \sqrt{f_a}} \right)$$

Atshul e Tsaal

$$f' = 0,11 \cdot \left(\frac{\varepsilon}{D_h} + \frac{68}{Re} \right)^{0,25}$$

$$\text{se } f' \geq 0,018 : f_a = f'$$

$$\text{se } f' < 0,018 : f_a = 0,85 \cdot f' + 0,0028$$

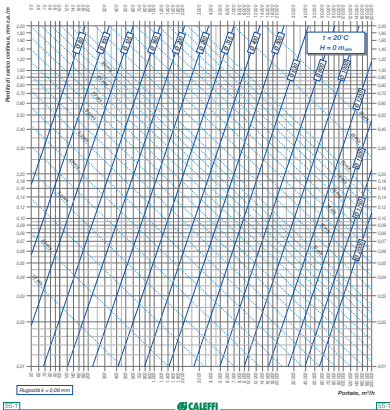
ε duct rugosity

Re Reynolds number

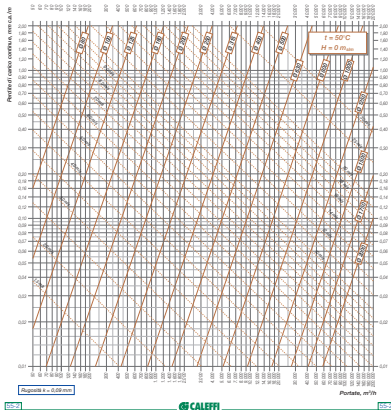
material	typology	rugosità ε [mm]
PVC	smooth	0,01-0,05
Alluminium		0,01-0,05
Steel		0,05
galvanized steel	medium	0,05-0,10
galvanized steel continuous		0,06 - 0,12
galvanized spiral duct		0,09 - 0,12
metal flexible	rough	1,2-2,1
not metal flexible		1,0-4,6

Friction chart

Perdite di carico continue dell'aria – CONDOTTI CIRCOLARI "LISCI" – $t = 20^\circ\text{C}$, $H = 0 \text{ m}_{\text{abs}}$



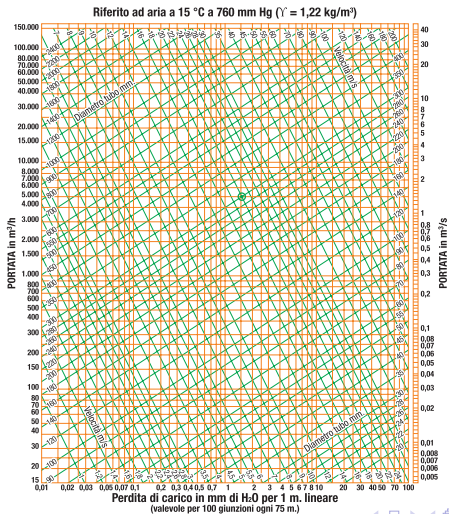
Perdite di carico continue dell'aria – CONDOTTI CIRCOLARI "LISCI" – $t = 50^\circ\text{C}$, $H = 0 \text{ m}_{\text{abs}}$



fonte Caleffi

Friction chart

> Diagramma perdite di carico <



Direct method

$$\Delta P_{conc} = \xi \frac{\rho v^2}{2} [Pa]$$

$$\Delta P_{conc} = \xi_1 \frac{\rho v_1^2}{2} = \xi_2 \frac{\rho v_2^2}{2}$$

equivalent length

$$L_{eq} = f \left(\frac{L}{D} \right)$$

$$L_{tot} = L_{effettiva} + \sum L_{eq}$$

> Tabella resistenze accidentali <

Canali rettangolari - valori indicativi dei coefficienti ξ - derivazioni e confluenze

Derivazioni a 90° $\xi_p = 0.2$ $\xi_s = 1.3$		Derivazioni a 30°, 45° e 60° $\xi_p = 0.2$ $\xi_s = 0.7, 0.9$	
Derivazioni con riduzione a 90° $\xi_p = 0.1$ $\xi_s = 1.3$		Derivazioni con riduzione a 30°, 45° e 60° $\xi_p = 0.1$ $\xi_s = 0.6, 0.7, 0.9$	
Derivazione a doppia curva $\xi_p = 0.30, 0.75, 1.00, 1.50, 2.00$ $\xi_s = 0.5, 0.5, 0.5, 0.5, 0.5$		Confluenza a doppia curva $\xi_p = 0.30, 0.75, 1.00, 1.50, 2.00$ $\xi_s = 0.5, 0.5, 0.5, 0.5, 0.5$	
Derivazione ad Y $\xi_p = 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9$		Confluenza a Y $\xi_p = 0.2, 0.3, 0.4, 0.5, 0.6, 0.7, 0.8, 0.9$	
Derivazione a T $\xi_p = 0.4$		Confluenza a T $\xi_p = 1.3$	

Pressione dinamica		Per $\gamma = 1,22 \text{ kg/m}^3$ $g = 9,81 \text{ m/s}^2$	
$pd = \frac{\gamma C^2}{2g}$		C	pd
		m/s	mm H ₂ O
Perdite accidentali $\Delta p = K \times pd$ (pd riferita alla velocità nel punto →)			
INGRESSO E SCARICO	$K = 0.5$ $K = 1.25$		
	$K = 0.5$ $K = 0.7$		
	$R/D = 0.25, 0.5, 0.75, 1, 1.5, 2$ $K = 0.2, 0.1, 0.08, 0.1, 0.08$		
	$a = 15, 30, 45, 60$ $K = 0.5, 0.5, 0.5, 0.4$		
	$K = 1$		
CURVE	$R/D = 0.5, 0.75, 1, 1.5, 2$ $K = 0.25, 0.1, 0.08, 0.1, 0.08$		
	$a = 10, 30, 45, 60, 90$ $K = 0.05, 0.2, 0.5, 0.7, 1.2$		
	$R/W = 0.5, 0.75, 1, 1.5, 2$ $K = 1, 0.5, 0.25, 0.15, 0.1$		
	$R/W = 0.5, 0.75, 1, 1.5, 2$ $K = 0.05, 0.2, 0.5, 0.7, 1.2$		
	$K = 0.3$		
BIFORCAZIONI	$K = 1.4$		
	$a = 10, 30, 45, 60$ $K = 0.1, 0.5, 0.7, 1.2$		
	$R/W = 0.5, 0.75, 1, 1.5$ $K = 0.1, 0.5, 0.7, 1.2$		
	$a = 15, 30, 45, 60, 90$ $K = 0.1, 0.5, 0.7, 1.2$		
	$R/D = 0.5, 0.75, 1, 1.5$ $K = 1.3, 0.9, 0.8, 0.6$		
CAMBIO DI SEZIONE	$\alpha = 10^\circ - 45^\circ$ $K = 0.1$		
	$\alpha = 5^\circ, 15^\circ, 30^\circ, 45^\circ, 60^\circ, 75^\circ, 90^\circ$ $K = 0.05, 0.2, 0.25, 0.4, 0.6, 0.8, 0.9$		
	$F = \text{Superficie}$ $F_1/F_2 = 0.2, 0.4, 0.6, 0.8, 1$ $K = 0.45, 0.2, 0.2, 0.1$		
	$F = \text{Superficie}$ $F_1/F_2 = 0.2, 0.4, 0.6, 0.8, 1$ $K = 1, 0.7, 0.4, 0.2, 0.1$		

Tubazioni rettangolari - Diametri equivalenti a parità di Perdita per attrito e di Perdita d'aria																				
b	a	250	300	350	400	450	500	550	600	650	700	750	800	850	900	1000	1200	1400	1600	1800
Diametri equivalenti																				
150	210	220	245	265	275	290	300	310	320											
200	245	265	285	305	320	340	360	380	390	400	415	430	445	455	470	480	495	505	520	
250	275	300	325	345	365	380	400	410	430	445	455	470	480	495	505	520	535	545	560	
300		350	380	405	430	450	460	480	495	510	525	540	555	565	580	600	615	625	640	
350			440	465	490	515	535	555	575	590	610	625	645	660	675	700	720	730	750	
400				490	520	545	565	585	610	630	650	670	685	705	725	750	770	790	810	
450					540	575	600	625	645	665	685	710	725	745	760	780	800	820	840	

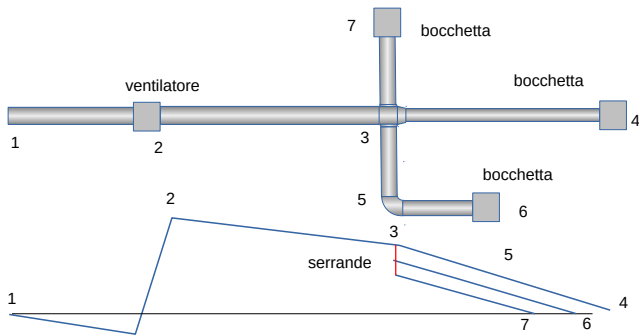
Esempio: La tubazione $\varnothing 300 \text{ mm}$ per una portata di $5000 \text{ m}^3/\text{h}$ ha una perdita di carico di $1.6 \text{ mm H}_2\text{O}$ per metro. Per la medesima portata e uguale perdita di resistenza si dovranno usare le seguenti tubazioni rettangolari: $a \times b = 150 \times 500, 200 \times 400, 250 \times 300 \text{ mm}$.

Equal friction method

- quick and simple method
- ideal for symmetrical systems with similar distances between vents and fans
- the ducts are sized with the same pressure loss per unit of length
- it must be checked that the pressure at the vents is sufficient
- they must be balanced
 - change sizes
 - dampers insertion

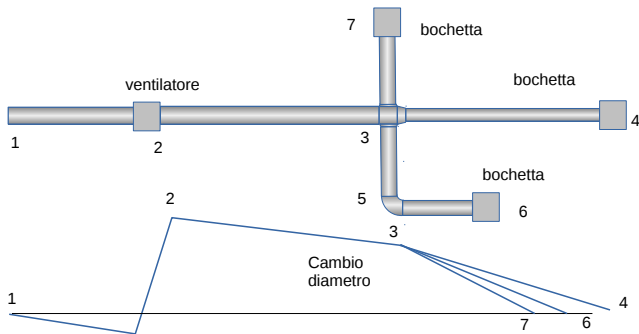
Equal friction method

system balancing with dampers



Equal friction methods

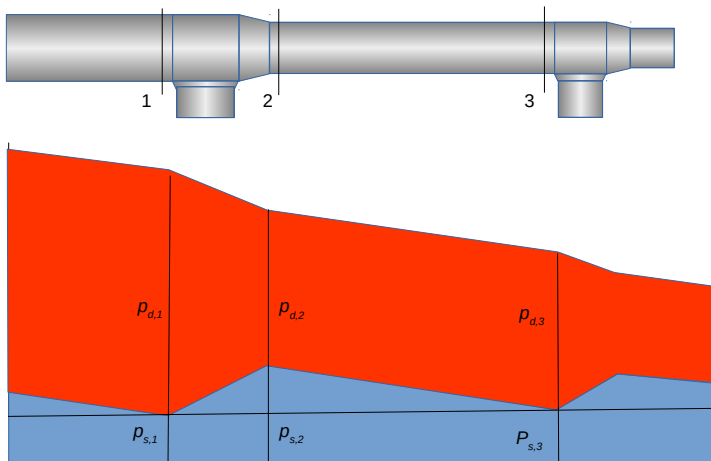
system balance by changing duct diameter



Static regain method

- at each section change the dynamic pressure is transformed into static pressure
- the value of P_{stat} is maintained at the beginning of each section
- the static pressure is kept constant
- can be used to maintain low pressures on the duct wall
- iterative solution
- more balanced network

Pressure distribution



Duct sizing

pressure

$$p_{t,1} = p_{s,1} + p_{d,1}$$

$$p_{t,3} = p_{s,3} + p_{d,3}$$

static pressure

$$p_{s,1} = p_{t,1} - p_{d,1}$$

$$p_{s,3} = p_{t,3} - p_{d,3}$$

constant static pressure

$$p_{s,1} - p_{s,3} = p_{t,1} - p_{t,3} - (p_{d,1} - p_{d,3}) = 0$$

$$p_{s,1} - p_{s,3} = (p_{t,1} - p_{t,2}) + (p_{t,2} - p_{t,3}) + (p_{d,3} - p_{d,1}) = 0$$

Duct sizing

parts of the relation

$(p_{t,1} - p_{t,2})$ pressure loss due to diverging fitting

$(p_{t,2} - p_{t,3})$ friction pressure loss between section 2 and 3

$(p_{d,3} - p_{d,1})$ velocity pressure difference between section 3 and 1

different static pressure

- ducts sizes are limited
- usually static pressure are not equal
- the diameter must be changed with a trial and error approach
- example : $p_{s,1} - p_{s,3} > 0$

$$p_{s,1} - p_{s,3} = (p_{t,1} - p_{t,2}) + (p_{t,2} - p_{t,3}) + (p_{d,3} - p_{d,1}) > 0$$

Duct sizing

Increase duct diameter of section 2-3

- $(p_{t,1} - p_{t,2})$ pressure loss must be computed from fittings tables
- $(p_{t,2} - p_{t,3}) \Downarrow$ friction pressure loss decreases since the diameter increased
- $(p_{d,3} - p_{d,1}) \Downarrow$ decrease, $p_{d,3}$ decreases due to the lower velocity
- $(p_{s,1} - p_{s,3}) \Downarrow$ decrease, before $(p_{s,1} - p_{s,3}) > 0$

$$p_{s,1} - p_{s,3} = (p_{t,1} - p_{t,2}) + (p_{t,2} - p_{t,3}) - (p_{d,1} - p_{d,3}) \Downarrow$$

Pressure difference is corrected

$$p_{s,1} - p_{s,3} = (p_{t,1} - p_{t,2}) + (p_{t,2} - p_{t,3}) - (p_{d,1} - p_{d,3}) \simeq 0$$