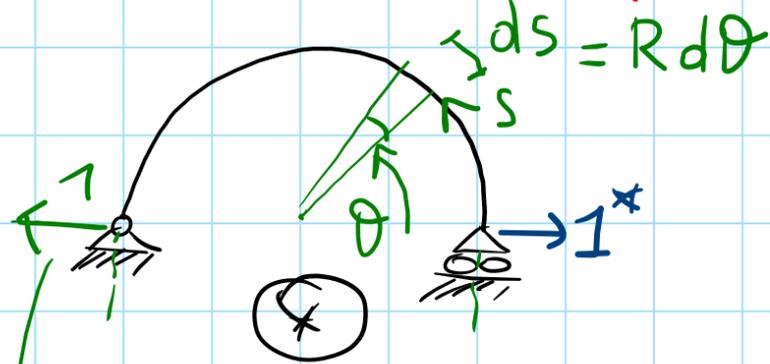
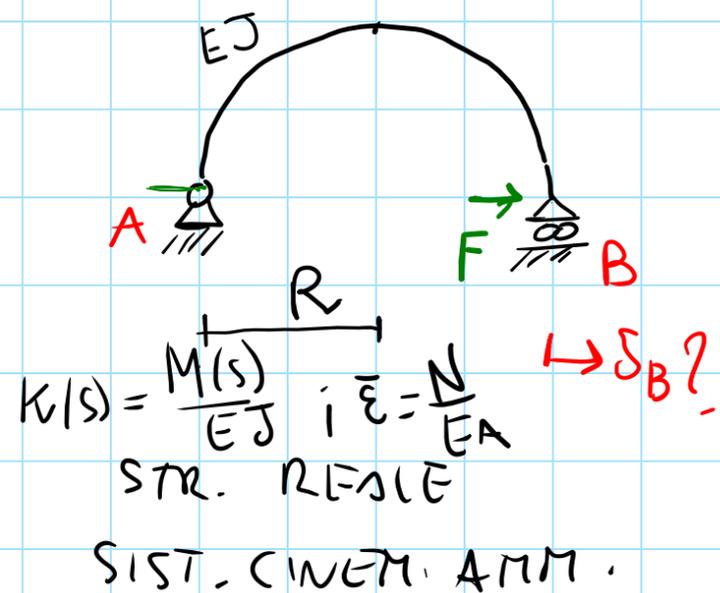


ES : TRASCURARE LA DEF. ASSIALE ( $EA \rightarrow \infty$ )

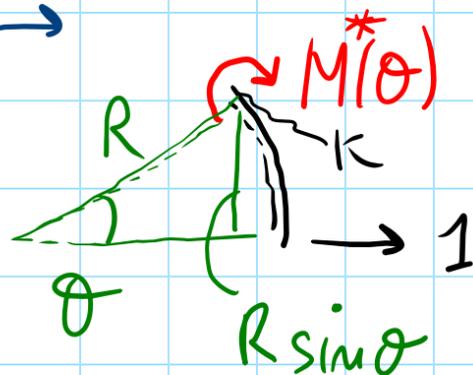
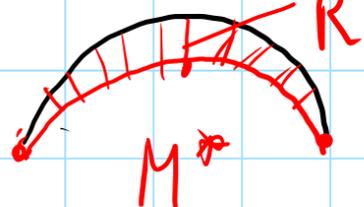
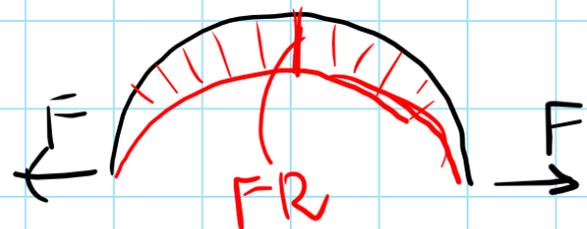
10/12/25



$$\delta_B = \int_{SM} M^*(s) \frac{M(s)}{EJ} + N^*(s) \left( \frac{N(s)}{EA} \right) ds$$

$$L_{ve} = L_{vi}; \quad 1^* \cdot \delta_B + 1 \cdot 0 = \int_{SM} M^*(s) K(s) + N^*(s) \bar{\epsilon}(s) ds$$

$$\delta_B = \int_{SM} M^*(s) \frac{M(s)}{EJ} ds \Rightarrow \delta_B = \int_{SMR} M^*(\theta) \frac{M(\theta)}{EJ} R d\theta$$



$$k^{\uparrow+}: -M^*(\theta) + 1 \cdot R \sin \theta = 0$$

$$M^*(\theta) = R \sin \theta \quad \theta \in [0, \pi]$$

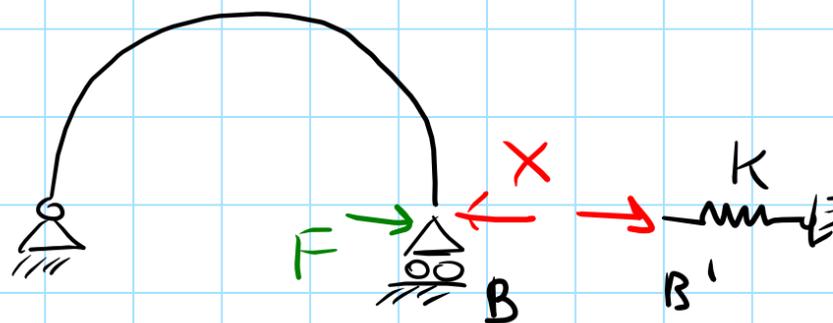
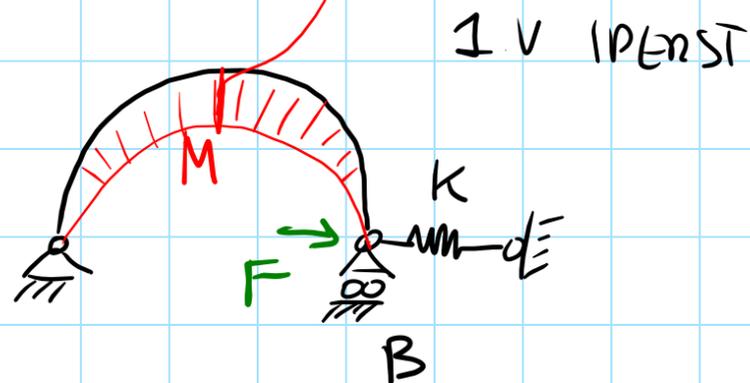
$$[M^*] = [L]$$

$$\delta_B = \int_0^\pi R \sin \vartheta \cdot \frac{FR \sin \vartheta}{EJ} R d\vartheta; \quad \delta_B = \frac{R^3 F}{EJ} \int_0^\pi \sin^2 \vartheta d\vartheta = \frac{FR^3}{EJ} \left[ \frac{\vartheta}{2} - \frac{\sin 2\vartheta}{4} \right]_0^\pi$$

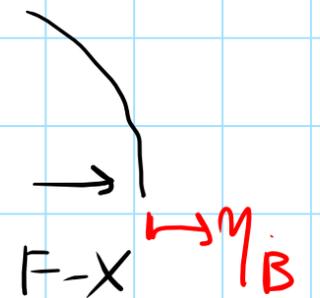
$$\delta_B = \frac{FR^3}{EJ} \left( \frac{\pi}{2} - 0 \right) = \frac{\pi}{2} \frac{FR^3}{EJ}$$

SPOSTI CONCORDE  
ALLA FORZA 1\*

APPLICAZ. (F-X)R

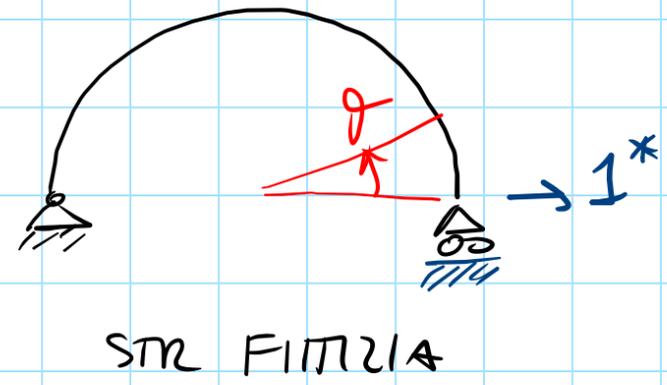
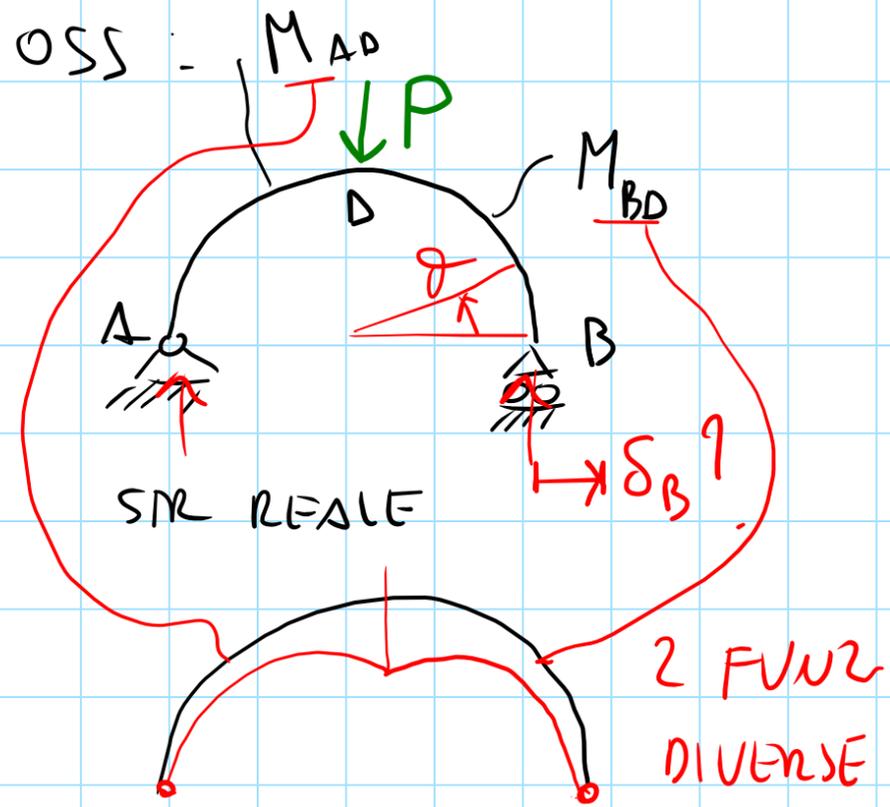


$\uparrow \eta$        $+\frac{X}{K}$   
 $M_B = M_{B'}$   
 EQ. DI CONGR.



$$M_B (F-X) = + \frac{\pi}{2} \frac{(F-X) R^3}{EJ}$$

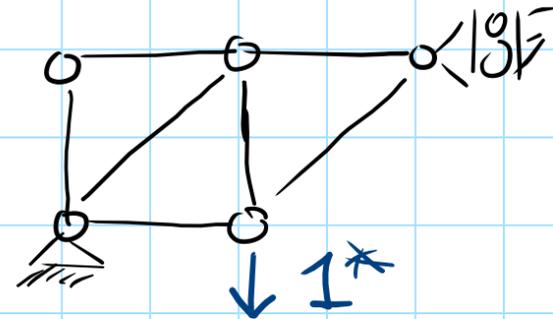
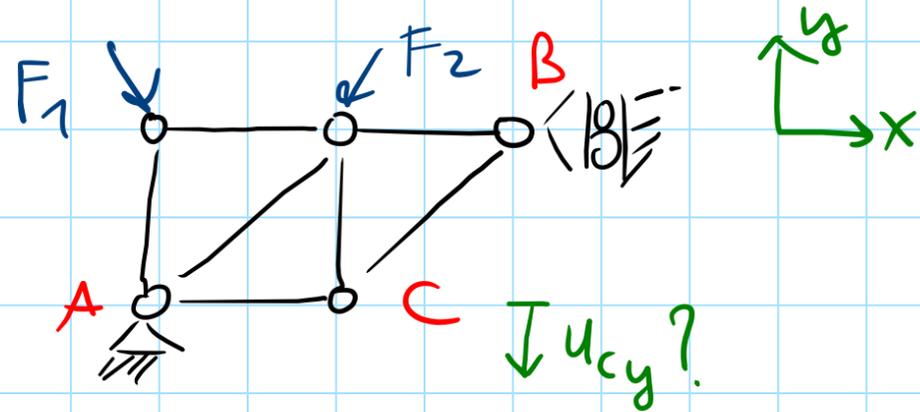
$$(F-X) R^3 \frac{\pi}{2EJ} = + \frac{X}{K} \quad \leadsto \quad X = f(F, EJ, K)$$



$$1^* \cdot \delta_B = \int_{s_m} M^*(s) \frac{M(s)}{EI} ds$$

$$\delta_B = \int_{BD} M^*(\theta) \frac{M_{BD}(\theta)}{EI} R d\theta + \int_{DA} M^*(\theta) \frac{M_{DA}(\theta)}{EI} R d\theta$$

# CALCOLO SPOST. NODALI IN STR. RETICOLARI ISOSTATICHE



T.L.V.

LAVORO FORZE  
(MOMENTI)

CONCENTRATI

NEZ SIST. FITTIZIO

$$= \int_{SM} N^* \bar{\epsilon} ds$$

$$L_{ve} = L_{vi}$$

STR REALE  
SIST. CINEM. AMM

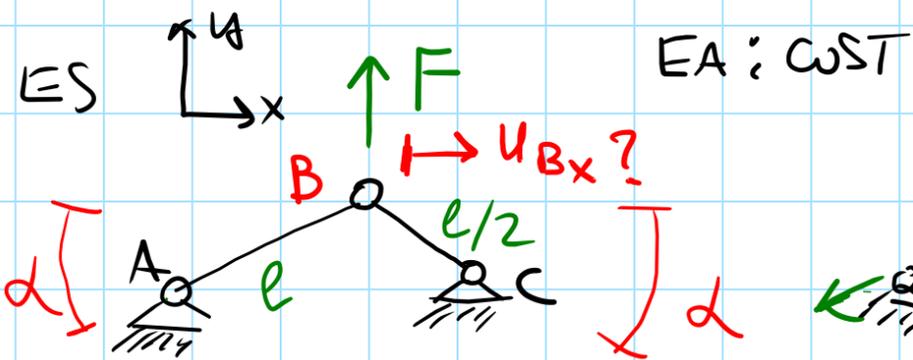
$(u, \bar{\epsilon} \dots)$

$M_a$ :  
N° ASTE

STR FITTIZIA (\*)  
SIST. STAT AMM.

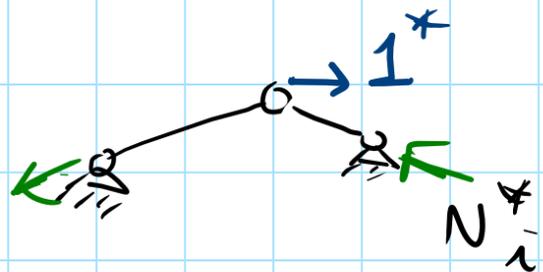
$(N^*)$

$$\text{elaboro } L_{vi} = \int_{SM} N^*(s) \frac{N(s)}{EA} ds = \sum_{i=1}^{M_a} N_i^* \frac{N_i}{(EA)_i} l_i \int ds$$



STR REALE  
SIST. CINEM. AMM

EA: COST

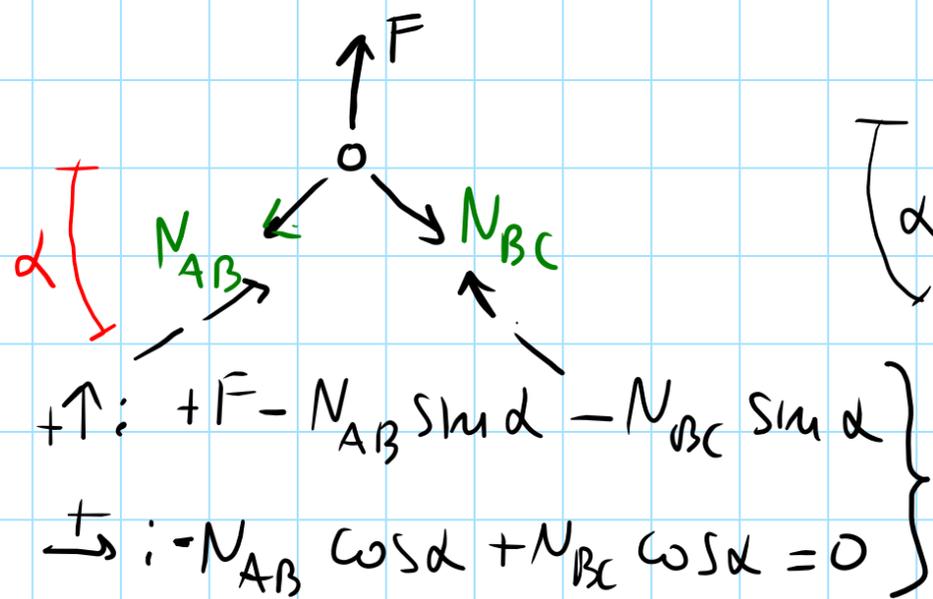


STR FIRTZIA  
SIST. STAT. AMM.

$$1 \cdot u_{Bx} = N_{AB}^* \frac{N_{AB}}{EA} l + N_{BC}^* \frac{N_{BC}}{EA} \frac{l}{2}$$

C: cost  
S: smd

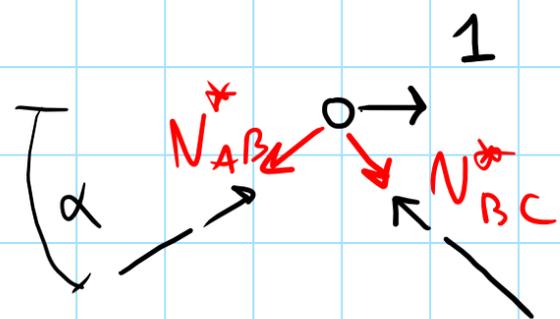
$$u_{Bx} = \frac{l}{EA} \left( \frac{1}{2C} \frac{F}{2S} + \left(-\frac{1}{2C}\right) \frac{F}{2S} \frac{1}{2} \right) = \frac{+ FL}{8CSEEA}$$



$$\begin{cases} +\uparrow: +F - N_{AB} \sin \alpha - N_{BC} \sin \alpha \\ +\rightarrow: -N_{AB} \cos \alpha + N_{BC} \cos \alpha = 0 \end{cases}$$

$$N_{AB} = N_{BC} = + \frac{F}{2 \sin \alpha}$$

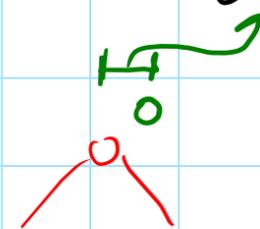
TRAZIONE NELLE ASSE



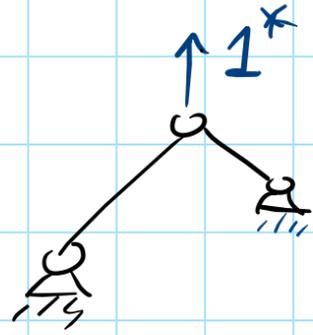
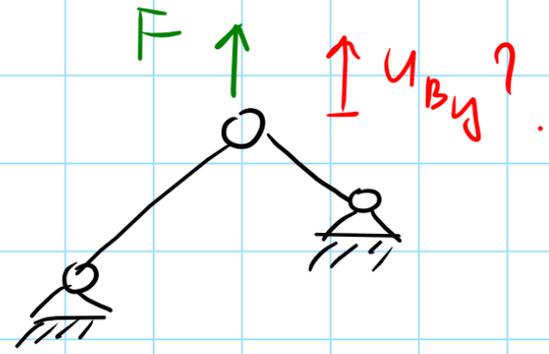
$$\begin{cases} +\uparrow: -N_{AB}^* \sin \alpha - N_{BC}^* \sin \alpha = 0 \\ +\rightarrow: 1 - N_{AB}^* \cos \alpha + N_{BC}^* \cos \alpha = 0 \end{cases}$$

$$\begin{cases} N_{AB}^* = + \frac{1}{2 \cos \alpha} \\ N_{BC}^* = - \frac{1}{2 \cos \alpha} \end{cases}$$

BC PUNTONE



ES

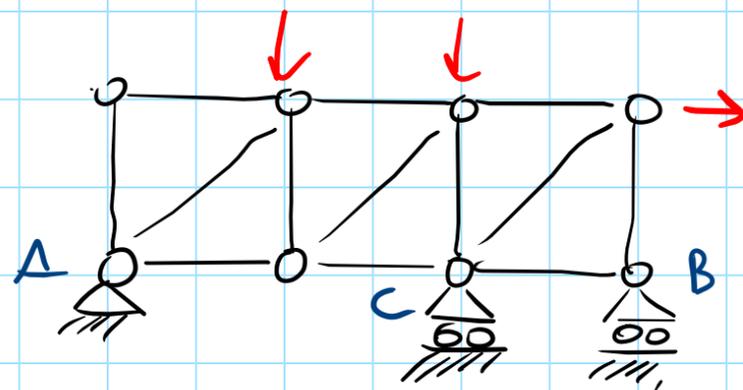


$$N_i = F N_i^*$$

$$1 \cdot u_{By} = N_{AB}^* \frac{N_{AB}}{EA} l + N_{BC}^* \frac{N_{BC}}{EA} \frac{l}{2}$$

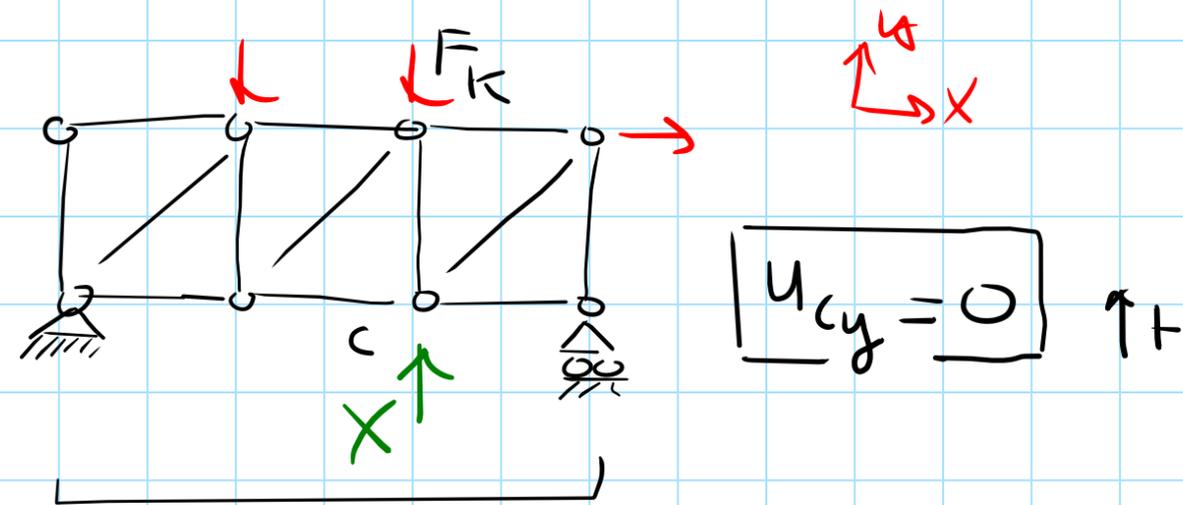
$$u_{By} = \frac{l}{EA} \left( F N_{AB}^{*2} + \frac{1}{2} F N_{BC}^{*2} \right)$$

RETI COLARE IPERST.



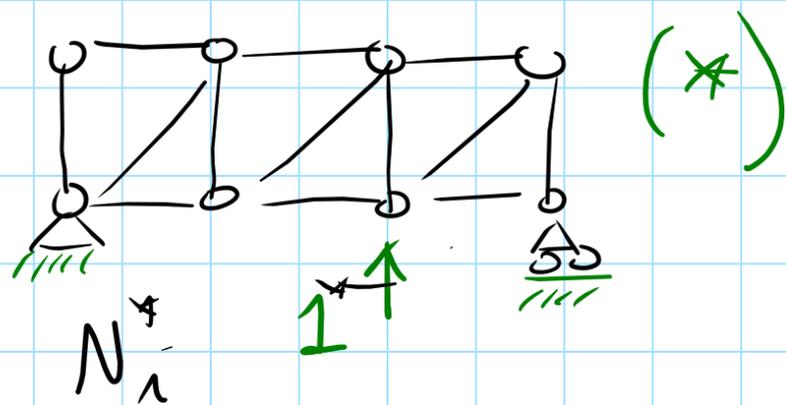
STR 1 V  
IPERST.

S.P.



STR. STAT. DET.  $\Rightarrow$  POSSO CALCOLARE  
QUI  $u_{cy}(F_K, X)$ . COME?

PRENDENDO COME SCHEMA FILTRO

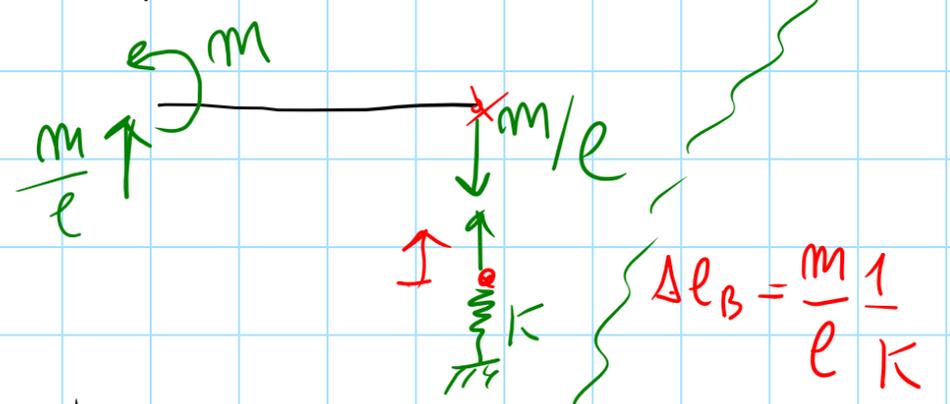
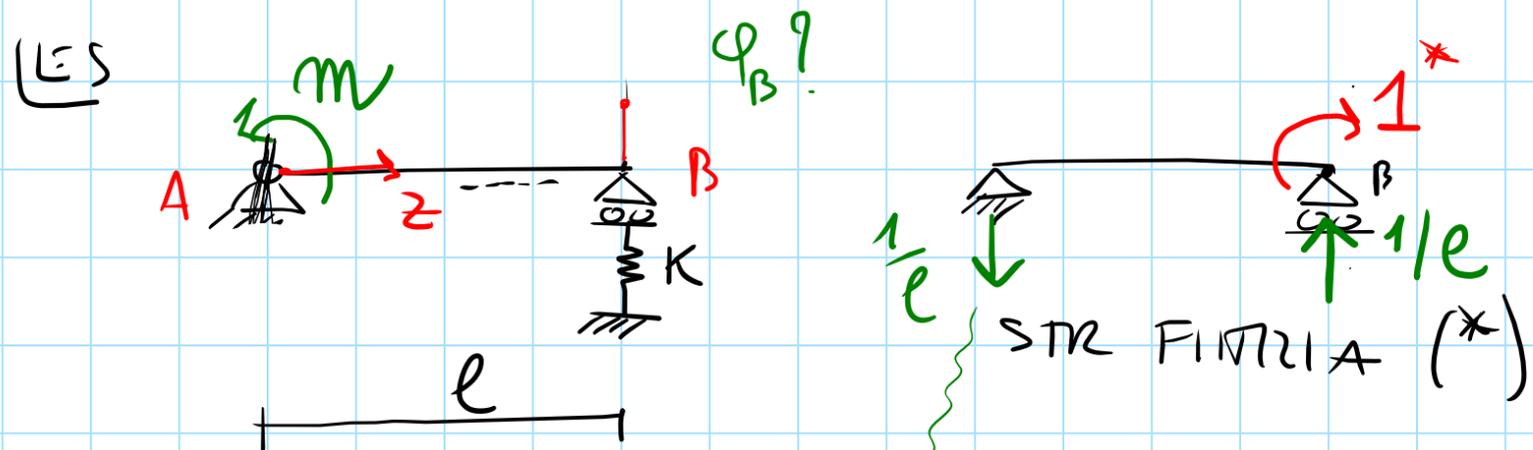


$\Rightarrow$

$$1^* \cdot u_{cy} = \sum_{i=1}^{m_a} N_i^* \frac{N_i(F_K, X)}{EA_i} l_i$$

$u_{cy}(F_K, X)$

POI IMPONGO L'EQ. DI CONGR.  $u_{cy} = 0 \Rightarrow X = f(F_K)$



$L_{ve} = L_{vu}$

$$1^* \varphi_B + \frac{1}{l} \left( +\frac{m}{lK} \right) + \frac{1}{l} \cdot 0 = \int_0^l \frac{M^*(z) M(z)}{EI} dz$$

$$\varphi_B + \frac{m}{l^2 K} = \int dz$$