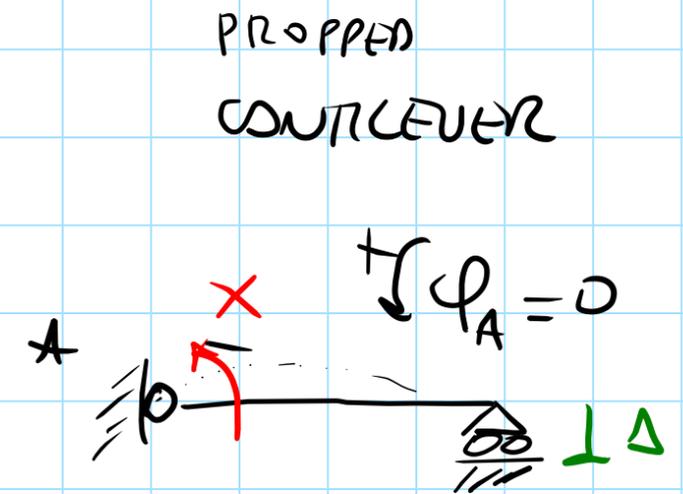
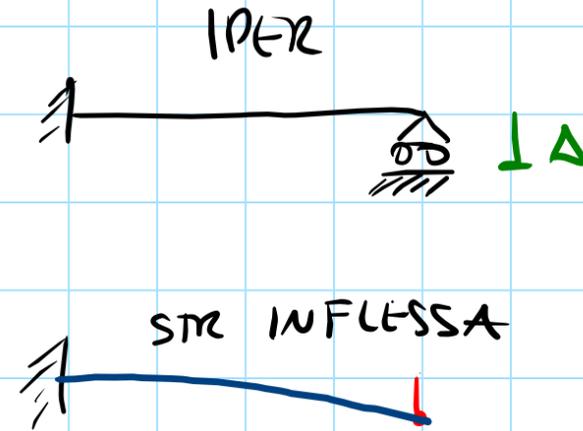
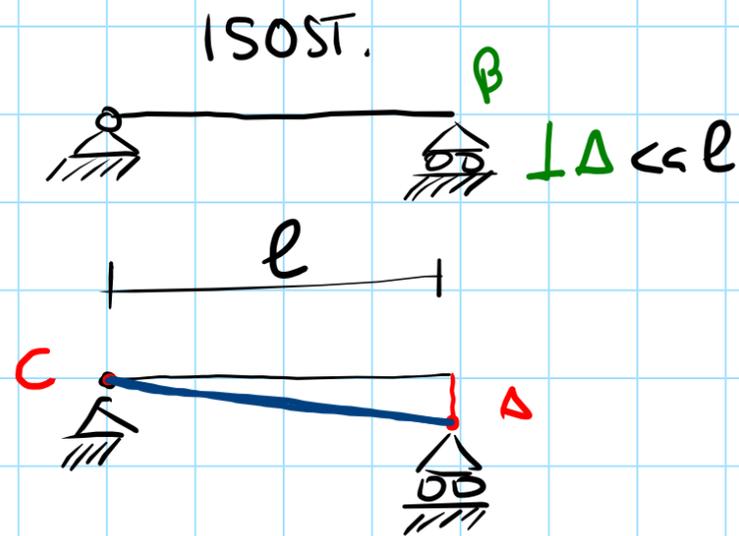


CEDIMENTI ELASTICI NELLE STRUTTURE

18/12/25



LA STRUTTURA "RUOTA"
(SI MUOVE RIGIDAMENTE)
E RAGGIUNGE UNA NUOVA
CONFIGURAZ.

LA STR. SI INFLETTE
(NASCONO SOLLECITAZ.
→ CDS ≠ 0 ← INDOTTE
DAL CEDIMENTO)

NO REAZ. VINCOLARI
NO SOLLECITAZ (CDS NULLE)

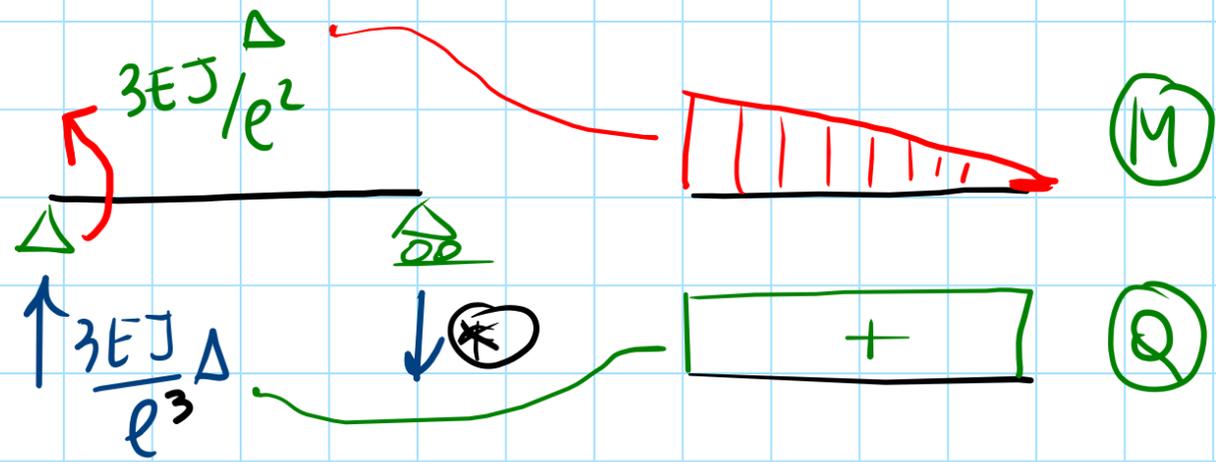
M, Q, N funz. del
cedimento (Δ)

$$\varphi_A(\Delta, x) = 0$$

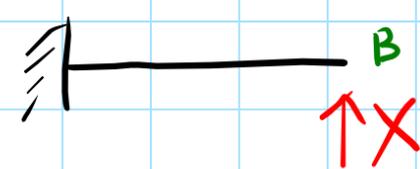
$$\varphi_A(x) = \frac{x^2}{3EI}$$

$$\varphi_A(\Delta) = -\frac{\Delta}{l}$$

$$\frac{x^2}{3EI} - \frac{\Delta}{l} = 0 ; x = \frac{3EI\Delta}{l^2}$$



W ALTERNATIVA:



$v_B = \Delta \downarrow +$

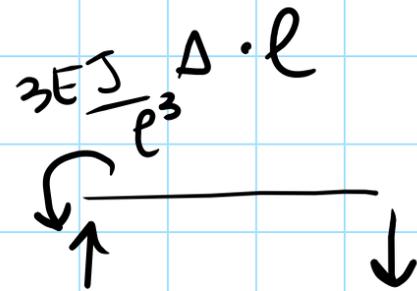
$[v_B(x)]$

$-\frac{x^3}{3EJ} = \Delta$

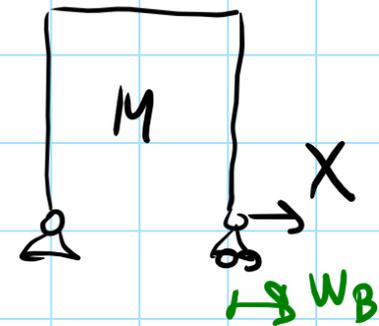
\Rightarrow

$x = -\frac{3EJ \Delta}{e^3}$

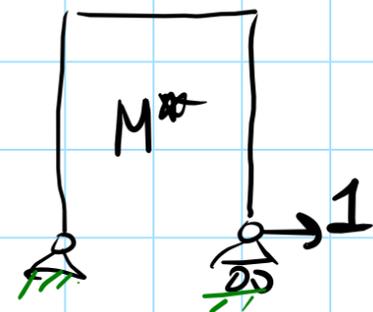
(*)



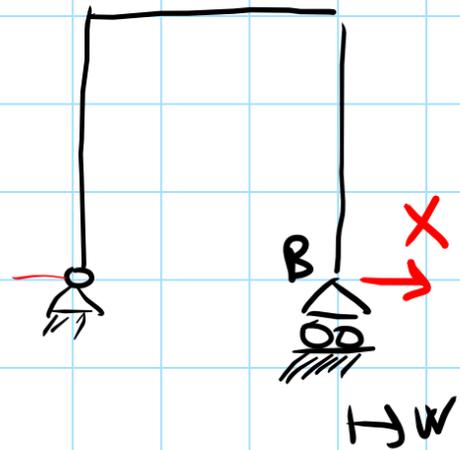
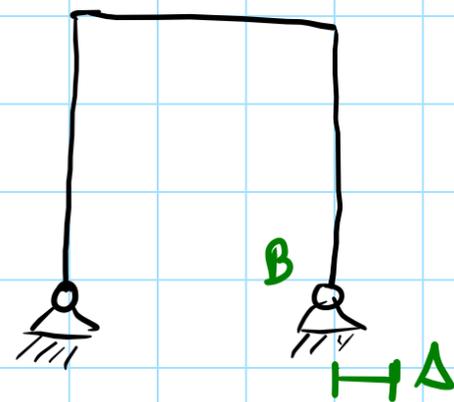
W_B CON Δ APPLICAZ.
T.L.V.



STR REALE

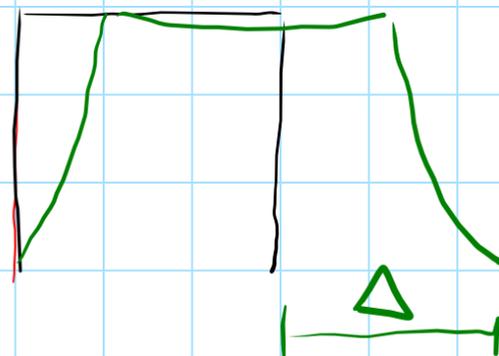


STR FINZIA

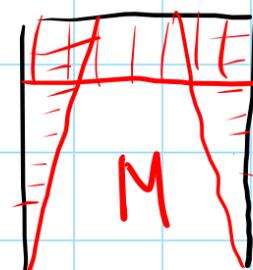


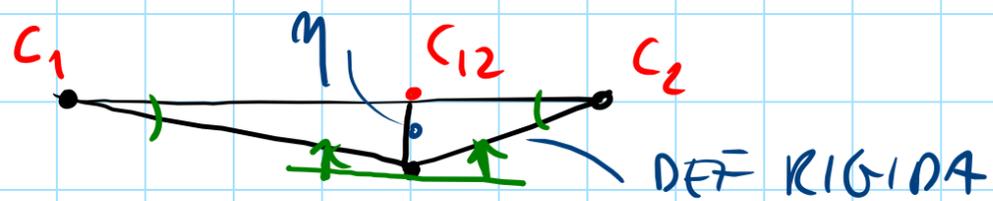
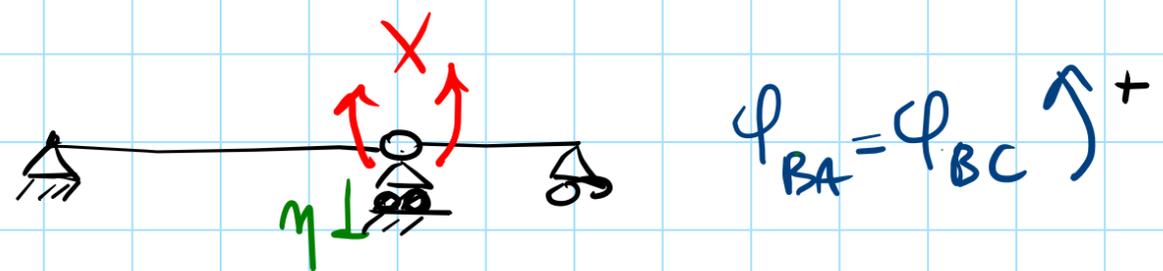
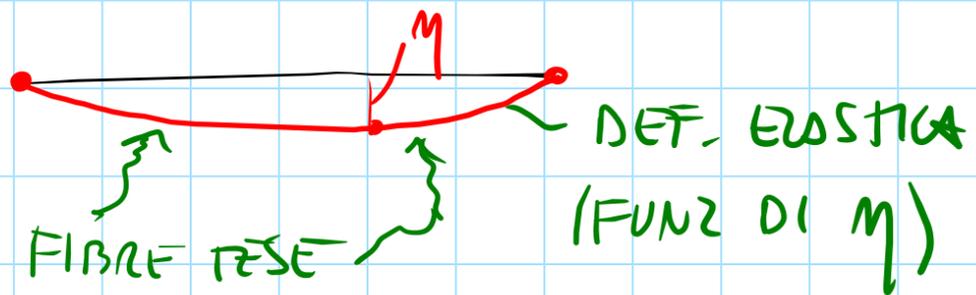
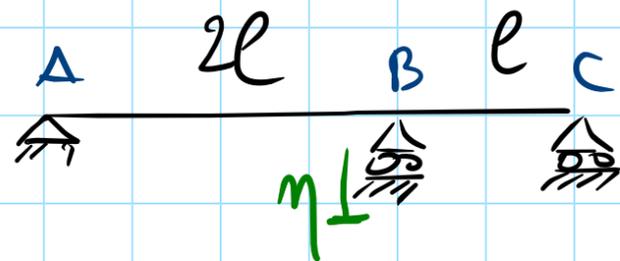
$W_B = \Delta$

$1 \cdot W_B = \int_{STR} M^* \frac{M}{EJ} ds$

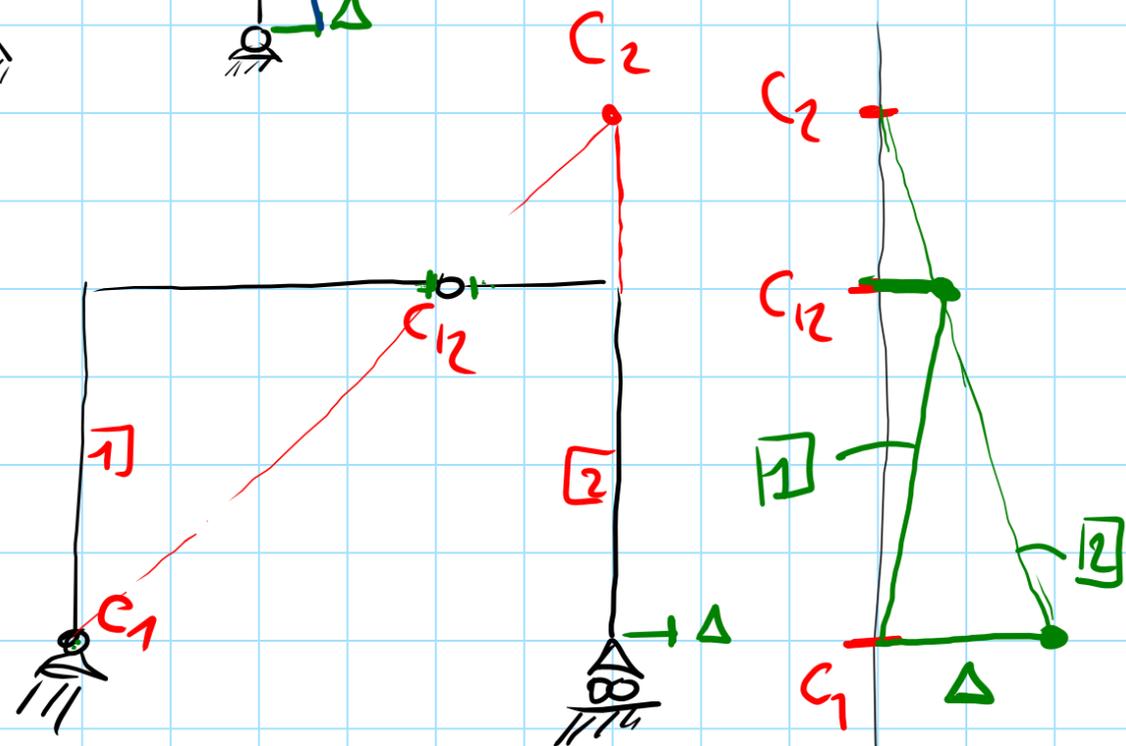
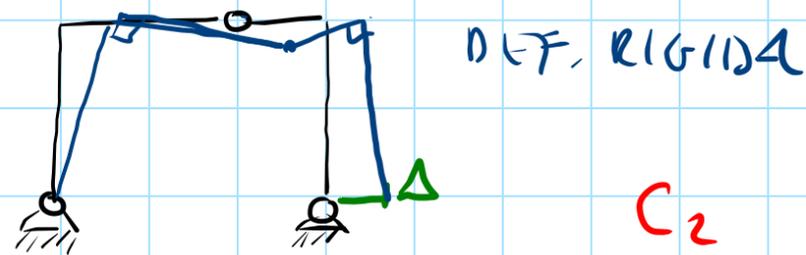
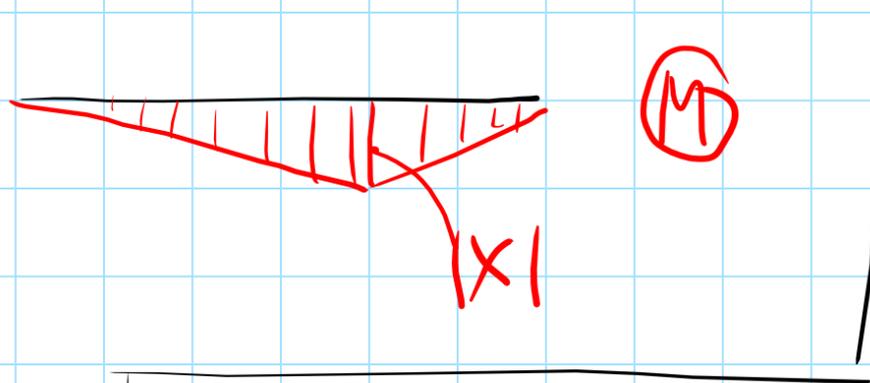


STR INFLESSA
M dipende
da X che
e sue volte dip da Δ





$$-\frac{x \cdot 2l}{3EI} - \frac{q}{2l} = \frac{x \cdot l}{3EI} + \frac{q}{2l} \quad (x < 0)$$

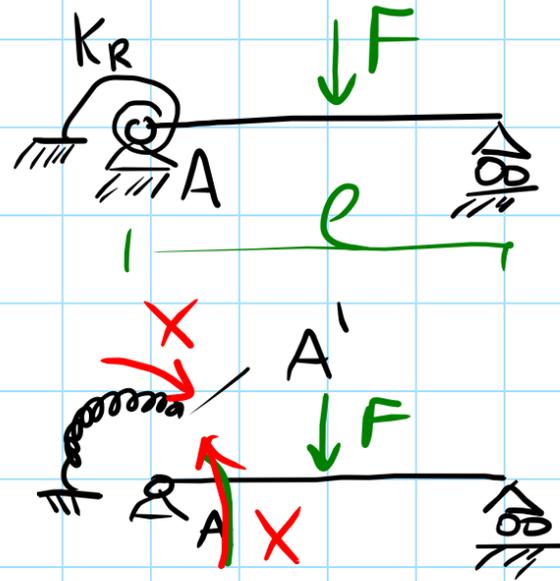


$C_2 \in \text{axe canello}$
 $C_1 \leftrightarrow C_{12} \leftrightarrow C_2$

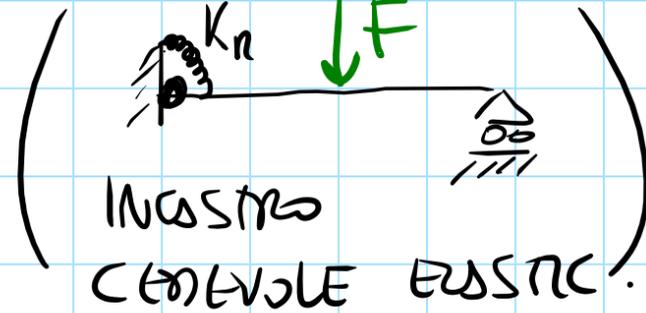
MOLLA ELASTICA

ROTAZIONALE

LEGGE ELASTICA



STRUTTURA IPERST.



$$M = K_R \varphi$$

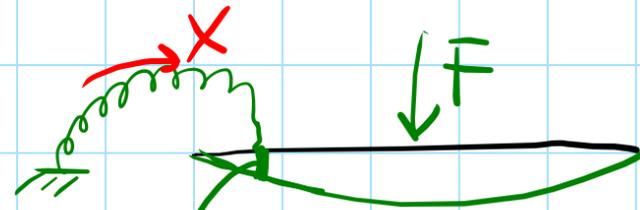
$$[K_R] = [FL]$$

Nm

$$+\downarrow \varphi_A = \varphi_{A'}$$

$$+\frac{x l}{3 E J} - \frac{F l^2}{16 E J} = -\frac{x}{K_R}$$

$$x > 0$$



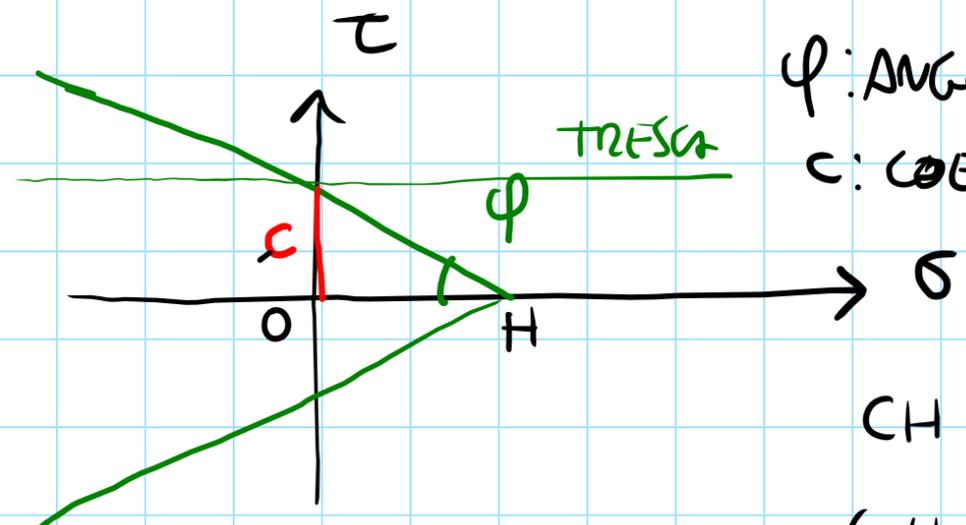
$$\varphi = \frac{x}{K_R} < \frac{F l^2}{16 E J} \quad \left(\begin{array}{l} \text{ANGOLO (N')} \\ \text{ASSENDA DI} \\ \text{MOLLA} \end{array} \right)$$

Se $K_R \rightarrow \infty$:



CRITERIO DI COULOMB-MOHR

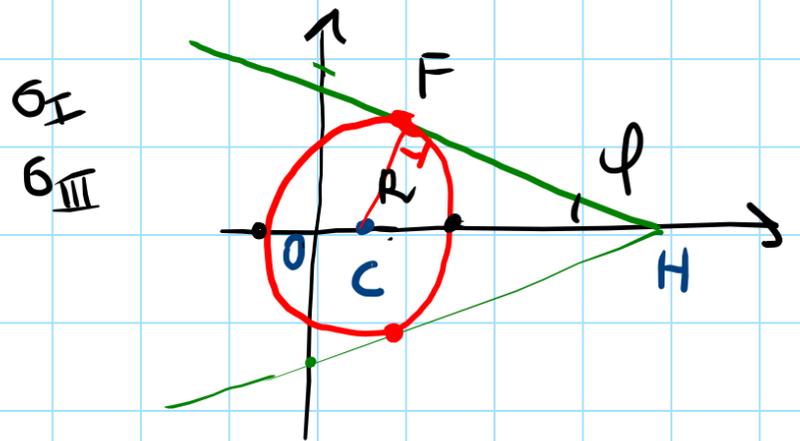
$$[f(\text{param.}) \leq 0]$$



φ : ANGOLO DI ATRIBU INTERNO } COST. DEL
 c: COESIONE } INTERNALE

$$CH \sin \varphi = R$$

$$(OH - OC) \sin \varphi = R, \quad \left(\frac{\tau}{\tan \varphi} - \frac{\sigma_I + \sigma_{III}}{2} \right) \sin \varphi = \frac{\sigma_I - \sigma_{III}}{2}$$



$$(\sigma_I + \sigma_{III}) \sin \varphi + \sigma_I - \sigma_{III} - 2c \cos \varphi = 0$$

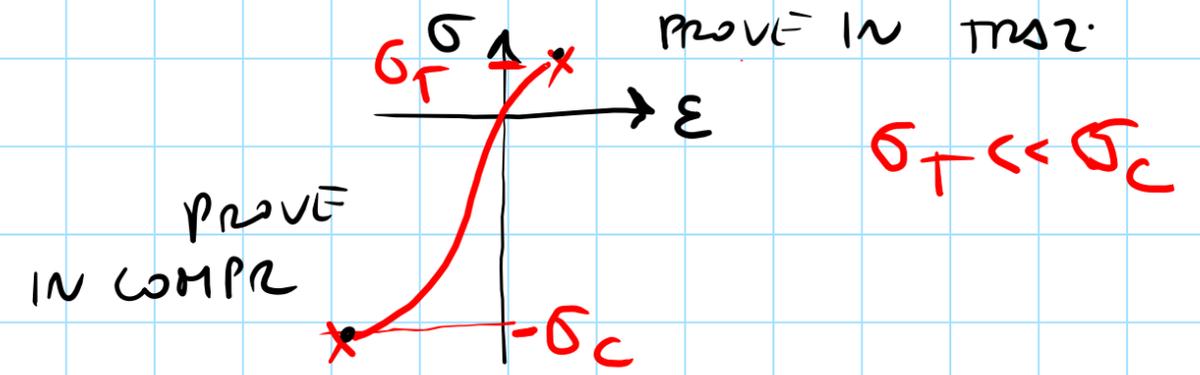
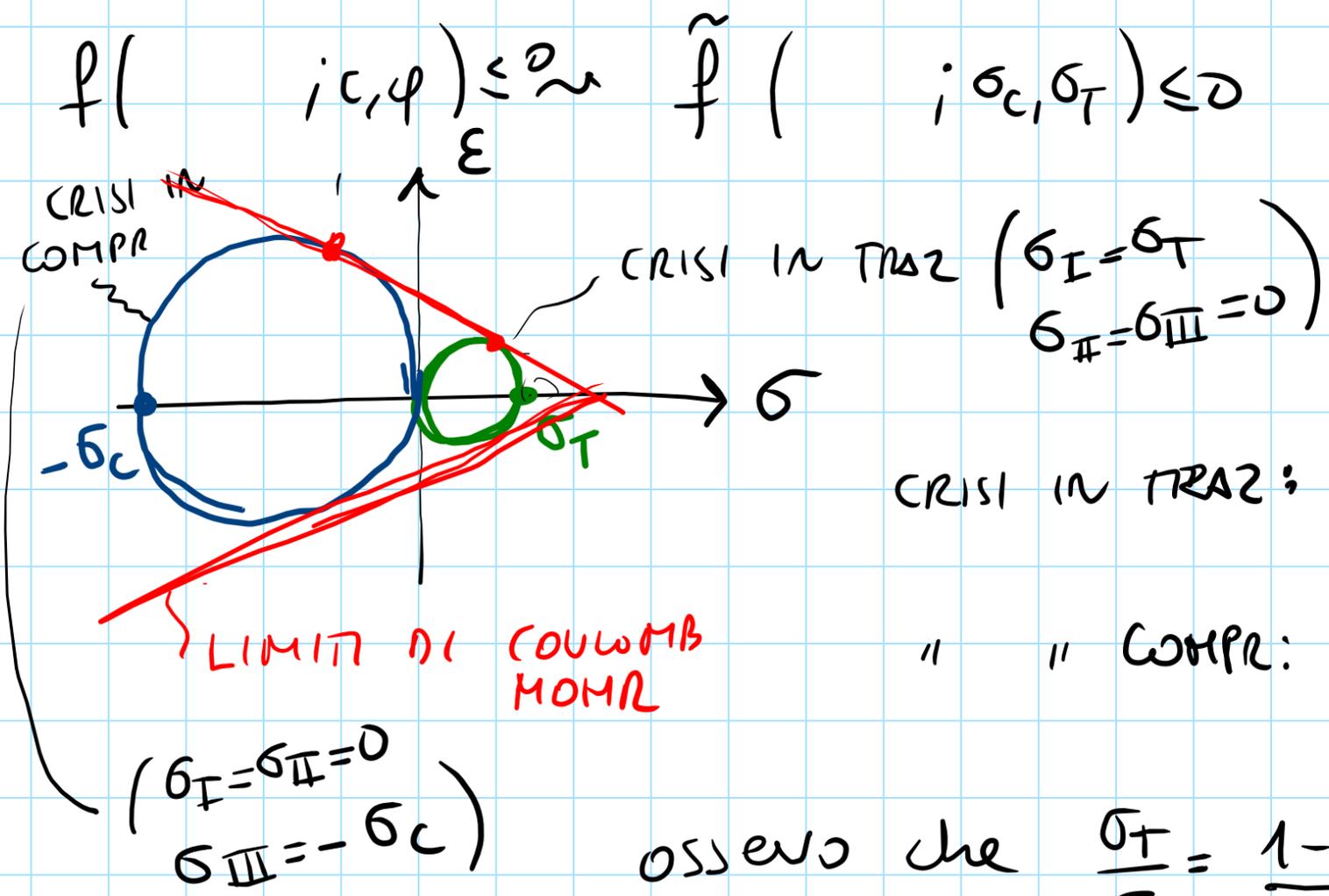
$$\sigma_I (1 + \sin \varphi) - \sigma_{III} (1 - \sin \varphi) - 2c \cos \varphi = 0$$

$$\sigma_I - \sigma_{III} \frac{1 - \sin \varphi}{1 + \sin \varphi} - 2c \frac{\cos \varphi}{1 + \sin \varphi} = 0$$

$$f = \max_{i,j=I,II,III} \left\{ \sigma_i - \sigma_j \frac{1 - \sin \varphi}{1 + \sin \varphi} \right\} - \frac{2c \cos \varphi}{1 + \sin \varphi} \leq 0$$

$$f(\sigma_I, \sigma_{II}, \sigma_{III}; c, \varphi) \leq 0$$

$\varphi \rightarrow 0$ $f \rightarrow$ TRESKA $(c \rightarrow \tau_0 = \sigma_0/2)$



CRISI IN TRAZ: $\sigma_T - \frac{2c \cos \varphi}{1 + \sin \varphi} = 0$; $\sigma_T = \frac{2c \cos \varphi}{1 + \sin \varphi}$
 " " COMP: $0 + \sigma_c \frac{1 - \sin \varphi}{1 + \sin \varphi} - \frac{2c \cos \varphi}{1 + \sin \varphi} = 0$; $\sigma_c = \frac{2c \cos \varphi}{1 - \sin \varphi}$

osserva che $\frac{\sigma_T}{\sigma_c} = \frac{1 - \sin \varphi}{1 + \sin \varphi}$

TRAZIA: $\sigma_c = \sigma_T = \sigma_0$

$\tilde{f} = \max_{i, j = I, II, III} \left\{ \sigma_i - \sigma_j \frac{\sigma_T}{\sigma_c} \right\} - \sigma_T \leq 0$

CENNI ALL'ESISTENZA DEL POTENZIALE ELASTICO COMPLEMENTARE.

$\varphi(\underline{\varepsilon})$: POTENZ. ELASTICO (DENSITA' DI ENERGIA ELASTICA)

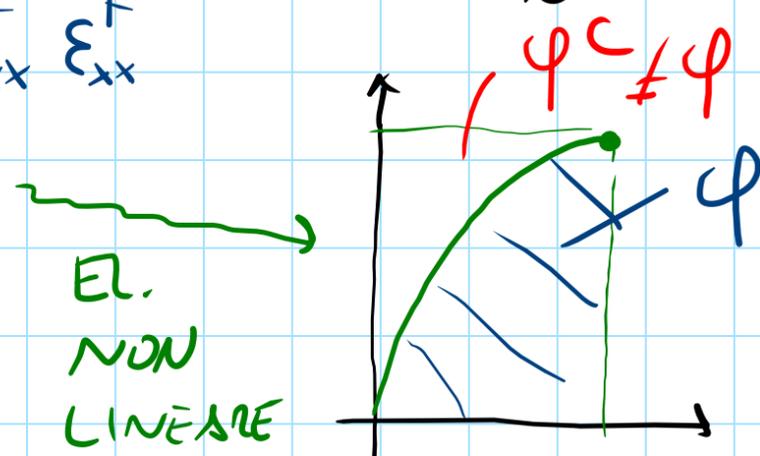
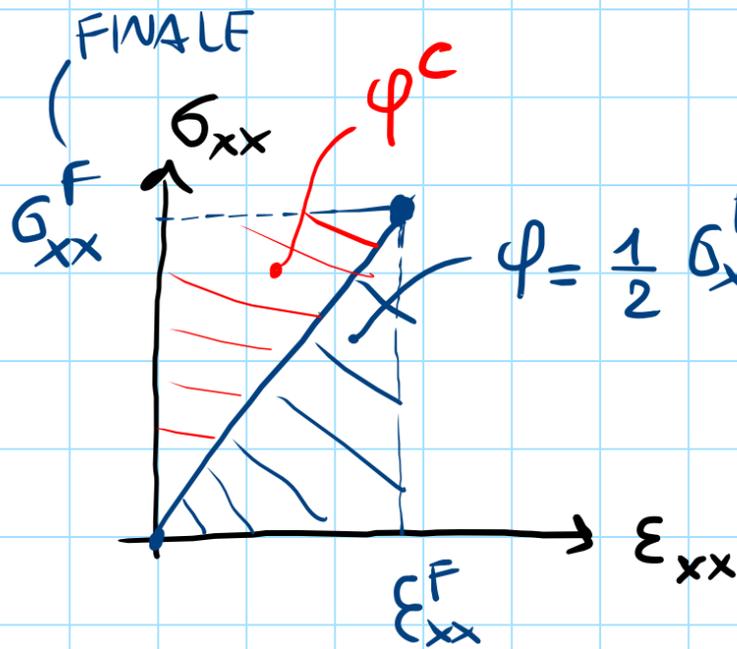
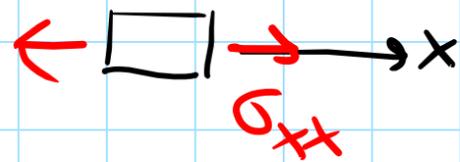
$$\Phi = \int_V \varphi dV$$

EN EL IMMAGAZZ. NEL CORPO

$$\varphi(\underline{\varepsilon}) = \frac{1}{2} \underline{\sigma} \cdot \underline{\varepsilon}$$

$$\sigma_{ij} = \frac{\partial \varphi}{\partial \varepsilon_{ij}}$$

IN TENS. MONO ASS.



$$\varphi^c + \varphi = \sigma_{xx}^F \varepsilon_{xx}^F$$

φ^c : POTENZ ELASTICO COMPL, IN ELASTICITA' LINEARE ASSUME LO STESSO VALORE

NUMERICO DI φ

$$\varphi^c + \varphi = \sigma_{xx}^F \varepsilon_{xx}^F$$

Sulle base delle proprietà $\varphi^c + \varphi = \underline{\sigma} \cdot \underline{\varepsilon}$ si può dimostrare che:

$$\varphi^c(\underline{\sigma}) = \frac{1}{2} \underline{\sigma} \cdot \underline{\sigma}^{-1} \underline{\sigma}, \quad \varepsilon_{ij} = \frac{\partial \varphi^c}{\partial \sigma_{ij}}$$

$$\Phi^c = \int_V \varphi^c dV : \text{EN ELASTICA COMPLEM.}$$