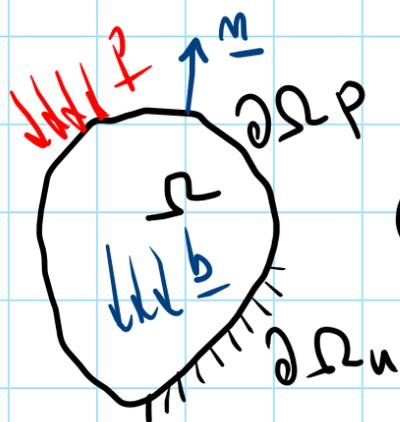


# LINEAR ELASTIC PROBLEM

21/3/25



$$\left\{ \begin{array}{l} \text{div } \underline{\underline{\sigma}} + \underline{\underline{b}} = \underline{\underline{0}} \quad (3) \\ \underline{\underline{\epsilon}} = \frac{1}{2} (\nabla \underline{\underline{u}} + \nabla \underline{\underline{u}}^T) \quad (6) \\ \underline{\underline{\sigma}} = \underline{\underline{C}} \underline{\underline{\epsilon}} \quad (6) \end{array} \right. \quad (15)$$

MATH. ANAL HAS SHOWN THAT, UNDER REGULAR HYPOTHESES, THE PROBLEM HAS A SOLUTION (EXISTENCE); MOREOVER, WITH A SIMPLE ARGUMENT, IT CAN BE SHOWN THAT IT IS UNIQUE (WITH  $\underline{\underline{C}}$  POSITIVE DEFINITE - KIRCHHOFF THEOREM)

## B. CONDITIONS

$$\underline{\underline{\sigma}} \underline{\underline{m}} = \underline{\underline{p}} \quad \text{on } \partial\Omega_p$$

$$\underline{\underline{u}} = \underline{\underline{\bar{u}}} \quad \text{on } \partial\Omega_u \quad (\underline{\underline{\bar{u}}}: \text{ASSIGNED DISPL on } \partial\Omega_u)$$

MOREOVER, EFFECT SUPERPOSITION IS VALID.

## UNKNOWN OF THE PROBLEM

$$\begin{array}{l} \underline{\underline{u}} : (3) \\ \underline{\underline{\sigma}} : (6) \\ \underline{\underline{\sigma}} : (6) \end{array} \quad \left| \quad (15) \right.$$

## DISPLACEMENTS METHOD (FOCUS ON $\underline{\underline{u}}$ )

$$\text{div} \left[ \frac{1}{2} \underline{\underline{C}} (\nabla \underline{\underline{u}} + \nabla \underline{\underline{u}}^T) \right] + \underline{\underline{b}} = \underline{\underline{0}} \quad (\Omega) \quad (3 \text{ EQS IN } 3 \text{ UNKNOWN})$$

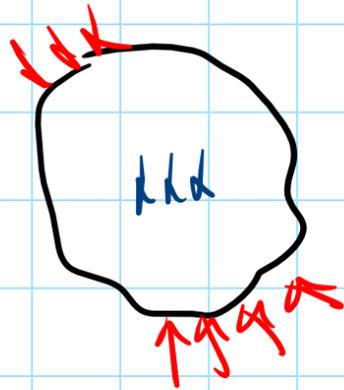
$$\left. \begin{array}{l} \frac{1}{2} \underline{\underline{C}} (\nabla \underline{\underline{u}} + \nabla \underline{\underline{u}}^T) \underline{\underline{m}} = \underline{\underline{p}} \\ \underline{\underline{u}} = \underline{\underline{\bar{u}}} \end{array} \right\} \text{b.c.'s}$$

NAVIER FORMULATION

# STRESS METHOD (BELTRAMI - MICHELL FORMULATION)

$\underline{\sigma}$  AS UNKNOWN (6 COMPONENTS); NOT VERY USEFUL WHEN  $\partial\Omega_u \neq \emptyset$

USEFUL WHEN  $\partial\Omega_u = \emptyset$ :



IN GENERAL, THE SOLUTION OF L.E.P. IS A 'MIXED' PROBLEM WHERE UNKNOWN OF DIFFERENT TYPE ARE IN.

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## WEAK FORMULATIONS OF L.E.P.

STATIONARITY OF TOTAL POTENTIAL ENERGY (DISPLACEMENT METHOD)

COMPLEMENTARY T.P.E. (STRESS METHOD)

FUNCTIONAL OF HELLINGER - REISSNER ( $\underline{u}, \underline{\sigma}$  UNKNOWN: 9 COMPONENTS)

" " HU - WASHIZU (ALL 15 UNKNOWN)

# H.-R. FUNCTIONAL

$$HR(\underline{u}, \underline{\sigma}) = \frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot (\nabla \underline{u} + \nabla \underline{u}^T) dV - \frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot \underline{C}^{-1} \underline{\sigma} dV - \int_{\partial \Omega_p} \underline{p} \cdot \underline{u} dS - \int_{\Omega} \underline{b} \cdot \underline{u} dV - \int_{\partial \Omega_u} \underline{\sigma}_m \cdot (\underline{u} - \bar{\underline{u}}) dS$$

$$\frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot \underline{\varepsilon} = \int_{\Omega} \underline{\sigma} \cdot \underline{\varepsilon} - \frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot \underline{\varepsilon} = \frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot (\nabla \underline{u} + \nabla \underline{u}^T) dV - \frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot \underline{C}^{-1} \underline{\sigma} dV$$

$$\Rightarrow \boxed{\delta_{\underline{u}} HR = 0 \quad ; \quad \delta_{\underline{\sigma}} HR = 0} \quad \text{STATIONARITY OF HR}$$

# HU-WASHIZU FUNCTIONAL (FREE FUNCTIONAL)

$$HW(\underline{u}, \underline{\sigma}, \underline{\varepsilon}) = \frac{1}{2} \int_{\Omega} \underline{C} \underline{\varepsilon} \cdot \underline{\varepsilon} dV - \int_{\partial \Omega_p} \underline{p} \cdot \underline{u} dS - \int_{\Omega} \underline{b} \cdot \underline{u} dV + \int_{\Omega} \underline{\sigma} \cdot \left[ \frac{1}{2} (\nabla \underline{u} + \nabla \underline{u}^T) - \underline{\varepsilon} \right] dV - \int_{\partial \Omega_u} \underline{\sigma}_m \cdot (\underline{u} - \bar{\underline{u}}) dS$$

$$\delta_{\underline{u}} HW = 0$$

$$\delta_{\underline{\sigma}} HW = 0$$

$$\delta_{\underline{\varepsilon}} HW = 0$$

STATIONARITY OF HW

# STATIONARITY OF T.P.E ( $\Pi(\underline{u})$ )

$$\Pi(\underline{u}) = \frac{1}{2} \int_{\Omega} \underline{\sigma} \cdot \underline{\varepsilon} \, dV - \int_{\partial\Omega_p} \underline{p} \cdot \underline{u} \, dS - \int_{\Omega} \underline{b} \cdot \underline{u} \, dV$$

$$\Pi(\underline{u}) = \frac{1}{2} \int \frac{1}{2} \mathbb{C} (\nabla \underline{u} + \nabla \underline{u}^T) \cdot \frac{1}{2} (\nabla \underline{u} + \nabla \underline{u}^T) \, dV - \dots$$

PRINCIPLE OF STATIONARITY OF T.P.E. ( $\delta \Pi^{(1)}(\underline{u}) = 0, \forall \delta \underline{u}$ )

WITHIN THE SET OF DISPL. FIELDS  $\underline{u}$  KINEMATICALLY ADMISSIBLE\*, THE ONE THAT SOLVE THE L.E.P. CORRESPONDS TO THE CONDITION

$$\delta \Pi^{(1)}(\underline{u}) = 0, \forall \delta \underline{u} \quad (\Leftrightarrow \text{EQUILIBRIUM})$$

SKETCH OF PROOF:  $\Pi(\underline{u} + \delta \underline{u}) = \Pi(\underline{u}) + \delta \Pi = \frac{1}{2} \int_{\Omega} \mathbb{C} \underline{\varepsilon} \cdot \underline{\varepsilon} - \underline{b} \cdot \underline{u} - \int_{\partial\Omega_p} \underline{p} \cdot \underline{u} + \int_{\Omega} \mathbb{C} \underline{\varepsilon} \cdot \delta \underline{\varepsilon} - \int_{\Omega} \underline{b} \cdot \delta \underline{u} -$

$\delta \Pi^{(1)}$  IS AN EXPRESSION OF THE THEOREM OF VIRTUAL WORK, AND BY IMPOSING  $\delta \Pi^{(1)} = 0$  WE CAN SHOW THAT  $\{\underline{\sigma}, \underline{p}, \underline{b}\}$  IS IN EQUILIBRIUM

$\delta \Pi^{(1)} > 0 \Leftrightarrow \mathbb{C}$  IS POSITIVE DEFINITE

\*:  $\underline{u}(P) = \bar{\underline{u}}$  on  $\partial\Omega_u$

# DISCRETIZATION OF THE L.E.P. BASED ON STATIONARITY OF T.P.E. (BASED ON DISPL. METHOD)

FOR AN ELEMENT (e)

$$\tilde{\underline{u}}_e(x, y, z) = \begin{bmatrix} \sum_{k=1}^m \bar{\Phi}_k(x, y, z) u_{kx}^e \\ \dots \\ u_{ky}^e \\ \dots \\ u_{kz}^e \end{bmatrix} = \tilde{\underline{N}} \underline{D}_e$$

(3x3m) (3m)

APPROX DISPL FIELD (3)

$$\tilde{\underline{N}} = \begin{bmatrix} \bar{\Phi}_1 & 0 & \bar{\Phi}_2 & 0 \\ 0 & \bar{\Phi}_1 & 0 & \bar{\Phi}_2 \\ \dots & \dots & \dots & \dots \\ 0 & \bar{\Phi}_1 & 0 & \bar{\Phi}_2 \end{bmatrix}$$

(3x3m)

$$\underline{D}_e = \begin{bmatrix} u_{1x}^e \\ u_{1y}^e \\ \vdots \\ u_{mz}^e \end{bmatrix} \quad (3m)$$

VECTOR OF NODAL DISPLACEMENTS

$\bar{\Phi}_1$ : SHAPE FUNCTIONS

$$\underline{\epsilon} = \begin{bmatrix} u_{x,x} & \frac{1}{2}(u_{x,y} + u_{y,x}) \\ & u_{y,y} \end{bmatrix}$$

NOW WE HAVE A GOAL:  $\tilde{\underline{\epsilon}}(x, y, z) = \tilde{\underline{B}} \underline{D}_e$

(6) (6x3m) (3m)

← COMPATIBILITY MATRIX (?)

$$\underline{\epsilon} = [\underline{\sigma}] \underline{u}$$

(6x3)

$$\tilde{\underline{B}} = [\underline{\sigma}] \tilde{\underline{N}}$$

(6x3) (3x3m)

OK!

$$\underline{\sigma}(x, y, z) = \underline{C} \underline{\epsilon}$$

(6) (6x6) (6)

(USING VOIGT NOTATION)

$$[\underline{\sigma}] = \begin{bmatrix} \cdot_{ix} & 0 & 0 \\ 0 & \cdot_{iy} & 0 \\ 0 & 0 & \cdot_{iz} \\ 0 & \frac{1}{2}\cdot_{iz} & \frac{1}{2}\cdot_{iy} \\ \frac{1}{2}\cdot_{iz} & 0 & \frac{1}{2}\cdot_{ix} \\ \frac{1}{2}\cdot_{iy} & \frac{1}{2}\cdot_{ix} & 0 \end{bmatrix}$$