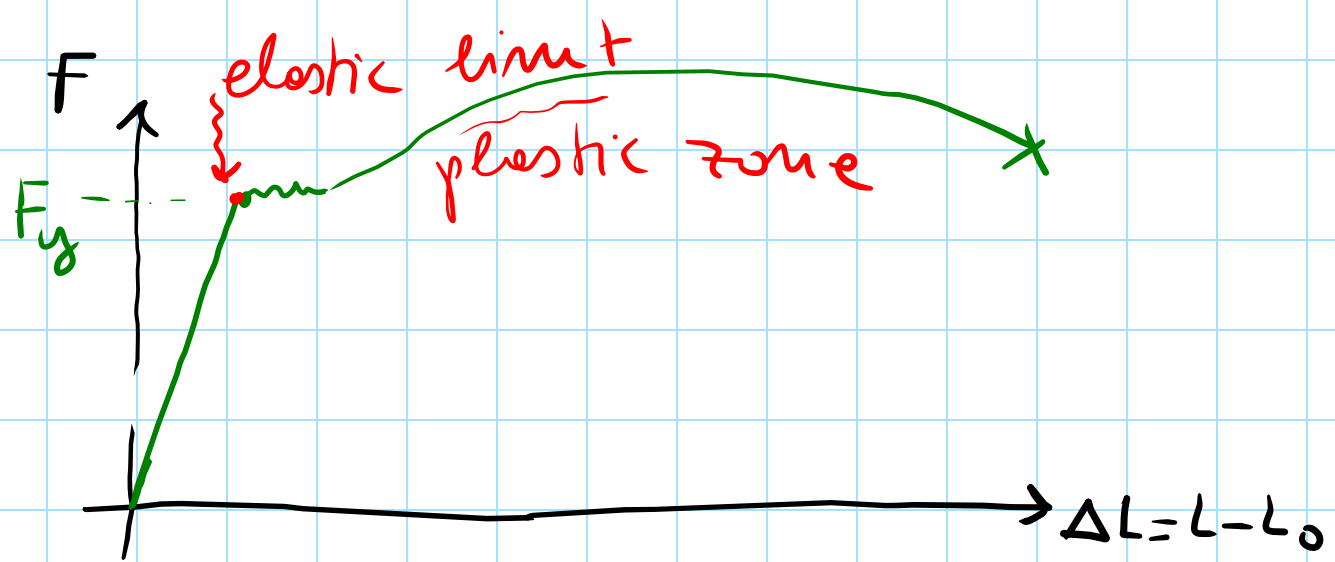
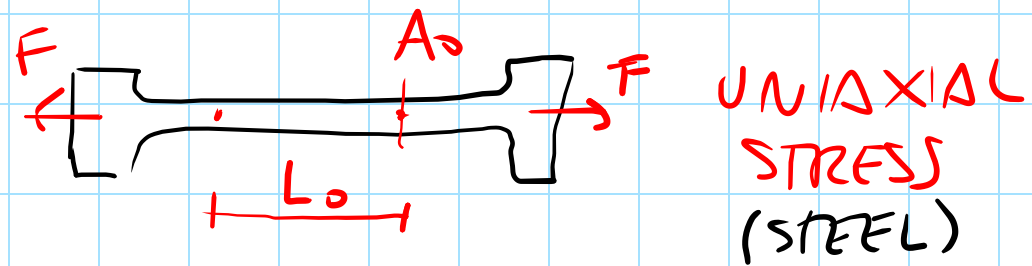
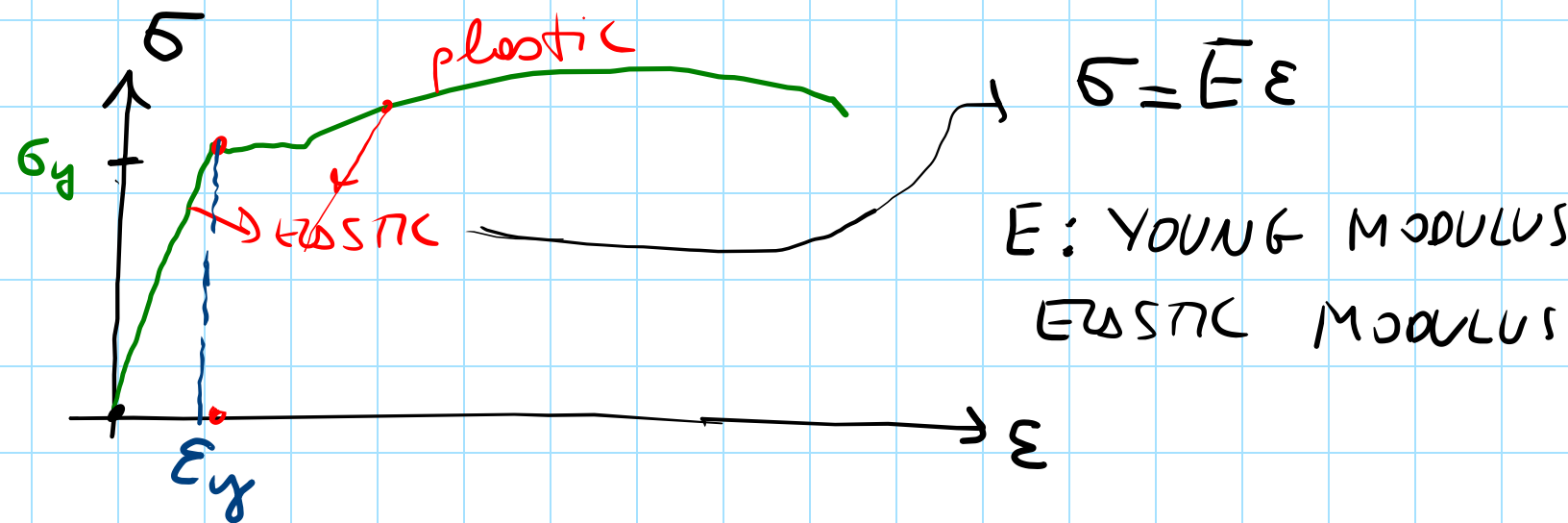
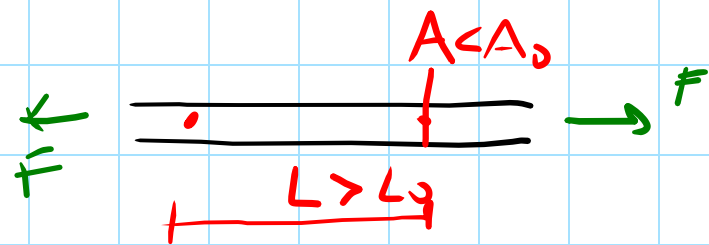


KINEMATICS : STRAIN, DEFORMATION

DEFORMAZIONE



THE SPECIMEN ELONGATES



LONGITUDINAL STRAIN [-]

$$\sigma = \frac{F}{A_0}; \quad \epsilon = \frac{\Delta L}{L_0} = \frac{L - L_0}{L_0}$$

UNIAXIAL STRESS

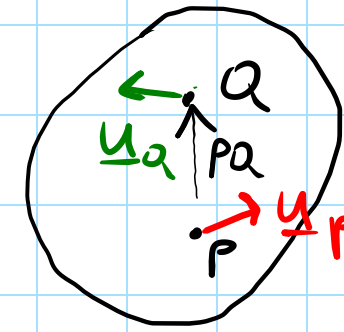
STEEL: $\sigma_y = 300 \text{ MPa}$
 $E \approx 200 \text{ GPa}$
 $\epsilon_y ?$

$$\epsilon_y \approx \frac{300}{200 \cdot 10^3} = 1.5 \cdot 10^{-3} = 1.5 \text{ ‰}$$

E: STEEL : 210 GPa , CONCRETE : 20 GPa
 ALUMINIUM : 70 GPa

MORE ABOUT STRAIN (3D ANALYSIS)

IMPORTANT: RIGID-BODY MOTION OF A BODY
 => ABSENCE OF STRAIN

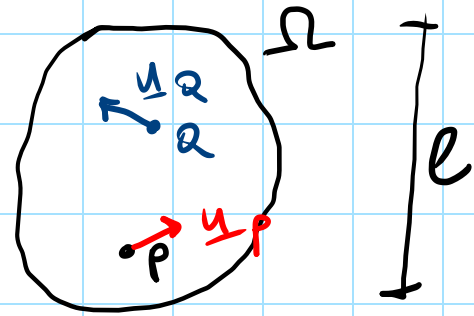


$$u_Q = u_P + \tilde{W} PQ$$

SKEW-SYMMETRIC

$$\tilde{W} = -\tilde{W}^T$$

HYPOTHESES OF ANALYSIS OF STRAIN



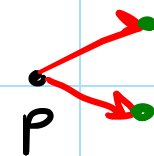
- SMALL DISPLACEMENTS, $|u_P| \ll l, \forall P \in \Omega$

- " DISPLACEMENT GRADIENT, $|\nabla u_P| \ll 1, \forall P \in \Omega$

- FUNCTION $u_P(\forall P)$ IS 1 TO 1:

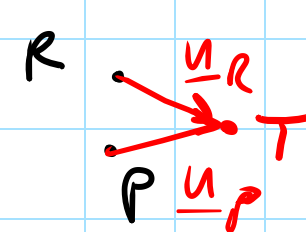


NEIGHBOURHOOD OF P



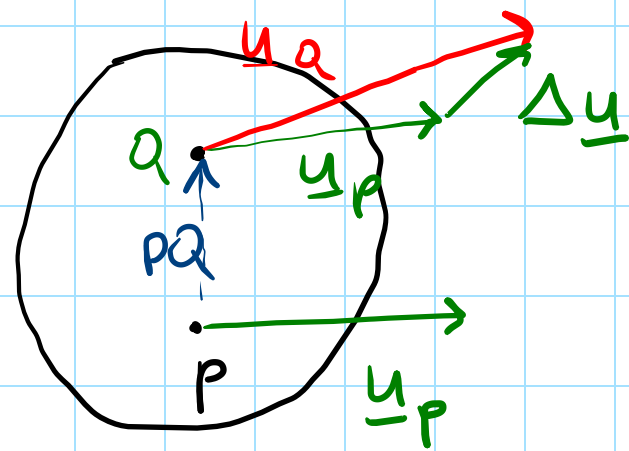
(NO)

CREATION OF A CRACK



(NO)

ANALYSIS OF STRAIN AT A POINT $P \in \Omega$



$$\underline{u}_Q = \underline{u}_P + \Delta \underline{u} \quad \rightarrow \text{TAYLOR EXPANS.}$$

$$\underline{u}_Q = \underline{u}_P + \underbrace{\nabla \underline{u}(P)}_{\text{TENSOR (DISPL.-GRADIENT)}} \underbrace{PQ}_{\text{VECTOR}}$$

$$\underline{u}_Q \approx \underline{u}_P + \nabla \underline{u}(P) PQ = \underline{u}_P + \left(\underbrace{\tilde{\underline{\varepsilon}}}_{\text{SYMM.}} + \underbrace{\tilde{\underline{w}}}_{\text{SKEW-SYMM}} \right)_P PQ = \underline{u}_P + \underbrace{\tilde{\underline{\varepsilon}} PQ}_{\text{STRAIN MOTION}} + \underbrace{\tilde{\underline{w}} PQ}_{\text{RIGID-BODY MOTION}}$$

$$\tilde{\underline{\varepsilon}} = \frac{1}{2} (\nabla \underline{u} + \nabla \underline{u}^T) \quad (\tilde{\underline{\varepsilon}} = \tilde{\underline{\varepsilon}}^T)$$

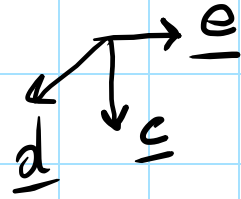
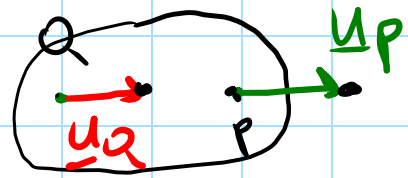
$$\tilde{\underline{w}} = \frac{1}{2} (\nabla \underline{u} - \nabla \underline{u}^T) \quad (\tilde{\underline{w}} = -\tilde{\underline{w}}^T)$$

$\tilde{\underline{\varepsilon}}$: STRAIN TENSOR (= 0 FOR RIGID-BODY MOTION!)

$$\rightarrow \varepsilon_{ij} = \frac{1}{2} (u_{i,j} + u_{j,i}) \quad \begin{matrix} \varepsilon_{11} = u_{1,1} \\ \varepsilon_{22} = u_{2,2} \end{matrix}, \quad \varepsilon_{12} = \frac{1}{2} (u_{1,2} + u_{2,1})$$

MEANING OF THE COMPONENTS OF $\underline{\underline{\epsilon}}$

- DIAGONAL OF $\underline{\underline{\epsilon}}$



$$u_p = 0.5 \underline{e}$$

$$u_q = 0.2 \underline{e}$$

$$PQ = -20 \underline{e}$$

$$\underline{\underline{\epsilon}} = \epsilon_{11} \underline{e} \otimes \underline{e} + \epsilon_{12} \underline{e} \otimes \underline{c} + \epsilon_{13} \underline{e} \otimes \underline{d} + \dots$$

$$\textcircled{*} \quad u_q - u_p = \underline{\underline{\epsilon}} PQ$$

$$\underline{v} = v_1 \underline{e} + v_2 \underline{c} + v_3 \underline{d}$$

$\{\underline{e}, \underline{c}, \underline{d}\}$ ORTHONORMAL BASIS

$$\textcircled{*} : 0.2 \underline{e} - 0.5 \underline{e} = \underline{\underline{\epsilon}} \underline{e} \quad (-20)$$

$$(0.2 - 0.5) \underline{e} = \epsilon_{11} (-20) \underline{e}$$

$$\epsilon_{11} = \frac{-0.3}{-20} = +0.015$$

$$\underline{\underline{\epsilon}} \underline{e} = \epsilon_{11} \underline{e}$$

ALTERNATIVE

$$\epsilon_e = \frac{\Delta L}{L_0} = \frac{20.3 - 20}{20} = \frac{0.3}{20} = 0.015 \quad (\text{ELONGATION})$$

$$\begin{bmatrix} 1 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

ELEMENTS ON THE DIAGONAL OF $\underline{\underline{\epsilon}}$:

LONGITUDINAL STRAINS

$\epsilon_{11} > 0$: ELONGATION

$\epsilon_{11} < 0$: CONTRACTION

- OFF-DIAGONAL TERMS OF $\underline{\underline{\epsilon}}$

EX: $\begin{cases} u_1(x_1, x_2, x_3) = \frac{\gamma_{12}}{2} x_2 \\ u_2(x_1, x_2, x_3) = \frac{\gamma_{12}}{2} x_1 \\ u_3(x_1, x_2, x_3) = 0 \end{cases}$ ($\gamma_{12} < 1, \gamma_{12} > 0$)

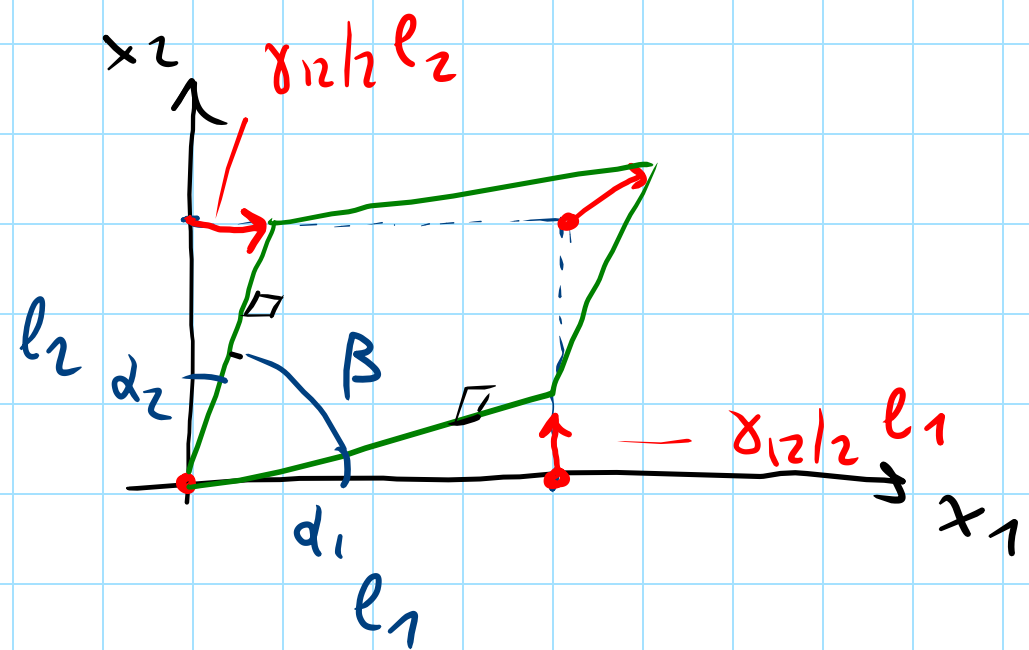
PURE SHEAR DEFORMATION

$\epsilon_{ij} = \frac{1}{2}(u_{i,j} + u_{j,i})$

$$[\underline{\underline{\epsilon}}] = \begin{bmatrix} 0 & \gamma_{12}/2 & 0 \\ \gamma_{12}/2 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix} \neq f(x_1, x_2, x_3)$$

HOMOGENEOUS STRAIN

$$[\underline{\underline{w}}] = [\underline{\underline{0}}]$$



γ_{12} GOVERNS THE CHANGE IN ANGLES OF AN INITIAL PARALLELEPIPED SHAPE IN THE NEIGHBOURHOOD OF THE POINT P.

$$\frac{\pi}{2} = \beta + d_1 + d_2 \rightarrow \frac{\pi}{2} = \beta + 2d \rightarrow \frac{\pi}{2} = \beta + \gamma_{12}$$

$$\gamma_{12} = \frac{\pi}{2} - \beta$$

γ_{12} : CHANGE IN SHAPE (SHEAR STRAIN) (SCORRIMENTO)

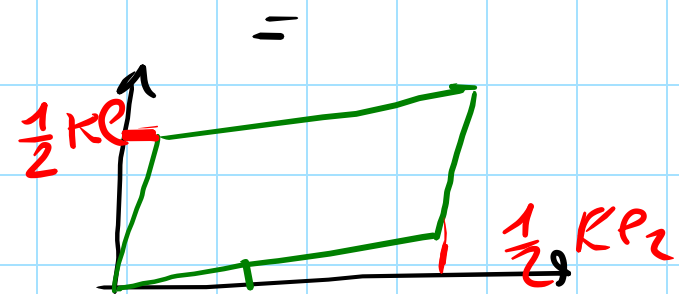
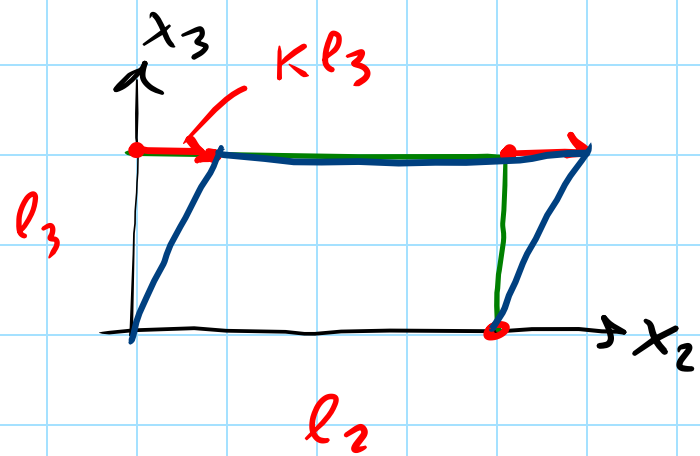
$$d_1 = d_2 = \frac{\gamma_{12}}{2}$$

EX $\begin{cases} u_1 = 0.005 x_2 \\ u_2 = 0.005 x_1 \end{cases} \rightarrow \gamma_{12} = 0.01, \beta = \frac{\pi}{2} - 0.01 \Rightarrow \beta = 89.43^\circ$

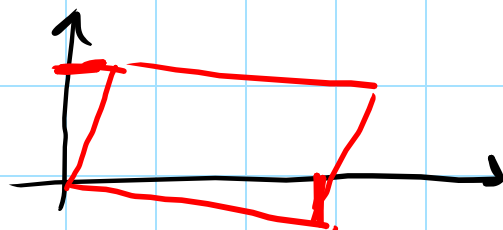
EX: SIMPLE SHEAR

($0 < k \ll 1$)

$$\begin{cases} u_1 = 0 \\ u_2 = kx_3 \\ u_3 = 0 \end{cases}$$



+



$$[\tilde{\epsilon}] = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & \frac{1}{2}k \\ 0 & \frac{1}{2}k & 0 \end{bmatrix}$$

$$[\tilde{w}] = \begin{bmatrix} 0 & 0 & 0 \\ 0 & 0 & \frac{1}{2}k \\ 0 & -\frac{1}{2}k & 0 \end{bmatrix}$$

RIGID BODY!

$$u_q - u_p = \underbrace{\tilde{\epsilon}_{PQ}}_{(1)} + \underbrace{w_{PQ}}_{(2)}$$

THE SIMPLE SHEAR DEFORMATION IS COMPOSED OF A "STRAIN" PART AND A "RIGID-BODY" PART.

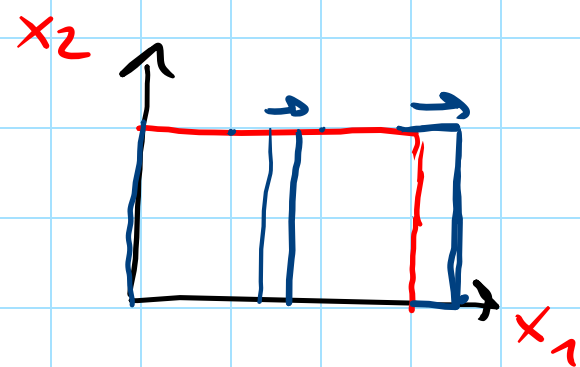
IT REPRESENTS A GENERIC DEFORMATION

(1) $\tilde{\epsilon}_{PQ}$ MAP.

(2) w_{PQ}

OTHER RELEVANT DEFORMATION / STRAIN STATES

- SIMPLE EXTENSION / ELONGATION



$$[\underline{\underline{\varepsilon}}] = \begin{bmatrix} \varepsilon_{11} & 0 & 0 \\ 0 & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

- PURE SHEAR

$$[\underline{\underline{\varepsilon}}] = \begin{bmatrix} 0 & * & 0 \\ * & 0 & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

* : $\neq 0$

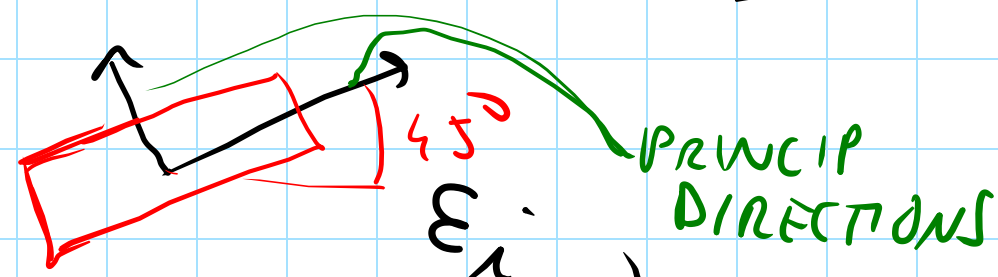
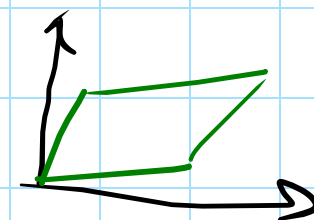
- PLANE STRAIN :

$$[\underline{\underline{\varepsilon}}] = \begin{bmatrix} * & * & 0 \\ * & * & 0 \\ 0 & 0 & 0 \end{bmatrix}$$

(IN x_1-x_2)

(DEFORM. PLANA)

$\underline{\underline{\varepsilon}}^x$: PURE SHEAR



WE DO NOT TALK ABOUT "PRINCIPAL STRAINS" (EIGENVALUES OF $\underline{\underline{\varepsilon}}$)

AND "PRINCIPAL DIRECTIONS OF STRAIN" (EIGENVECTORS OF $\underline{\underline{\varepsilon}}$) \underline{u}_i

HOWEVER, DUE TO $\underline{\underline{\varepsilon}} = \underline{\underline{\varepsilon}}^T \Rightarrow \varepsilon_i$ and \underline{u}_i ARE MUTUALLY ORTHOGONAL $\in \mathbb{R}$