

**Enrico Nobile**

*Dipartimento di Ingegneria e Architettura  
Università degli Studi di Trieste*

*Computational Methods for Fluid Dynamics and Heat Transfer*

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## Description of the problem

In the fully developed<sup>1</sup> laminar channel flow for straight pipes of constant cross-section, constraints from the continuity equation and the no-slip condition, require the existence of only the streamwise velocity component  $u = u(y, z)$ , while the other two velocity components vanish, i.e.  $v = w = 0$ .

In this situation, we are left with only the  $x$ -momentum equation, which reduces to the following Poisson equation:

$$\frac{\partial^2 u}{\partial y^2} + \frac{\partial^2 u}{\partial z^2} = \frac{1}{\mu} \frac{dp}{dx} \quad (1)$$

where, in eq. (1),  $\mu$  is the dynamic viscosity of the fluid and  $dp/dx$  is the streamwise pressure gradient (please note that, in this situation,  $p = p(x)$ ). A schematic diagram of a fully developed laminar channel flow is shown in figure 1.

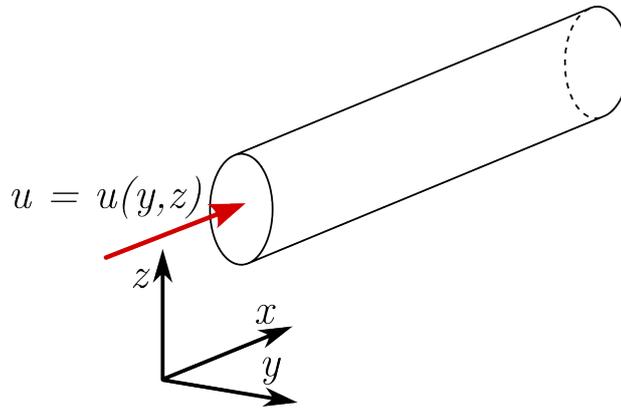


Figure 1: Fully developed laminar channel flow in a straight pipe.

## Fluid flow parameters

For these type of problems, the fluid flow characteristics are expressed in terms of certain hydrodynamic parameters which are define here.

**Hydraulic diameter** The *Hydraulic Diameter*  $D_h$ , for a pipe of generic cross-section, is defined as

$$D_h = \frac{4A}{P} \quad (2)$$

where  $A$  is the cross-section area and  $P$  is the wetted perimeter.

<sup>1</sup>We recall that with *fully developed laminar flow* we mean that region where both the velocity components  $v$  and  $w$  lying in the cross-section plane of the pipe *and* the gradient of the axial velocity component  $\partial u/\partial x$  are everywhere zero.

**Reynolds number** The *Reynolds number* is defined as

$$Re = \frac{\rho D_h U}{\mu} \quad (3)$$

where  $\rho$  is the density and  $U$  is the bulk, i.e. mean, streamwise velocity value.

**Fanning friction factor** The *Fanning friction factor*<sup>2</sup>  $f$  is defined as the ratio of the *average* wall shear stress  $\bar{\tau}_w$  to the flow kinetic energy per unit volume  $\rho U^2/2$

$$f = \frac{\bar{\tau}_w}{\rho U^2/2} \quad (4)$$

Since for a single phase, fully developed flow in a pipe, the shear stress at the fluid-solid boundary is balanced by the pressure drop, a one-dimensional force balance can be written as:

$$A \Delta p = P L \bar{\tau}_w$$

where  $L$  is the pipe length.

Therefore, equation (4) can be written also as

$$f = \frac{(dp/dx) A}{\rho U^2/2 P} \quad (5)$$

## Proposed problems

Develop, in MATLAB or other language of choice, a Finite Volume (FV) program/script that computes the flow field in a straight duct of *rectangular* cross-section, assuming a steady laminar flow of a Newtonian fluid of constant thermophysical properties.

Consider the two following cases:

1. Square channel with  $L_y = L_z = 25$  [mm].  
 $dp/dx = -1.0$  [Pa/m].  
 $\rho = 997$  [kg/m<sup>3</sup>].  
 $\mu = 8.9 \times 10^{-4}$  [kg/m s].
2. Rectangular channel with  $L_y = 10$  [mm] and  $L_z = 25$  [mm].  
 $dp/dx = -1.0$  [Pa/m].  
 $\rho = 997$  [kg/m<sup>3</sup>].  
 $\mu = 8.9 \times 10^{-4}$  [kg/m s].

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<sup>2</sup>This quantity is not to be confused with the *Moody (or Darcy) friction factor*, which is a dimensionless parameter defined as  $f_D = -(dp/dx)D_h/\rho U^2/2$ .

For circular pipes the relation between the two parameters is

$$f = \frac{f_D}{4}$$

Using an *adequate* number of cells, for both cases:

- a. Plot a *contour* of the velocity field.
- b. Compute the *Fanning friction factor* and compare it with the following approximation

$$f \text{ Re} = 24 (1 - 1.3553\alpha + 1.9467\alpha^2 - 1.7012\alpha^3 + 0.9564\alpha^4 - 0.2537\alpha^5) \quad (6)$$

where

$$\alpha = \min(L_z/L_y, L_y/L_z)$$

The equation (6) closely approximates, within +0.05%, the following exact analytical expression for the fully developed *Fanning friction factor* for ducts of rectangular cross-section

$$f \text{ Re} = \frac{24}{\left(1 + \frac{1}{\alpha}\right)^2 \left(1 - \frac{192}{\pi^4 \alpha} \sum_{n=1,3,\dots}^{\infty} \frac{\tanh(n\pi\alpha/2)}{n^5}\right)} \quad (7)$$

#### TIP

After the (discrete) solution of equation (1), the *Fanning friction factor* can be computed using either eq. (4), once the *wall-averaged* shear stress and mean velocity  $U$  have been computed, or eq. (5) if the mean velocity  $U$  has been obtained.

## References

- [1] F. P. Incropera, D. P. Dewitt, T. L. Bergman, A. S. Lavine, *Fundamentals of Heat and Mass Transfer*, 6th Ed., Wiley, (2007).
- [2] R.K. Shah, A.L. London, *Laminar Flow Forced Convection in Ducts*, Elsevier Inc., (1978).