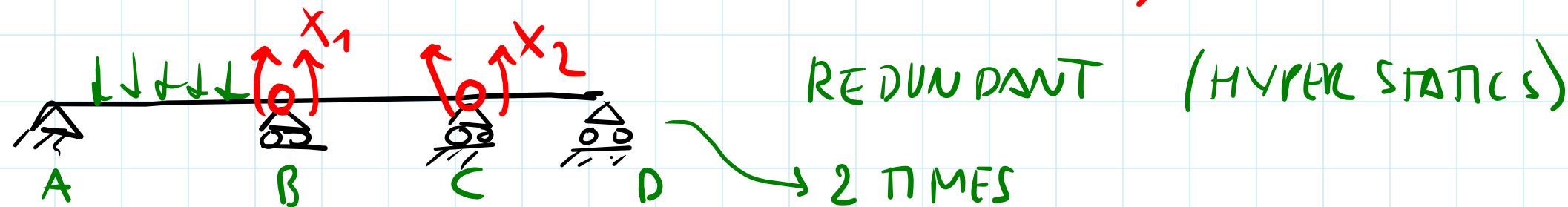


METHODS OF SOLUTION OF ELASTIC STRUCTURES (REVIEW)

CSM 24/9/26

1°: METHOD OF FORCES (COMPATIBILITY ---)



TO SOLVE (X_1, X_2 ARE THE UNKNOWN!) $\Rightarrow$ COMPATIBILITY EQS: $\left. \begin{array}{l} \varphi_{BA} = \varphi_{BC} \\ \varphi_{CB} = \varphi_{CD} \end{array} \right\}$

LINEAR SYST.

$$\left[\underset{\substack{\text{FLEXIBILITY} \\ \text{MATRIX}}}{\zeta} \right] \left[\underset{\substack{\text{UNKNOWN}}}{\underline{X}} \right] = \left[\underset{\substack{\text{KNOWN TERMS} \\ \text{(DISPLAC., ROTATION)}}}{\underline{U}} \right]$$

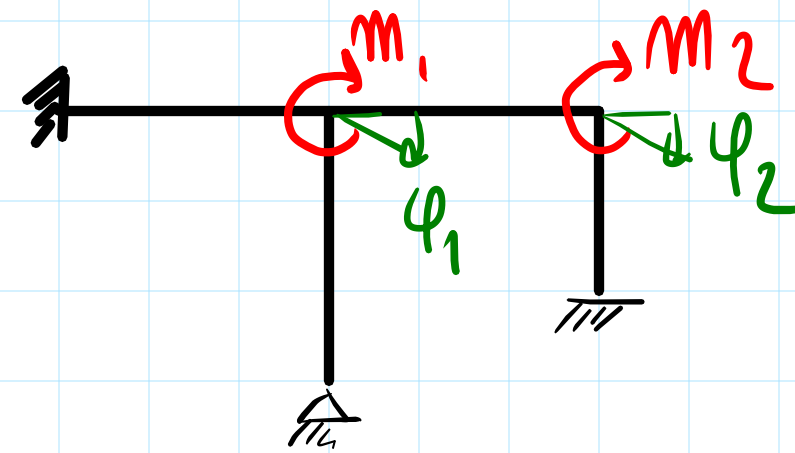
LINEAR SYSTEM

$$\underline{X} = \zeta^{-1} \underline{U}$$

2°: DISPLACEMENT METHOD

$$\begin{bmatrix} \tilde{K} \end{bmatrix} \begin{bmatrix} \underline{U} \end{bmatrix} = \begin{bmatrix} \underline{F} \end{bmatrix} \quad \text{SCHEMA II}$$

STIFFNESS MATRIX DISPLACEMENTS (UNKNOWN) (φ_1, φ_2) NODAL FORCES (m_1, m_2)

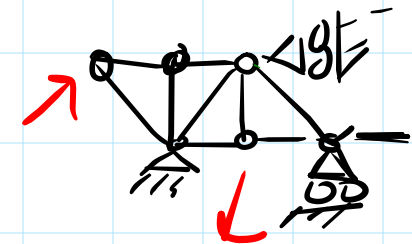


$$\underline{U} = \tilde{K}^{-1} \underline{F}$$

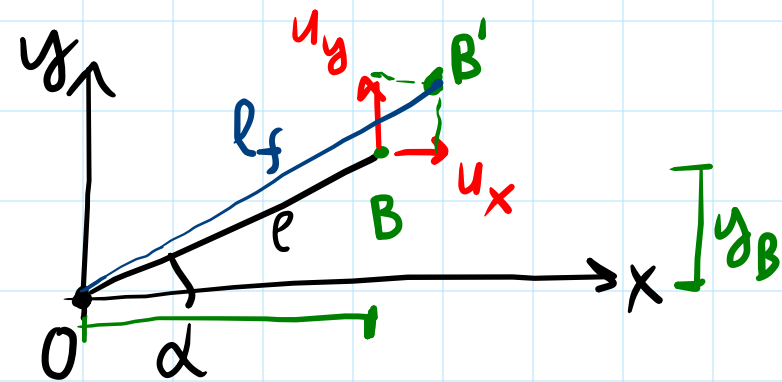
FEMs FORMULATED FROM STATIONARITY OF THE TOTAL POTENTIAL ENERGY LEAD TO A LINEAR SYSTEM THAT IS EXACTLY

$$\boxed{\tilde{K} \underline{U} = \underline{F}}$$

DISPLACEMENT METHOD FOR PLANE TRUSS STRUCTURES



KINEMATICS OF A BAR IN THE PLANE



$$l = \sqrt{x_B^2 + y_B^2}, \quad l_f = \sqrt{(x_B + u_x)^2 + (y_B + u_y)^2} = l_f(u_x, u_y)$$

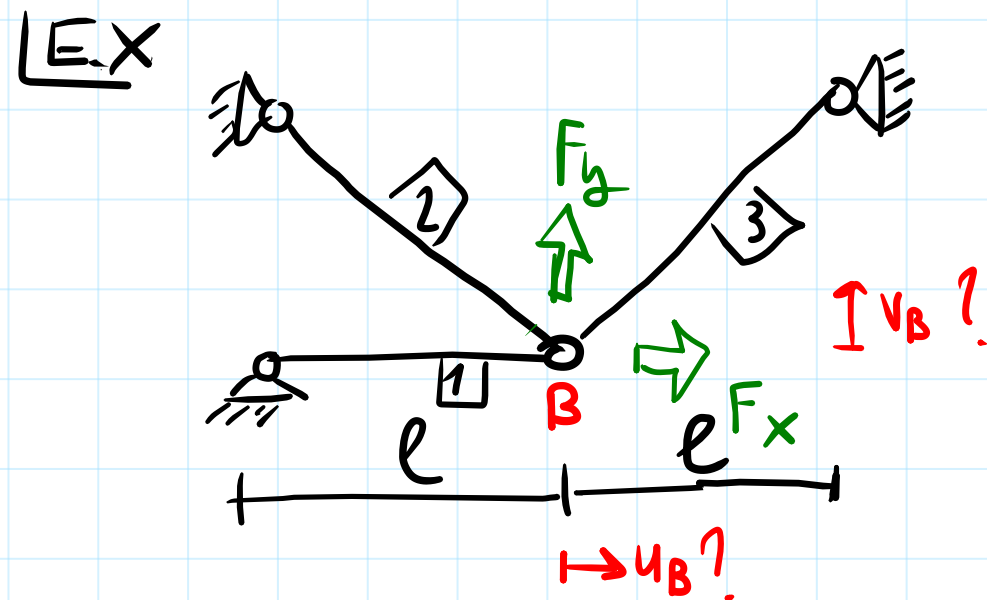
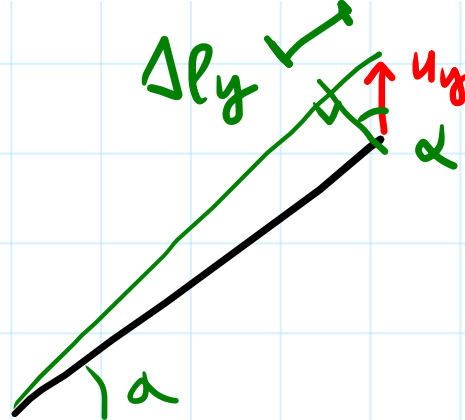
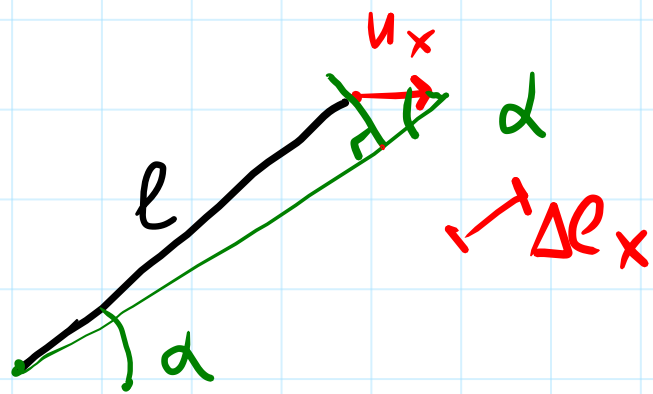
GOAL: LINEARIZE $l_f(u_x, u_y)$

$$l_f = l_f(0, 0) + \frac{\partial l_f}{\partial u_x} \bigg|_{(0,0)} u_x + \frac{\partial l_f}{\partial u_y} \bigg|_{(0,0)} u_y + O(\sqrt{u_x^2 + u_y^2})$$

$$= l + \left[\frac{1}{\sqrt{\dots}} (x_B + u_x) \right]_{(0,0)} u_x + \left[\frac{1}{\sqrt{\dots}} (y_B + u_y) \right]_{(0,0)} u_y + \dots$$

$$l_f \approx l + \underbrace{\frac{1}{l} x_B}_{\cos \alpha} u_x + \underbrace{\frac{1}{l} y_B}_{\sin \alpha} u_y \rightarrow l_f = l + \underbrace{\cos \alpha}_{\Delta l_x} u_x + \underbrace{\sin \alpha}_{\Delta l_y} u_y$$

CHANGE IN LENGTH



2 DOFs: u_B, v_B

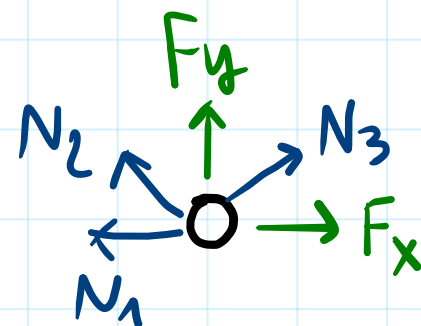
$$l_1 = l \quad A_1 = A$$

$$l_2 = l\sqrt{2} \quad A_2 = \sqrt{2}A$$

$$l_3 = l\sqrt{2} \quad A_3 = \sqrt{2}A$$

E : CONST

SOLVE VIA DISPL. METHOD ; OBTAIN u_B, v_B



$$\left. \begin{aligned} \rightarrow : -N_1 - N_2 \frac{1}{\sqrt{2}} + N_3 \frac{1}{\sqrt{2}} + F_x &= 0 \\ \uparrow : N_2 \frac{1}{\sqrt{2}} + N_3 \frac{1}{\sqrt{2}} + F_y &= 0 \end{aligned} \right\}$$

USE CONSTITUTIVE EQS

$$N_1 = \frac{EA}{l} \Delta l_1$$

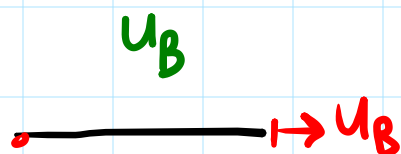
$$N_2 = \frac{E\sqrt{2}A}{l\sqrt{2}} \Delta l_2 = \frac{EA}{l} \Delta l_2$$

$$N_3 = \frac{E\sqrt{2}A}{l\sqrt{2}} \Delta l_3 = \frac{EA}{l} \Delta l_3$$

$$\Delta l_i = \Delta l_i(u_B, v_B) \quad \begin{matrix} > \\ < \end{matrix}$$

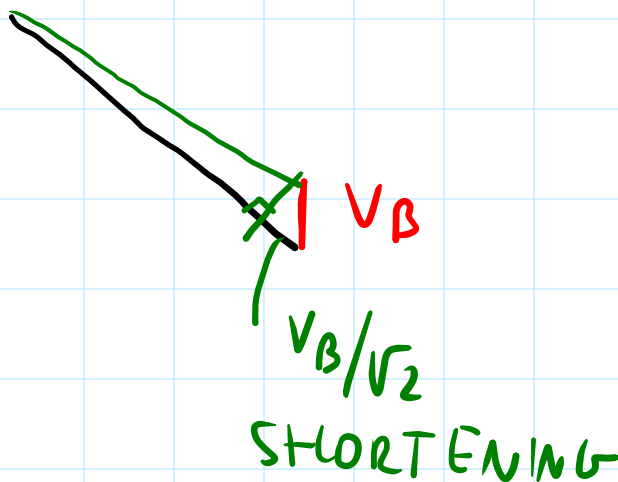
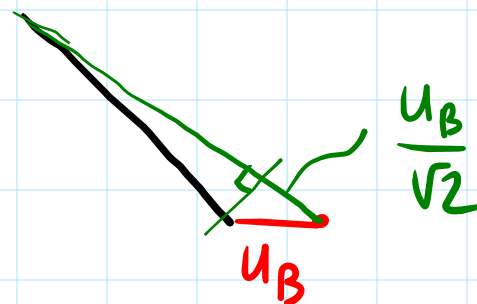
$$K = \frac{EA}{l}$$

1)



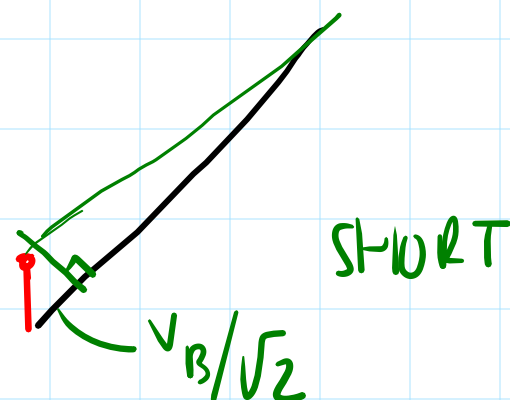
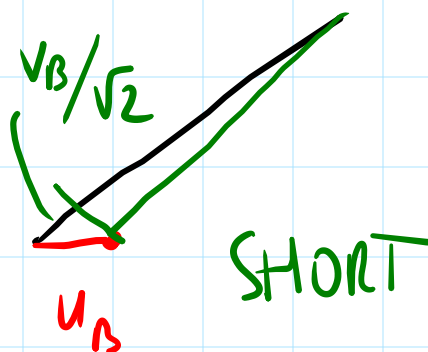
Δl_i
 $\Delta l_1 = +u_B + 0$

2)



$\Delta l_2 = +\frac{u_B}{\sqrt{2}} - \frac{v_B}{\sqrt{2}}$

3)



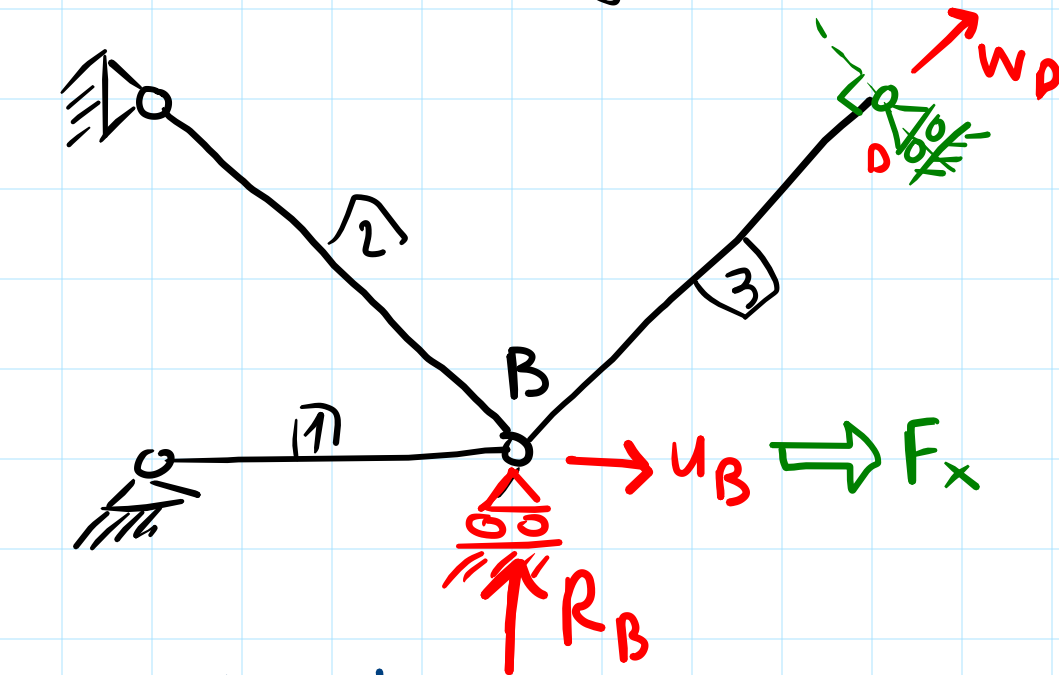
$\Delta l_3 = -\frac{u_B}{\sqrt{2}} - \frac{v_B}{\sqrt{2}}$

$$\text{EQ. EQS : } \left. \begin{aligned} -K u_B - \frac{1}{\sqrt{2}} K \frac{1}{\sqrt{2}} (u_B - v_B) + \frac{1}{\sqrt{2}} K \frac{1}{\sqrt{2}} (-u_B - v_B) + F_x &= 0 \\ + \frac{1}{\sqrt{2}} K \frac{1}{\sqrt{2}} (u_B - v_B) + \frac{1}{\sqrt{2}} K \frac{1}{\sqrt{2}} (-u_B - v_B) + F_y &= 0 \end{aligned} \right\} \begin{matrix} u_B \\ v_B \end{matrix} = f(K, F_x, F_y)$$

$$-\underbrace{\begin{bmatrix} 2K & 0 \\ 0 & K \end{bmatrix}}_{\tilde{K}_{2 \times 2}} \underbrace{\begin{bmatrix} u_B \\ v_B \end{bmatrix}}_{\underline{u}} + \underbrace{\begin{bmatrix} F_x \\ F_y \end{bmatrix}}_{\underline{F}} = \underbrace{\begin{bmatrix} 0 \\ 0 \end{bmatrix}}_{\underline{0}} \Rightarrow \tilde{K} \underline{u} = \underline{F}; \quad \underline{u} = \tilde{K}^{-1} \underline{F}$$

$\tilde{K}$: SYMMETRIC, POSITIVE DEFINITE $\} \tilde{K}^{-1}$ ALWAYS EXIST

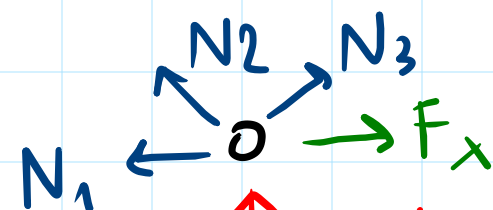
LET US DISCUSS A CHANGE $\Rightarrow$ IN THE PREVIOUS EXERCISE



2 DOFs ; $u_B, w_D \Rightarrow$ EQUIL EQS

$$\sum F_{(u_B)}^B = 0 \rightarrow +$$

$$\sum F_{(w_D)}^B = 0 \nearrow +$$

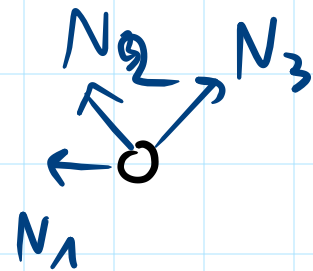
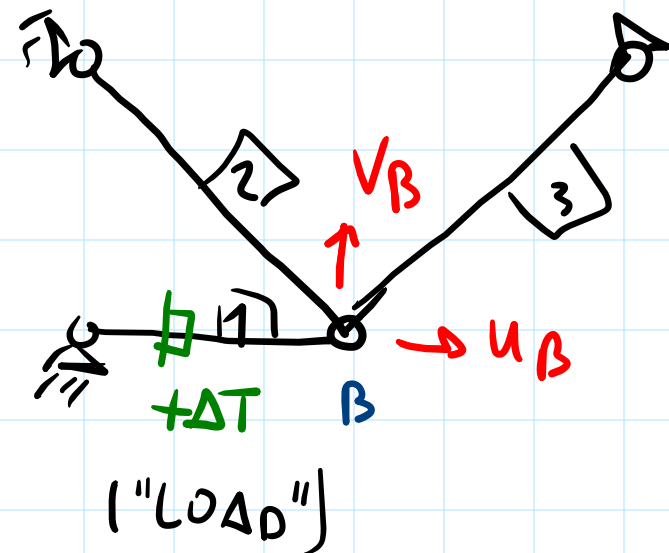


$\uparrow R_B$; THIS IS UNKNOWN
AND CAN BE SOLVED
ONLY AFTER HAVING
OBTAINED u_B, w_D, N_1, N_2, N_3

THROUGH $\sum F^B = 0 \uparrow +$ (R_B IS THE ONLY UNKNOWN)

$$R_B + \frac{N_2}{\sqrt{2}} + \frac{N_3}{\sqrt{2}} = 0$$

HOW TO DEAL WITH A THERMAL VARIATION



$$\left. \begin{aligned} \rightarrow : -N_1 - \frac{N_2}{\sqrt{2}} + \frac{N_3}{\sqrt{2}} &= 0 \\ \uparrow : \frac{N_2}{\sqrt{2}} + \frac{N_3}{\sqrt{2}} &= 0 \end{aligned} \right\} \text{NO APPLIED FORCES}$$

CONST. EQS: $N_2 = \frac{E\sqrt{2}A}{\sqrt{2}l} \Delta l_2$; $N_3 = \frac{E\sqrt{2}A}{\sqrt{2}l} \Delta l_3$

$$N_1 = \frac{EA}{l} \Delta l_1^{\text{elast}} = \frac{EA}{l} (\Delta l_1 - \alpha \Delta T l)$$

SEE PREVIOUS EXCHANGE
(u_B, v_B)

$$\begin{bmatrix} 2K & 0 \\ 0 & K \end{bmatrix} \begin{bmatrix} u_B \\ v_B \end{bmatrix} = \begin{bmatrix} K\alpha\Delta T l \\ 0 \end{bmatrix}$$

u IS A FUNCTION OF THE "THERMAL LOAD"

$\tilde{K}$

u

F

$$\tilde{K} \underline{u} = \underline{F}^{\text{el}} + \underline{F}^{\text{INELASTIC}} + \underline{F}^{\text{DISP}^*}$$

* $\underline{F}^{\text{DISP}}$: DISPLACEMENT IMPOSED TO CONSTRAINED